

- Supplementary Material -

Ethanol condensation at elevated pressure over copper on AlMgO and AlCaO porous mixed-oxide supports

Davi D. Petrolini^{1,†}, Nathaniel Eagan^{2,†}, Madelyn R. Ball², Samuel P. Burt², Ive Hermans², George W. Huber², James A. Dumesic² and Leandro Martins^{1,*}

¹*Instituto de Química, Unesp - Universidade Estadual Paulista, R. Prof. Francisco Degni 55, 14800-900 Araraquara, SP, Brazil*

²*Department of Chemical and Biological Engineering, University of Wisconsin-Madison, 1415 Engineering Drive, Madison, Wisconsin 53706, United States*

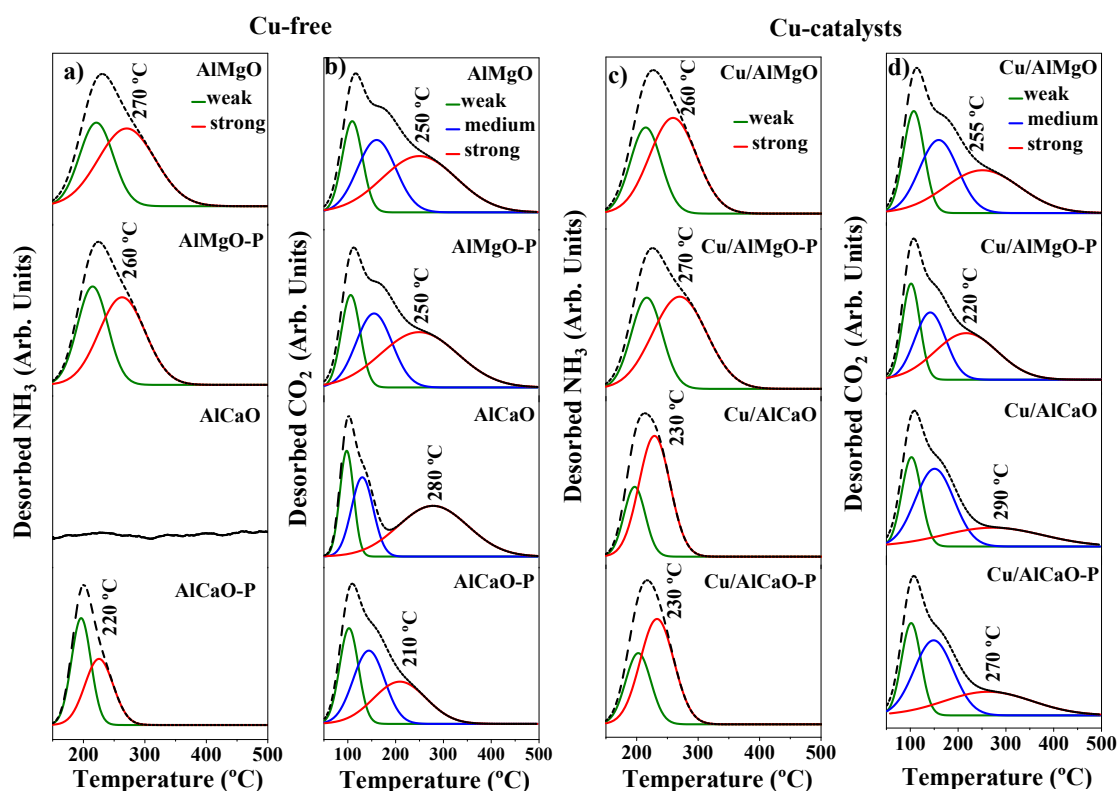


Fig. S1. Deconvolutions of (a, c) NH₃-TPD profiles and (b, d) CO₂-TPD profiles of Cu-free and Cu-catalysts.

