

Electronic Supplementary Information for:

Using Li⁺ as the electrochemical messenger to fabricate an aqueous rechargeable Zn-Cu battery

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Experimental section

CV curves for Cu electrode were traced on Chenhua 660D electrochemistry workstation at a scan rate of 0.01 V s⁻¹ using a piece of natural graphite brush as the work electrode, Pt electrode as the counter and a saturated calomel electrode (SCE) as the reference. The electrolyte was prepared by carefully adding 0.1 mol L⁻¹ CuSO₄ aqueous solution into 1 mol L⁻¹ Li₂SO₄ aqueous solution. Note that the density of CuSO₄ solution is high than that of Li₂SO₄ and thus sinks to the bottom of the container. As a result, the solution was kept in two layers. Then the counter and the reference were carefully dipped to the bottom of the solution and the graphite brush was kept touching the CuSO₄ layer slightly across the Li₂SO₄ layer. The CV curve for Zn electrode was carried out in the same way.

The Zn-Cu batteries were fabricated as follows. The cathode aqueous electrolyte was composed of CuSO₄ mixed with Li₂SO₄ with a concentration of 0.1 mol L⁻¹ and 1 mol L⁻¹, respectively, using a piece of polished copper as the current collector. 0.1 mol L⁻¹ ZnSO₄ mixed with 1 mol L⁻¹ Li₂SO₄ aqueous solution was used as the anode, a piece of polished zinc as the anode current collector. All solutions were washed by N₂ flow for 30 minutes prior to tests. A piece of sandwiched membrane was employed as the separator which had been reported in former

studies.^[1] A mixture of LiClO₄ and PMMA (polymethylmethacrylate) in N-methyl-2-pyrrolidone (NMP) solution was cast on a porous PVDF (poly(vinylidene fluoride) film. The mass ratio of LiClO₄ and PMMA is about 1:10. After dried at 75 °C in vacuum, another layer of the porous PVDF film was covered on the PMMA layer. Then the membrane was tailored into a disk with a thickness of about 0.2 mm. SS-Cu and Zn-C systems were constructed in the same way with Zn-Cu battery, by using stainless steel replacing the Zinc electrode or the carbon brush replacing the copper electrode, respectively.

The impedance spectra in the frequency range of 0.01 Hz–100 kHz was characterized using zinc as the work electrode and copper as the counter. The excitation voltage was 10 mV. The charge-discharge curves and cycle calendar life were traced on a cell tester (Neware) between 0.5–1.5 V. All of the characterizations were collected at room temperature. An *ex-situ* ICP-AES examination was performed to study the concentration of Cu²⁺ and Li⁺ swung with charge and discharge process. Four Zn-Cu batteries that obtained almost the same contents were fabricated and performed at various charge-discharge depths. Then the electrodes were taken out and the left electrolytes were subjected to the ICP-AES. Scanning electron microscope (SEM) images of the samples were collected on a JSM-6360LA. Conventional powder XRD patterns were carried out in the 10–80° 2 θ range using a D/max 2500 PC with vertical goniometer and Cu K α radiation (λ =1.5406 Å).

References

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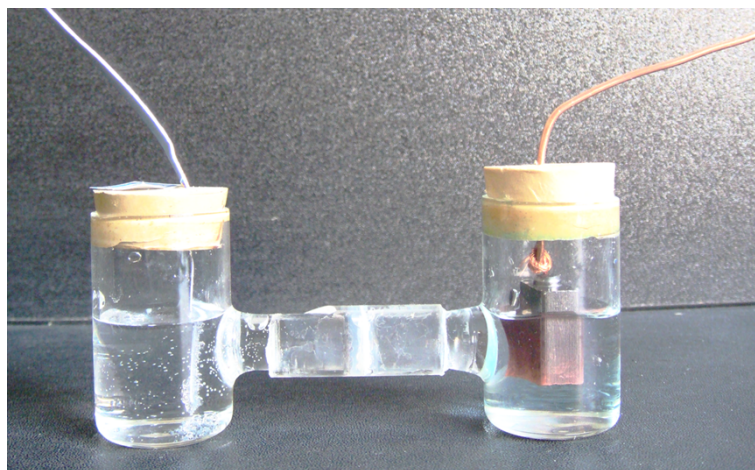


Fig. S1 The Zn|ZnSO₄ + Li₂SO₄|ion-block membrane|CuSO₄ + Li₂SO₄|Carbon system.

