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1	Supporting information
2	for
3	Heterogeneous reaction of sulfur dioxide on mineral dust
4	nanoparticles: from single component to mixed components
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Figure S1. Hematite-alumina mixtures after grinding preparations.
(From left to right, HA-100 to HA-0)



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## Figure S2. DRIFTS spectra of hematite during pretreatment process.

Before the introduction of  $SO_2$  into the DRIFTS chamber, each sample was pretreated in a stream of high-pure air with a flow of 100 ml·min<sup>-1</sup> for 60 min to blow off water and impurities on sample surfaces. A background was recorded before the pretreatment, and then a series of spectra were collected every five minutes.

Negative peaks located at 3701 and 1643 cm<sup>-1</sup>, as well as the broad bands between 3650-2900 cm<sup>-1</sup> and centered at 2100 cm<sup>-1</sup> are totally attributed to the vibrations of O-H groups. In detail, the peaks centered at 1643 and 2100 cm<sup>-1</sup> are both assigned to liquid water,<sup>1-3</sup> whereas the others are characteristics of diverse surface hydroxyl groups.<sup>4-6</sup> Carbonate species formed during sample preparations significantly decreased, as evident by the successive peaks around 1539, 1310 and 1084 cm<sup>-1</sup>.<sup>7, 8</sup> All the peaks declined over time and then gradually became stable after 45 min. The spectra of all the mixtures are roughly the same. Therefore, 60 min pretreatment was employed in each experiment.



Figure S3. XRD patterns of the (a) laboratory prepared hematite, (b) purchased alumina, and (c) HA-50
 mixture. All samples were manually grinded before XRD analysis.

X-ray diffraction (XRD) patterns of the two oxides match well to the standard Joint Committee on
 Powder Diffraction Standards (JCPDS) Cards of iron oxide (PDF 33-0664) and corundum (PDF 10-0173),

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Hematite (%)	S <sub>BET</sub> (m <sup>2</sup> ·g <sup>-1</sup> )	Pore volume (cm <sup>3</sup> ·g <sup>-1</sup> )	Pore size (nm <sup>2</sup> )
0	46.97	0.251	21.335
10	46.19	0.252	21.705
20	45.37	0.249	21.954
30	43.41	0.243	22.157
40	41.65	0.236	22.387
50	39.66	0.226	22.720
60	37.42	0.217	23.227
70	34.60	0.207	23.984
80	32.23	0.199	25.064
90	29.27	0.193	26.542
100	26.23	0.190	28.491

**Table S1.** BET specific surface area ( $S_{BET}$ ), pore volume and pore size of the hematite-alumina mixtures





Figure S5. DRIFTS spectra of hematite-alumina mixtures after 60 min exposure to SO<sub>2</sub>-containing
 high-pure air. From a to k: mixtures from HA-0 to HA-100.

81 Smoothing processes were employed for the spectra of HA-0, HA-10, HA-20, HA-30 and HA-40,

82 owing to the strong lattice oxide absorptions of alumina.<sup>3</sup>

 Table S2. Parameters for uptake coefficient calculations

Parameter (	unit)	Value
Sulfate formation rate: $d[S$	$[0^{2}_{4}]/dt$ (ion·s <sup>-1</sup> )	According to reactions
	$A_{BET}$ (m <sup>2</sup> )	$S_{BET}$ ×sample mass 1.96×10 <sup>-5</sup> 1.15×10 <sup>20</sup>
ticle reactive surface area: As (m <sup>2</sup> )	A <sub>geo</sub> (m <sup>2</sup> )	1.96×10-5
Reactant concentration: [So	O₂] (molecule∙m⁻³)	$1.15 \times 10^{20}$
$v_{S0_2}$ Temperatu	Gas constant: R (J·mol <sup>-1</sup> ·K <sup>-1</sup> )	8.314
	Temperature: T (Kelvin)	298
	Molar mass: $M_{SO_2}$ (kg·mol <sup>-1</sup> )	6.4×10 <sup>-2</sup>
	Pi: $\pi$ (dimensionless)	3.1416

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Figure S6. Calibration plot with numbers of  $SO_4^{2-}$  versus corresponding integrated areas for sulfate products on hematite.

A conversion is obtained from a calibration plot with the number of  $SO_4^{2-}$  analyzed by IC versus the integrated areas for sulfate products on hematite. Ultrapure water (5 ml, specific resistance  $\ge 18.2 \text{ M}\Omega$  cm) containing 1% formaldehyde was used as extraction solvent to prevent oxidation processes. A spectral peak-fitting program using Gaussian-Lorentzian peak fitting was employed to the product spectra, and the integrated areas of sulfate peaks were calculated.