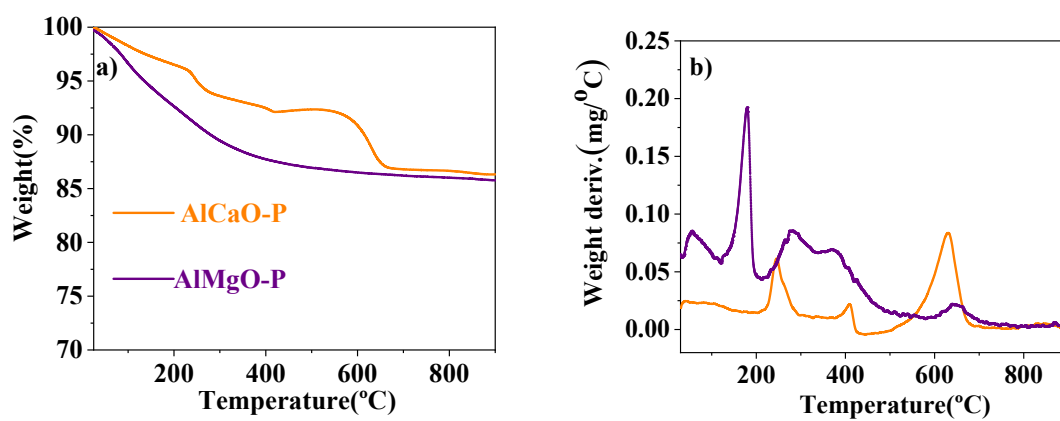


Fig. S2. a) Thermogravimetric curves; b) weight derivative for calcined and exposed to atmospheric environment AlMgO-P and AlCaO-P catalysts.

Table S1. BET area, Cu loading, Cu particle size, Cu⁰ site density, and distribution of strengths of surface acid and basic sites.

Sample	BET area (m ² /g)	Cu loading ^a (%)	Cu particle size ^b (nm)	Cu ⁰ sites ^c (μmol/g)	Acid site distribution ^d			Base site distribution ^e			
					Weak (%)	Strong (%)	Total NH ₃ (μmol/g)	Weak (%)	Medium (%)	Strong (%)	Total CO ₂ (μmol/g)
Cu/AlMgO	106	8.0	3.7	67	37.1	62.9	92.9	25.9	34.6	39.5	115
Cu/AlMgO-P	171	8.0	2.1	91	36.2	63.8	106	25.1	31.2	43.7	78.6
Cu/AlCaO	102	9.0	2.6	118	28.3	71.7	10.1	26.3	45.4	28.4	52.4
Cu/AlCaO-P	120	9.6	3.1	140	33.6	66.4	12.5	26.3	43.1	30.6	49.7
AlMgO	191	-		-	52.6	47.4	76.9	20.9	31.5	47.6	192
AlMgO-P	315	-		-	42.6	57.4	85.6	20.1	30.7	49.2	238
AlCaO	133	-		-	-	-	-*	16.4	36.9	46.7	43.8
AlCaO-P	202	-		-	52.6	47.4	4.0	28.4	36.5	35.1	46.9

^a Cu loading determined by ICP.

^b Cu particle sizes obtained from STEM.

^c Metallic copper sites quantified by N₂O chemisorption.

^d Acid sites quantified from NH₃-TPD profiles.

^e Base sites quantified with CO₂-TPD profiles.

*Without significant acidity.

Table S2. Ethanol (EtOH) dehydrogenation to acetaldehyde (AcAl) equilibrium as a function of pressure compared to experiment. y_{AcAl} is the molar concentration of AcAl in the gas. Temperature = 325°C, EtOH feed concentration = 12.3 vol%, balance H₂.

Pressure (bar)	1-H₂	10-H₂	24-H₂	31-H₂	31-Ar
Equilibrium					
AcAl yield (C%)	55.0	11.1	4.9	3.9	42.0
P _{AcAl} (kPa)	6.40	13.43	14.49	14.67	151.7
y_{AcAl} (mol%)	6.3	1.3	0.6	0.5	4.9
AcAl:EtOH (mol/mol)	1.22	0.13	0.05	0.04	0.72
Experiment					
AcAl yield (C%)	10.1	5.6	2.9	2.5	4.4
P _{AcAl} (kPa)	1.2	6.9	8.4	9.7	17.0
y_{AcAl} (mol%)	1.2	0.7	0.4	0.3	0.5
AcAl:EtOH (mol/mol)	0.12	0.07	0.04	0.03	0.07

Table S3. Data collected from literature for catalysts, reactions conditions, conversion and selectivity for Guerbert coupling. *Nominal WHSV were calculated for batch reactions for approximate comparison with flow studies.