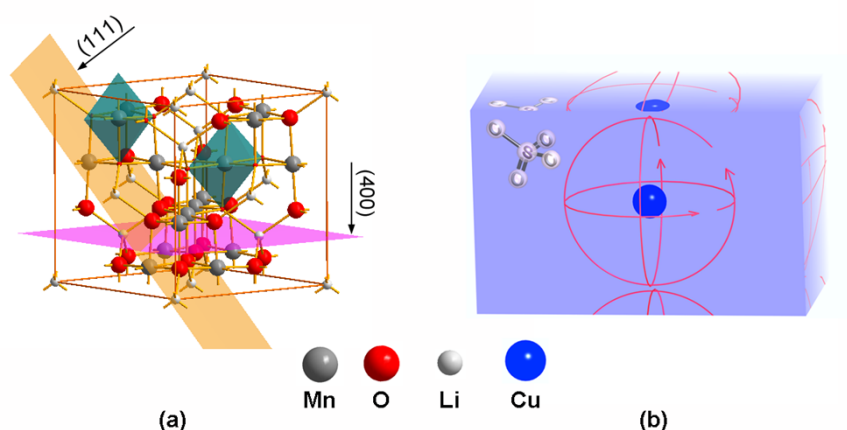


Fig. S2 The chemical surroundings of (a) the Mn³⁺/Mn⁴⁺ active centre in LiMn₂O₄ crystal lattice and (b) Cu²⁺ in CuSO₄ aqueous solution.

The capacity loss for materials in solid state might be different with materials in liquid state. In the Zn-Cu system, the practical capacity is 98.5% of the theoretical capacity. This result is notable since the practical capacities for most of the active materials in solid state are much lower than their theoretical capacity.¹⁻⁶ The capacity loss for materials in solid state might be ascribed to the steric hindrance that prohibits the free rotation of the active interface to the right direction, leading to the decrease of the capacity, as illustrated in Fig. S2. In the case of LiMn₂O₄, facet (111) is

superior, although enhancing facet (400) is helpful for the intercalation/de-intercalation of Li^+ , the $\text{Mn}^{3+}/\text{Mn}^{4+}$ active centre is still confined in the crystal lattice which indicates $\text{Mn}^{3+}/\text{Mn}^{4+}$ redox couple can not receive-release the electrons freely.⁷ In the case of CuSO_4 in aqueous solution however, no steric hindrance holds back the movement of the Cu^{2+} active centre. As a result, the active ions can move and rotate freely to the right location and right direction to accept or release electrons, which certainly helps to elevate the capacity.

References

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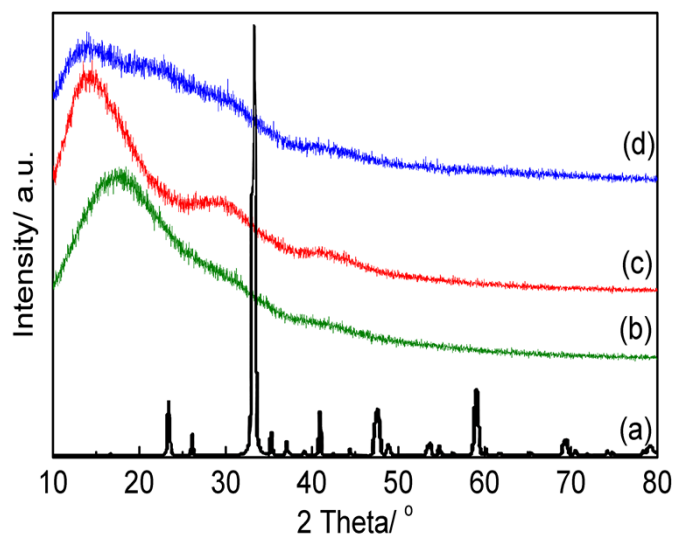


Fig. S3 XRD patterns of the contents of the PVDF/PMMA- LiClO_4 /PVDF sandwiched ion-block membrane. (a) LiClO_4 . (b) PMMA. (c) PMMA mixed with LiClO_4 before cycling, and (d) The PMMA- LiClO_4 inner layer after 332 cycles with the outer PVDF layers being peeled off.