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101 Figure S7. Integrated areas for sulfur-containing products on fresh (green) and sulfated HA-50 (red).

102 For fresh sample, product formation rate is relatively low in the beginning, resulting probably from the 103 initial diffusion of  $SO_2$  on particle surfaces. The formation rate for sulfated sample (after 20 min in-situ

104 exposure to  $SO_2$ ) is much higher than that for fresh nanoparticles.



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Figure S8. Linear fitting of product integrated areas during different reaction episodes: (a) 0-60 min; (b)
 20-60 min. Take HA-50 as an example.

After being introduced to the DRIFTS chamber, some SO<sub>2</sub> molecules diffuse to the nanoparticle surface, resulting in the slow product formation rate in the initial episode (0-20 min). Therefore, for the scatter diagram of product integrated areas as a function of time, the slope and  $R^2$  value of fitted curve become larger if the initial episode is not involved. Uptake coefficients for the whole polluted period (0-60 min) may underestimate the real reactive capacity. To reveal the actual and steady process of SO<sub>2</sub> oxidation, only the latter 40 minutes (20-60 minutes) is involved in the uptake coefficient calculations.

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Figure S9. Bilogrithmic plots of the product formation rates versus corresponding SO<sub>2</sub> concentrations for
two studied samples: (a) HA-100; (b) HA-50.

In this study, formation rate of sulfur-containing compounds is related to  $SO_2$  concentration, number of active sites on mixture surfaces, and  $O_2$  concentration, which could be shown by **equation S1** based on the law of mass action.<sup>9, 10</sup>

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$$d[SO_4^{2-}]/dt = k[SO_2]^m[Mixture]^n[O_2]^p$$
 Eq.S1

Where  $[SO_4^{2-}]$  is the concentration of products,  $[SO_2]$  is the concentration of SO<sub>2</sub>, [*Mixture*] is the concentration of active sites on mixture surfaces,  $[O_2]$  is the concentration of O<sub>2</sub>, m, n, p are the reaction orders of SO<sub>2</sub>, active site and O<sub>2</sub>, respectively. Oxygen is sufficient for the oxidation processes.<sup>11</sup> No saturation effects on the formation of sulfur-containing products were observed, and thus the [*Mixture*] is approximately constant.<sup>6</sup> Hence, the product formation rate is largely relative to SO<sub>2</sub> concentration. As reported previously, the reaction order here is determined by double-logarithmic plots of the formation rates versus the SO<sub>2</sub> concentrations based on **equation S2**.<sup>6, 12, 13</sup>

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$$\ln\left(d\left[SO_{4}^{2-}\right]/dt\right) = m\ln[SO_{2}] + n\ln[Mixture] + p\ln[O_{2}] + lnk \qquad Eq.S2$$

The reaction order for HA-100 and HA-50 are 1.16 and 1.12, respectively, both indicating the reaction order of 1 for SO<sub>2</sub>. Therefore, the heterogeneous uptake of SO<sub>2</sub> on hematite-alumina mixture can be viewed as pseudo-first-order reaction.

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135 **Table S3.** Summary of uptake coefficients for the heterogeneous reactions of SO<sub>2</sub> on hematite-alumina

mixtures			
Hematite (%)	γβετ	$\gamma_{ m geo}$	
0	7.37×10 <sup>-13</sup> ±2.73×10 <sup>-13</sup>	<b>3.42</b> ×10 <sup>-8</sup> ±1.44×10 <sup>-8</sup>	
10	1.18×10 <sup>-12</sup> ±1.05×10 <sup>-13</sup>	7.56×10-8±1.61×10-8	
20	1.47×10 <sup>-12</sup> ±8.93×10 <sup>-15</sup>	<b>9.12</b> ×10 <sup>-8</sup> ±2.58×10 <sup>-9</sup>	
30	<b>3.96</b> ×10 <sup>-12</sup> ±7.07×10 <sup>-13</sup>	<b>2.49</b> ×10 <sup>-7</sup> ±5.36×10 <sup>-8</sup>	
40	<b>9.08</b> ×10 <sup>-12</sup> ±2.60×10 <sup>-14</sup>	6.57×10 <sup>-7</sup> ±2.51×10 <sup>-8</sup>	
50	<b>3.31</b> ×10 <sup>-11</sup> ±3.10×10 <sup>-12</sup>	2.30×10 <sup>-6</sup> ±2.58×10 <sup>-7</sup>	
60	<b>4.64</b> ×10 <sup>-11</sup> ±1.46×10 <sup>-12</sup>	<b>2.80</b> ×10 <sup>-6</sup> ±1.12×10 <sup>-7</sup>	
70	7.34×10 <sup>-11</sup> ±4.65×10 <sup>-12</sup>	<b>4.29</b> ×10 <sup>-6</sup> ±1.60×10 <sup>-7</sup>	
80	8.53×10 <sup>-11</sup> ±3.59×10 <sup>-13</sup>	<b>5.15</b> ×10 <sup>-6</sup> ±8.74×10 <sup>-8</sup>	
90	8.87×10 <sup>-11</sup> ±6.21×10 <sup>-12</sup>	<b>5.20</b> ×10 <sup>-6</sup> ±2.66×10 <sup>-7</sup>	
100	<b>9.00</b> ×10 <sup>-11</sup> ±6.68×10 <sup>-12</sup>	<b>5.68</b> ×10 <sup>-6</sup> ±4.14×10 <sup>-7</sup>	