Catalyst	T (°C)	P (bar)	WHSV* (h ⁻¹)	Flow or Batch	Gas Cofeed	Conv. (%)	Sel. (%) to n-butanol	Ref.
AlMgO	325	32	2.1	flow	H ₂	7.1	28.4	This work
AlMgO-P	325	32	2.1	flow	H ₂	11.1	36.2	
Cu/AlMgO	325	32	2.1	flow	H ₂	19.7	48.7	
Cu/AlMgO-P	325	32	2.1	flow	H ₂	23.3	43.3	
Cu/AlMgO-P	325	32	0.7	flow	H ₂	32.8	35.8	
AlCaO	325	32	2.1	flow	H ₂	0.2	42.7	
AlCaO-P	325	32	2.1	flow	H ₂	0.2	61.6	
Cu/AlCaO	325	32	2.1	flow	H ₂	8.7	20.4	
Cu/AlCaO-P	325	32	2.1	flow	H ₂	8.4	21.4	
MgAlOx	250	30	3.2	flow	N ₂	0.2	57.1	[1]
NiMgAlOx	300	30	3.2	flow	N ₂	27.9	45.1	[1]
MgAlOx	200	30	3.5	batch	N ₂	3.6	50.5	[2]
Pd/MgAlOx/0.25Ga	200	30	3.5	batch	N ₂ +H ₂	11.6	94.0	[2]
Pt/MgAlOx	200	30	3.5	batch	N ₂	13.0	82.0	[2]
Cu/AlMgO	310	80	23.7	batch	Ar	37.8	22.0	[3]
Ni/AlMgO	310	80	23.7	batch	Ar	30.3	73.0	[3]
Cu/Ni-AlMgO	310	80	23.7	batch	Ar	47.9	72.0	[3]
MgO	360	2	-	flow	N ₂	4.4	33.0	[4]
Ca ₁₀ (PO ₄) ₆ (OH) ₂	360	2	-	flow	N ₂	4.9	72.0	[4]
Sr ₃ (PO ₄) ₂	360	2	-	flow	N ₂	4.2	9.0	[4]
CuMgAl	300	1	23.7	batch	N ₂	46.5	62.2	[5]
Pd-CuMgAl	260	1	23.7	batch	N ₂	20.9	45.5	[5]
In-CuMgAl	260	1	23.7	batch	N ₂	26.6	60.0	[5]
Ni/γ-alumina	250	180	6.4	flow	He	35.0	61.7	[6]
Ni/Al ₂ O ₃	250	100	23.9	batch	He	25.0	80.0	[7]
Au/Al ₂ O ₃	250	100	23.9	batch	He	6	35	[7]
Cu ₁₀ MgAl ₃ O	200	autogenic	78.9	batch	-	4.5	28.0	[8]
Ag ₅ MgAlO	200	autogenic	78.9	batch	-	1.6	38.8	[8]
Mn ₅ MgAlO	200	autogenic	78.9	batch	-	0.7	53.3	[8]
Fe ₅ MgAlO	200	autogenic	78.9	batch	-	0.3	39.2	[8]
Sm ₅ MgAlO	200	autogenic	78.9	batch	-	1.3	66.3	[8]
Yb ₅ MgAlO	200	autogenic	78.9	batch	-	1.2	53.0	[8]
Mg ₁ Al ₁ O	350	1	-	flow	N ₂	40.5	22.0	[9,10]
Mg ₃ Al ₁ O	350	1	-	flow	N ₂	33.2	34.2	[9,10]
Cu ₅ MgAl ₍₁₎ O	200	autogenic	78.9	batch	-	7.3	50.5	[11]