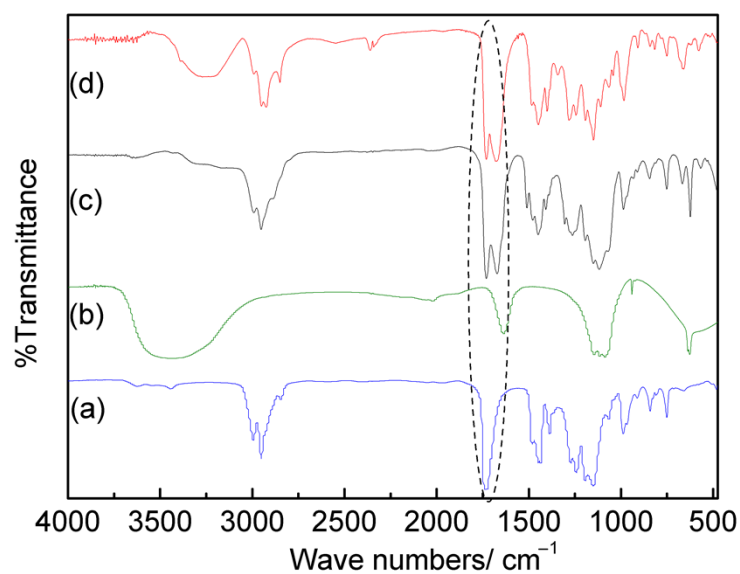


Fig. S4 FTIR of the contents of the PVDF/PMMA- LiClO_4 /PVDF sandwiched ion-block membrane. (a) PMMA. (b) LiClO_4 . (c) The original PMMA- LiClO_4 film, and (d) The PMMA- LiClO_4 inner layer after 332 cycles with the outer PVDF layers being peeled off.