18.0 Polluted period 15.0 Integrated area 12.0 Π 9.0 6.0 **Clean period** 3.0 0.0 20 40 60 80 100 120 Reaction time (min)

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139 Figure S10. Integrated areas for sulfur-containing products during polluted period (I), clean period (II),

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and clean period with the DRIFTS chamber closed (III).

141 The experiment including three steps is aimed at verifying the sources of sulfur-containing products in

142 clean period.

143 I. Sulfur-containing species were formed on HA-50 along with the introduction of SO<sub>2</sub> in polluted144 period.

II. SO<sub>2</sub> was cut off and only high-pure air (100 ml·min<sup>-1</sup>) was introduced for 25 min. The calculated air
volume (2500 ml) is 1000 times more than that of the DRIFTS chamber (2.5×10<sup>-5</sup> m<sup>3</sup>). Hence, the
chamber was washed for about 1000 times and could be considered clean.<sup>14</sup> The process is mainly
aimed at thoroughly flowing away the residual SO<sub>2</sub> in gas supply system and reaction chamber. Prior

149 research has found the extremely low adsorption capacity of the DRIFTS chamber.<sup>8</sup>

150 III. Pure air flux was also cut off and then the inlet and the outlet of the chamber were closed. The reaction

151 only proceeded in a closed environment. Formation still occurred during this period.

Therefore, sulfur-containing species formed during clean period originate primarily from the  $SO_2$ physically adsorbed on mixtures in polluted period, rather than the residual  $SO_2$  in gas supply system and/or DRIFTS chamber.

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Table S4. Sulfate yields on hematite-alumina mixtures in polluted and clean periods

	Polluted period			Clear	n period	
Hematite (%)	Y ma (ion·g <sup>-1</sup> )	Y st (ion·g <sup>-1</sup> )	Dev	Y ma (ion·g <sup>-1</sup> )	Y st (ion·g <sup>-1</sup> )	Dev
0	$1.11 \times 10^{15} \pm 4.82 \times 10^{14}$		0.0 %	7.10×10 <sup>14</sup> ±	1.21×10 <sup>15</sup>	0.0 %
10	1.50×10 <sup>15</sup> ±5.50×10 <sup>12</sup>	<b>6.68</b> ×10 <sup>15</sup>	-77.6 %	<b>9.95</b> ×10 <sup>14</sup> ±1.38×10 <sup>14</sup>	<b>1.73</b> ×10 <sup>15</sup>	-42.4 %
20	$1.84 \times 10^{15} \pm 7.88 \times 10^{13}$	<b>1.22</b> ×10 <sup>16</sup>	-85.0 %	$1.14 \times 10^{15} \pm 3.90 \times 10^{14}$	<b>2.74</b> ×10 <sup>15</sup>	-58.5 %
30	<b>4.33</b> ×10 <sup>15</sup> ±7.23×10 <sup>14</sup>	<b>1.78</b> ×10 <sup>16</sup>	-75.7 %	$3.14 \times 10^{15} \pm 3.38 \times 10^{14}$	<b>3.76</b> ×10 <sup>15</sup>	-16.4 %
40	$\pmb{8.61}{\times}10^{15}{\pm}1.25{\times}10^{13}$	<b>2.34</b> ×10 <sup>16</sup>	-63.1 %	<b>6.79</b> ×10 <sup>15</sup> ±6.25×10 <sup>14</sup>	<b>4.77</b> ×10 <sup>15</sup>	42.4 %
50	$3.03 \times 10^{16} \pm 3.21 \times 10^{15}$	<b>2.89</b> ×10 <sup>16</sup>	4.6 %	$1.01 \times 10^{16} \pm 1.53 \times 10^{15}$	<b>5.79</b> ×10 <sup>15</sup>	74.6 %
60	4.15×10 <sup>16</sup> ±1.35×10 <sup>15</sup>	<b>3.45</b> ×10 <sup>16</sup>	20.2 %	$1.04 \times 10^{16} \pm 1.42 \times 10^{15}$	<b>6.80</b> ×10 <sup>15</sup>	52.5 %
70	6.15×10 <sup>16</sup> ±4.14×10 <sup>15</sup>	<b>4.01</b> ×10 <sup>16</sup>	53.5 %	$1.15 \times 10^{16} \pm 1.01 \times 10^{15}$	7.82×10 <sup>15</sup>	47.1 %
80	6.62×10 <sup>16</sup> ±1.30×10 <sup>14</sup>	<b>4.56</b> ×10 <sup>16</sup>	45.1 %	$1.16 \times 10^{16} \pm 8.14 \times 10^{14}$	8.83×10 <sup>15</sup>	31.4 %
90	6.20×10 <sup>16</sup> ±4.37×10 <sup>15</sup>	<b>5.12</b> ×10 <sup>16</sup>	21.2 %	$1.19 \times 10^{16} \pm 1.33 \times 10^{15}$	<b>9.85</b> ×10 <sup>15</sup>	21.2 %
100	<b>5.68</b> ×10 <sup>16</sup> ±4.01×10 <sup>15</sup>		0.0 %	<b>1.09</b> ×10 <sup>16</sup> ±	7.26×10 <sup>14</sup>	0.0 %