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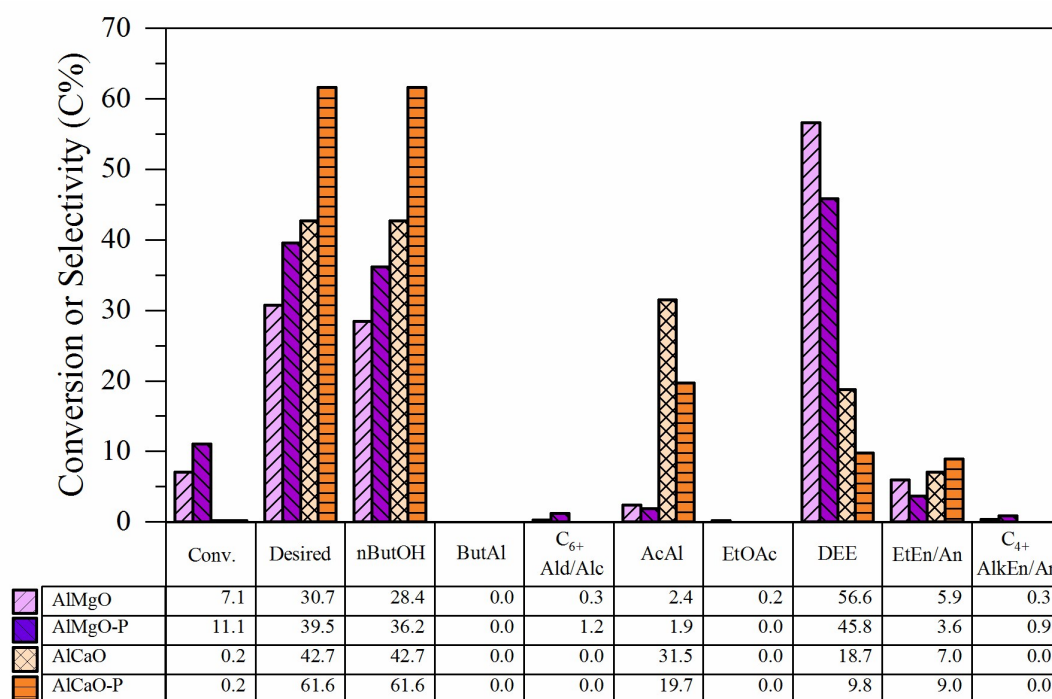


Fig. S3. Conversion and selectivities to major species in ethanol conversion over Cu-free catalysts. Conditions: 325°C, 225 mg catalyst, 10 $\mu\text{L min}^{-1}$ ethanol, 30 mL min^{-1} H_2 , 32 bar total pressure.