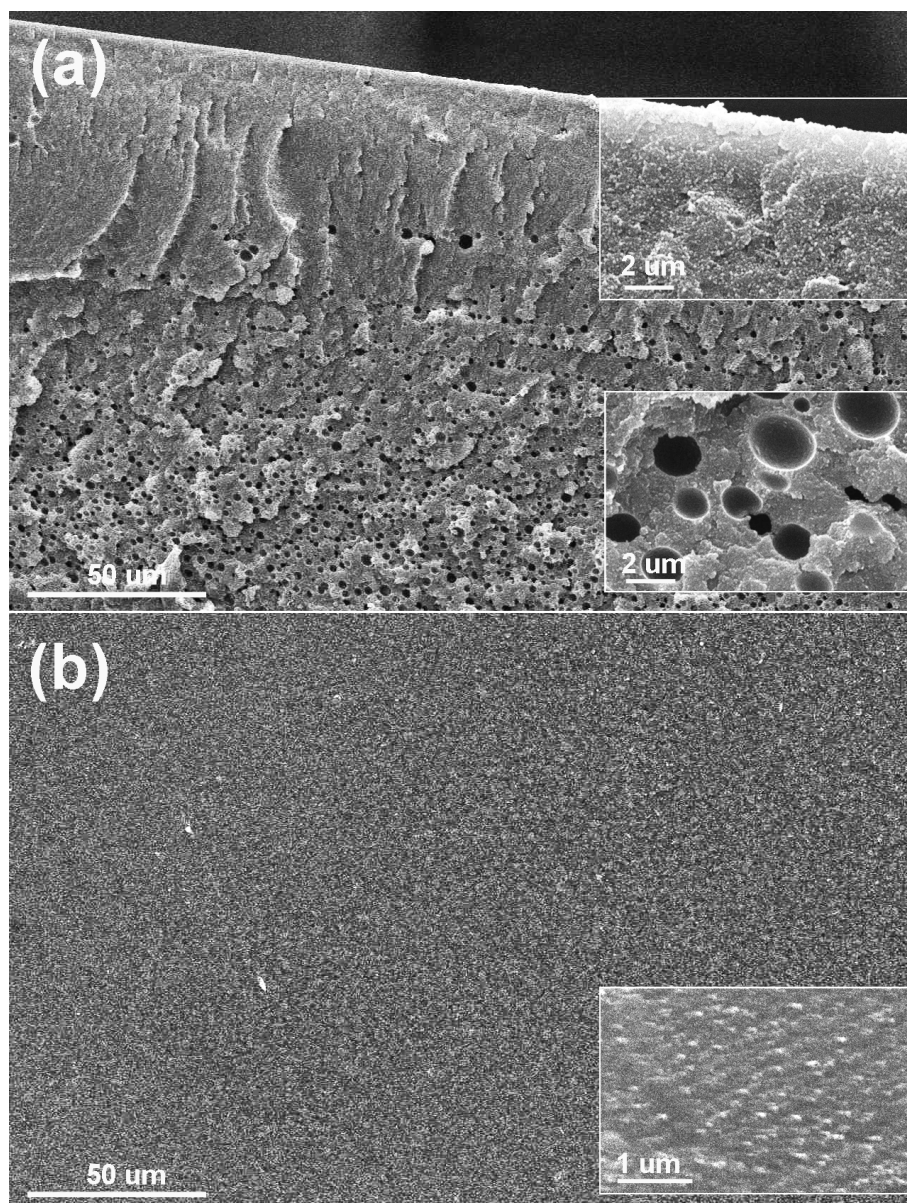


Fig. S5 SEM of (a) the section and (b) the surface of the PVDF/PMMA-LiClO₄/PVDF sandwiched ion-block membrane after 332 cycles with the outer PVDF layers being peeled off.