157 Deviation (Dev) is calculated in this study based on equation S3 to present the gaps between Y<sub>ma</sub> and

158 corresponding Y<sub>st</sub>.

$$Dev = \frac{(Y_{ma} - Y_{st})}{Y_{st}} \times 100\% \qquad Eq.S3$$

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Figure S11. Oxidation of adsorbed SO<sub>2</sub> and sulfite products.

As described in **Figure S10**, a series of experiments were carried out to confirm the physical adsorption of SO<sub>2</sub> on the nanoparticle surface. Each sample was exposed to SO<sub>2</sub> (4.686 ppm) for 50 minutes under dry condition before IC analysis. HCHO solution or high-pure air were introduced to the extraction solutions to prevent or accelerate oxidation processes, respectively. Blank experiments for unreacted samples were considered. The sulfate yields of sample A, B, C and D are denoted as  $Y_A$ ,  $Y_B$ ,  $Y_C$ and  $Y_D$ , respectively.

180 Y<sub>B</sub> is higher than Y<sub>A</sub>, and Y<sub>D</sub> is higher than Y<sub>C</sub>, both suggesting the oxidation of sulfite species. Due 181 to the great capacity of hematite in the heterogeneous oxidation of SO<sub>2</sub> to sulfate products, Y<sub>A</sub> is 182 significantly higher than Y<sub>C</sub>. Note that, Y<sub>D</sub> is extremely higher than Y<sub>B</sub> although the integrated area for the total sulfur-containing products on alumina after 60 min SO<sub>2</sub> exposure is much lower than that on hematite 183 184 (Figure S4). It has been confirmed that physisorbed and chemisorbed SO<sub>2</sub> (surface-coordinated sulfite) are formed after interactions of SO<sub>2</sub> with acid and base sites on α-Al<sub>2</sub>O<sub>3</sub> surfaces, respectively.<sup>12, 15, 16</sup> Hence, 185 186 the gap between Y<sub>C</sub> and Y<sub>D</sub> is attributed not only to sulfite oxidation, but also the oxidation of large amount 187 of physically adsorbed SO<sub>2</sub> on alumina inner surfaces. As amphoteric metal oxide with relative large  $S_{BET}$ 188 and pore volume (Table S1), alumina contains many effective acid sites. As basic metal oxide, hematite 189 contains few acid sites on surfaces, which makes SO<sub>2</sub> physical adsorption difficult.



Figure S12. EDX-mapping images of (a) HA-70 and (b) HA-20.

193 Mapping results from a Phenom XL scanning electron microscope equipped with an energy-dispersive

194 X-ray spectrometer (SEM-EDX) present the mass fractions (%) of Fe and Al in the surface layers of HA-70

195 and HA-20. There are no significant differences between measured and theoretical values. The hematite

196 proportions of HA-70 and HA-20 calculated by EDX-mapping results are 69.0% and 21.8%, respectively,

- 197 excluding the possibility of compact surface coating.
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