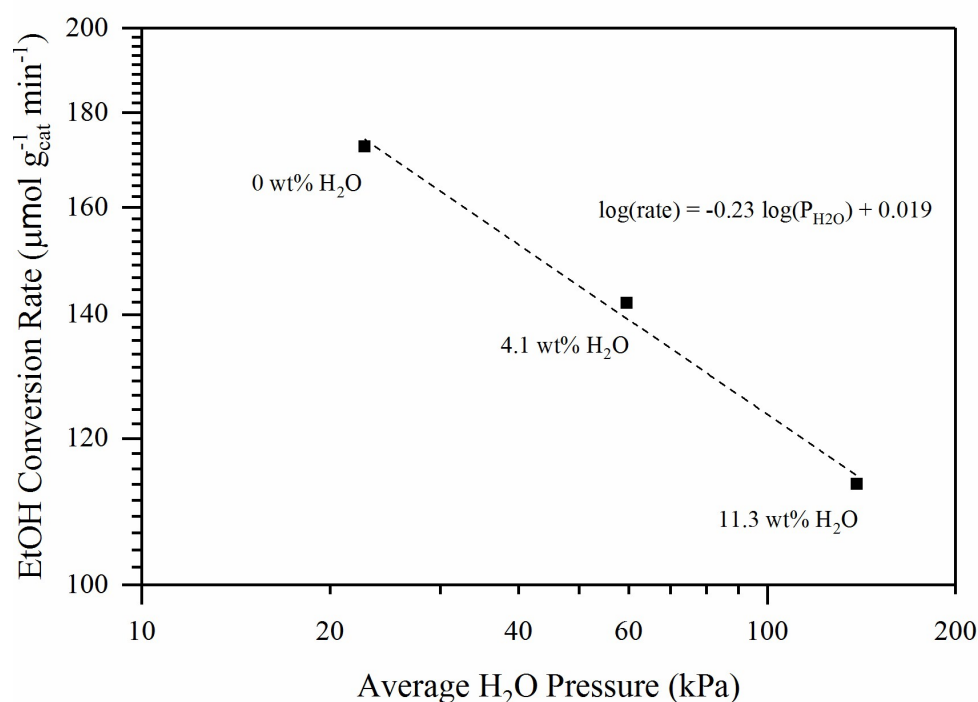


Fig. S4. Ethanol conversion rate vs. the average partial pressure of water across the catalyst bed calculated based upon the observed products and assumed reaction stoichiometries. The log-log plot provides a rate order for water of -0.23 with respect to ethanol conversion.

Transport Calculations:

The possibility that reaction rates were limited by heat or mass transport was examined through evaluation of several transport criteria which must be satisfied to ensure that this is not the case. These criteria have been notably applied and discussed by Shabaker et al. The criteria considered and their evaluations are shown below. Descriptions and approximations for each parameter are also provided. Ethanol condensation to 1-butanol and water was assumed to be the main reaction when one was required for estimation purposes, such as for the absolute heat of reaction. For parameters which were not measured, worst-case approximations were assumed (e.g. a high activation barrier, low particle thermal conductivity, high rate order). **In all cases, the tests were satisfied by multiple orders of magnitude.**

J.W. Shabaker, R.R. Davda, G.W. Huber, R.D. Cortright, J.A. Dumesic, Aqueous-phase reforming of methanol and ethylene glycol over alumina-supported platinum catalysts, *J. Catal.* 215 (2003) 344-352.

Test	Equation	Evaluation
Interphase heat transport	$\frac{q R r_p}{h T_B} < 0.15 \frac{R T_B}{E}$	$3.98 * 10^{-5} \ll 7.46 * 10^{-8}$
Intraparticle heat transport	$\frac{q R r_p^2}{\lambda T_S} < 0.75 \frac{R T_S}{E}$	$3.83 * 10^{-5} \ll 3.73 * 10^{-7}$
Interphase mass transport	$\frac{R r_p^2}{C_b k_c} < \frac{0.15}{n}$	$3.28 * 10^{-8} \ll 7.50 * 10^{-2}$
Intraparticle mass transport	$\frac{R r_p^2}{C_s D_{eff}} < 0.3$	$3.33 * 10^{-4} \ll 3.00 * 10^{-1}$

Parameter	Definition	Approximate Value
q	Absolute heat of reaction	$21,517 \text{ J mol}^{-1} \text{ ethanol}$
R	Volumetric reaction rate	$8.86 \text{ mol m}^{-3} \text{ s}^{-1}$
r_p	Catalyst particle radius	$1.25 * 10^{-4} \text{ m}$
R	Gas constant	$8.314 \text{ J mol}^{-1} \text{ K}^{-1}$
T_B	Bulk temperature	598 K
T_S	Catalyst surface temperature	598 K
h	Heat transfer coefficient	$1000 \text{ W m}^{-2} \text{ K}^{-1}$
E	Activation barrier	$100,000 \text{ J mol}^{-1} \text{ K}^{-1}$
λ	Thermal conductivity of catalyst particle	$0.13 \text{ W m}^{-1} \text{ K}^{-1}$
C_b	Bulk concentration of ethanol	$79.1 \text{ mol ethanol m}^{-3}$
C_s	Ethanol surface concentration	$79.1 \text{ mol ethanol m}^{-3}$
k_c	Surface-bulk mass transfer coefficient	$5.34 * 10^{-2} \text{ m s}^{-1}$
n	Rate order	2
D_{eff}	Effective diffusivity	$5.25 * 10^{-6} \text{ m}^2 \text{ s}^{-1}$