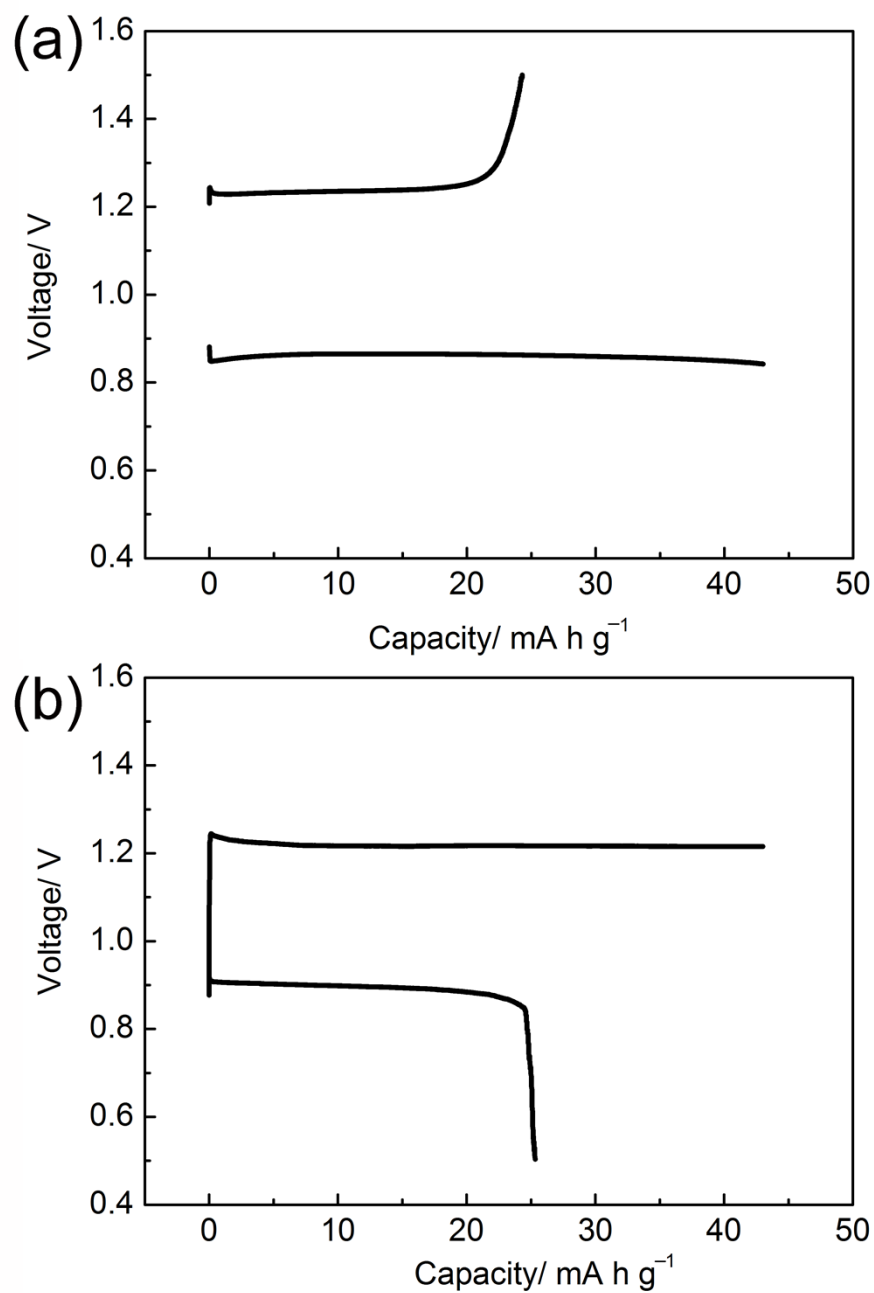


Fig. S6 Charge-discharge curves of (a) Zn-C and (b) SS-Cu systems at a current density of 6 mA cm⁻².

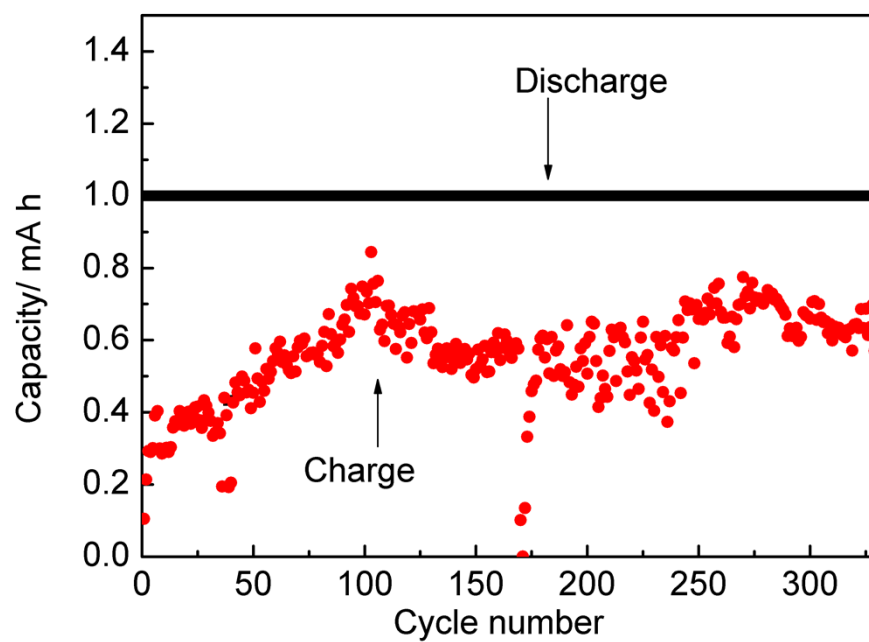


Fig. S7 Cyclic performance of Zn-C system. The discharge capacity is controlled at 1 mA h.

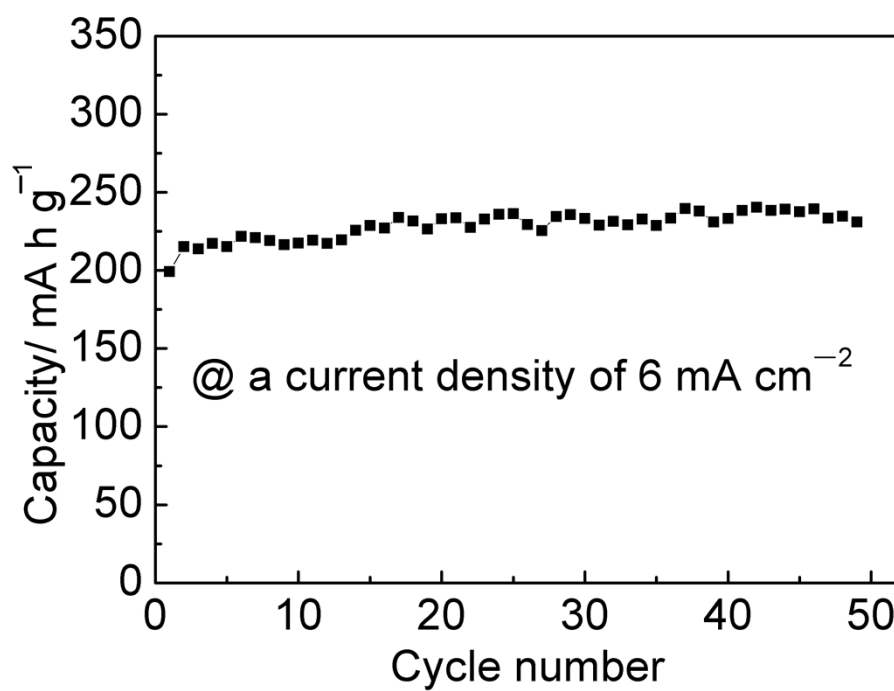


Fig. S8 Cyclic performance of the Zn-Cu system based on the capacity of CuSO₄. The current density is calculated according to the area of the membrane that the current passes through.

Calculation of the theoretical capacity for CuSO₄

The calculation is based on the following equation:

$$C = Q/M \quad (1)$$

where C is the capacity, Q corresponds to the quantity of electricity carried by per mole of CuSO₄ in unit time, and M is the molecular weight.

Then, after unit conversions,

$$C = 2 \times 1.602 \times 10^{-19} \times 6.02 \times 10^{23} \div 3600 \div 159.61 \times 1000 = 336 \text{ mAh g}^{-1} \quad (2)$$

In our work, the practical capacity based on CuSO₄ is up to 330 mA h g⁻¹ at a current density of 1 mA cm⁻², which is 98.5% of the theoretical capacity without considering the concentration of the aqueous solution. Here we intend to disclose that almost all of the CuSO₄ in the solution has been involved in the electrochemical reaction, which is different from most of solid active materials. When the concentration of the aqueous solution is taken into consideration, the theoretical capacity of CuSO₄ would be as follows:

$$C = 2 \times 1.602 \times 10^{-19} \times 6.02 \times 10^{23} \div 3600 \div 159.61 \times 1000 \times 20.5\% = 69 \text{ mAh g}^{-1} \quad (3)$$

Here the concentration of the CuSO₄ in aqueous solution is about 20.5 wt% at 20 °C (according to Lange's Handbook of Chemistry, 15th Edition). However, the practical capacity would still be 98.5% of the theoretical capacity.

On the other hand, if the calculation is carried out according to the mass of ZnSO₄, the anode material in aqueous solution, the theoretical capacity would be 332 mAh g⁻¹. When the concentration of 53.8 wt% at 20 °C is accounted (according to Lange's Handbook of Chemistry, 15th Edition), the theoretical capacity would come to be 179 mAh g⁻¹. In either case, the practical capacity would be 98.5% of the theoretical capacity.

Table S1. Technology Comparison of Potential Batteries^a for Utility Applications^{b, c}

type	open circuit voltage (V)	specific energy (W h kg ⁻¹)	operating temperature (°C)	Discharge time (h)	self-discharge % per month, @ 20 °C	cycle life (deep cycles)	round-trip DC energy efficiency (%)
LAB	2.1	25–40	–40–60	Up to 8 h	4–50	1000	50–75
NCB	1.35	30–45	–10–45	Up to 4 h	5–20	2000	55–70
VRB	1.4	10–20	10–40	4–12 h	3–9	5000	65–80
LCB	2.1	25–40	–40–60	Up to 4 h		3000	
Na-S	2.1	150–240	300–350	4–8 h	negligible	4000	75–90
ZEBRA	2.6	95–120	300–350	4–8 h	negligible	3000	75–90
C-LC	3–4	155	–25–40	Up to 4 h	2	1000	94–99
LT-LFP	1.7	50–70	–25–40	Up to 4h	2	4000	94–99
CLB	1.4	30–45	–10–45	Up to 4 h	3–9	4000	85–95
Zn-Cu	1.08	68	–10–45	Up to 4 h	3–9	4000	85–95

^a LAB: lead-acid batteries; NCB: nickel-cadmium batteries; VRB: all-vanadium redox flow batteries; LCB: lead-carbon ultrabatteries; Na-S: sodium-sulfur batteries; ZEBRA: Zeolite Battery Research Africa; C-LC: Li-ion batteries of C anode and LiCoO₂ cathode; LT-LFP: Li-ion batteries of Li₄Ti₅O₁₂ anode and LiFePO₄ cathode; CLB: Cr³⁺ (aqueous)/LiMn₂O₄ hybrid redox flow battery. Zn-Cu: Zn|ZnSO₄ + Li₂SO₄|PVDF/PMMA-LiClO₄/PVDF | CuSO₄ + Li₂SO₄|Cu battery

^b Except CLB and Zn-Cu, the other data is referenced from dx.doi.org/10.1021/cr100290v | *Chem. Rev.* 2011, 111, 3577–3613.

^c CLB is referenced from *J. Mater. Chem. A*, 2013, 1, 14476–14479

Calculation of the specific energy of the aqueous rechargeable Zn-Cu Daniell-type battery

(a) The theoretical specific energy (with the ideal concentration of 100 wt% for the electrode, i.e., water is neglected at the state of 100% DOD)



$$W = V \times 1000 / (Q^+ + Q^-) \text{ (W h kg}^{-1}\text{)} \quad (5)$$

Where W, V, Q⁺ and Q[–] represents energy density, open-circuit voltage, electrochemical equivalence of the cathode and electrochemical equivalence of the anode, respectively.

For this system,

$$V = 1.08 \text{ V.} \quad (6)$$

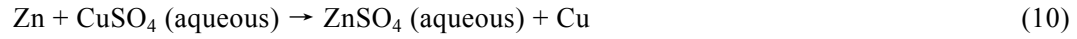
$$Q^+ = M_{\text{CuSO}_4} / (26.8 \times 2) = 159.61 / (26.8 \times 2) = 2.98 \text{ g (A h)}^{-1} \quad (7)$$

$$Q^- = M_{\text{Zn}} / (26.8 \times 2) = 65.38 / (26.8 \times 2) = 1.22 \text{ g (A h)}^{-1} \quad (8)$$

As a result, $W = 1.08 \times 1000 / (2.98 + 1.22) = 257 \text{ W h kg}^{-1}$

(9)

(b) The expected specific energy (with an aqueous concentration of 20.5 wt% for the cathode CuSO₄)



The formula is:

$$W = V \times 1000 / (Q^+ + Q^-) \text{ (W h kg}^{-1}\text{)} \quad (11)$$

Where,

$$V = 1.08 \text{ V} \quad (12)$$

$$Q^+ = M_{\text{CuSO}_4} / (26.8 \times 2 \times 14\%) = 159.61 / (26.8 \times 2 \times 20.5\%) = 14.53 \text{ g (A h)}^{-1} \quad (13)$$

$$Q^- = M_{\text{Zn}} / (26.8 \times 2) = 65.38 / (26.8 \times 2) = 1.22 \text{ g (A h)}^{-1} \quad (14)$$

As a result,

$$W = 1.08 \times 1000 / (14.53 + 1.22) = 68 \text{ W h kg}^{-1} \quad (15)$$