

Figure 2: A and B) The measured frequency behavior of the microfluidic chip. The lines in the graph show the average of 50 measurements obtained with the impedance/gain phase analyzer using LC buffer with or without (non)viable NS-1 cells. The shaded area indicates the measurement frequencies which have been studied and the dashed line represents the frequency used during all subsequent experiments C) Simulation of the frequency response of the real electrical impedance of the equivalent circuit model with viable NS-1 cells, beads (representing non-viable cells) and only LC buffer.

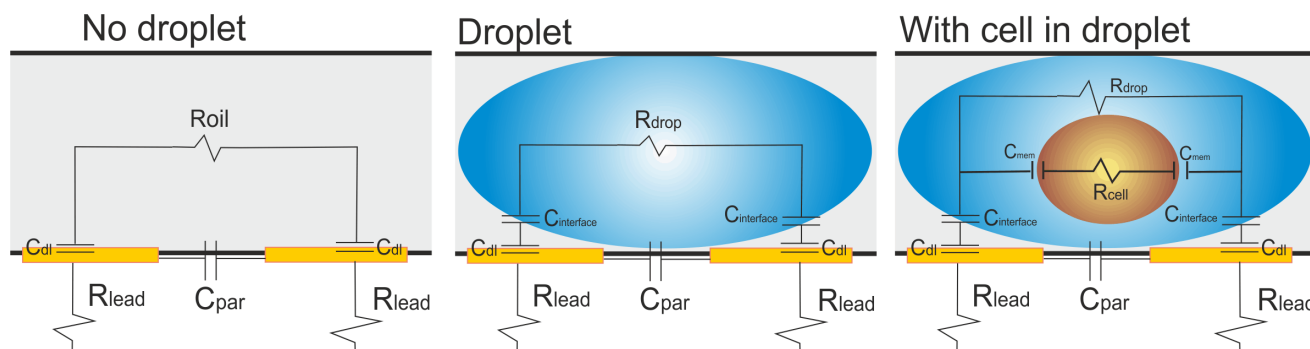


Figure 3: Simplified equivalent circuit model of the microfluidic device w/o droplet, with droplet and with cell in droplet. In all situations, there are two double layer capacitances (C_{dl}), caused by the electrode-fluid interface, a parasitic capacitance (C_{par}) and a lead resistance (R_{lead}). The passage of an empty droplet adds two capacitances to the model and when the droplet contains a cell, an additional circuit for the cell is implemented. This is represented by the addition of two capacitances for the oil-buffer interface at the droplet ($C_{interface}$), a resistance of the droplet fluid (R_{drop}) and an equivalent circuit model for a cell. The capacitances in this simplified model of the cell are the cell membrane (C_{mem}) and the resistance of the cell interior (R_{cell}).

With our device, droplets containing LC buffer or PBS were detected up to 475Hz. NS-1 cells suspended in LC buffer were detected and can be differentiated regarding viability (fig4). Viable NS-1 cells show negative peaks, whereas non-viable cells show positive peaks. Furthermore, polystyrene beads suspended in LC buffer behave similar to non-viable cells (fig4). When a mixture of viable and non-viable NS-1 cells were suspended in PBS, only positive peaks were observed (fig4), of which the height of the individual peak area corresponded to cell size (not shown). Hence, by using LC buffer it is possible to differentiate between viability based on the peak appearances.

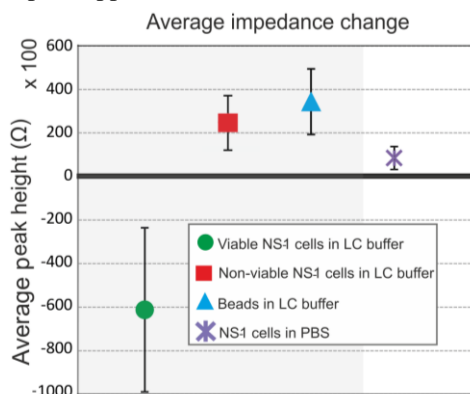


Figure 4: Impedance change of viable ($n=68$) and non-viable NS-1 cells ($n=154$), 11 μm sized beads all in LC buffer ($n=15$) and impedance change of viable and non-viable NS-1 cells in PBS ($n=37$). The shaded area represents data from LC buffer.

Next, cells were encapsulated in LC buffer. Since, the LC buffer is still more conducting than the continuous phase (oil), the impedance signal of empty droplets decreased, resulting in negative peaks. Cell containing droplets generated an increasing negative peak, in the real part of the impedance measurements, compared to empty droplets (fig5), which is in correspondence with our observation. Cell containing droplets can be detected up to a droplet frequency of 60Hz.

Future experiments are focused on increasing the operating frequency to several kilohertz, using a dedicated lock-in-amplifier and discriminate between non-viable and viable cells in LC droplets. Furthermore, we want to detect cells in PBS droplets and perform downstream selection of cell containing droplets.

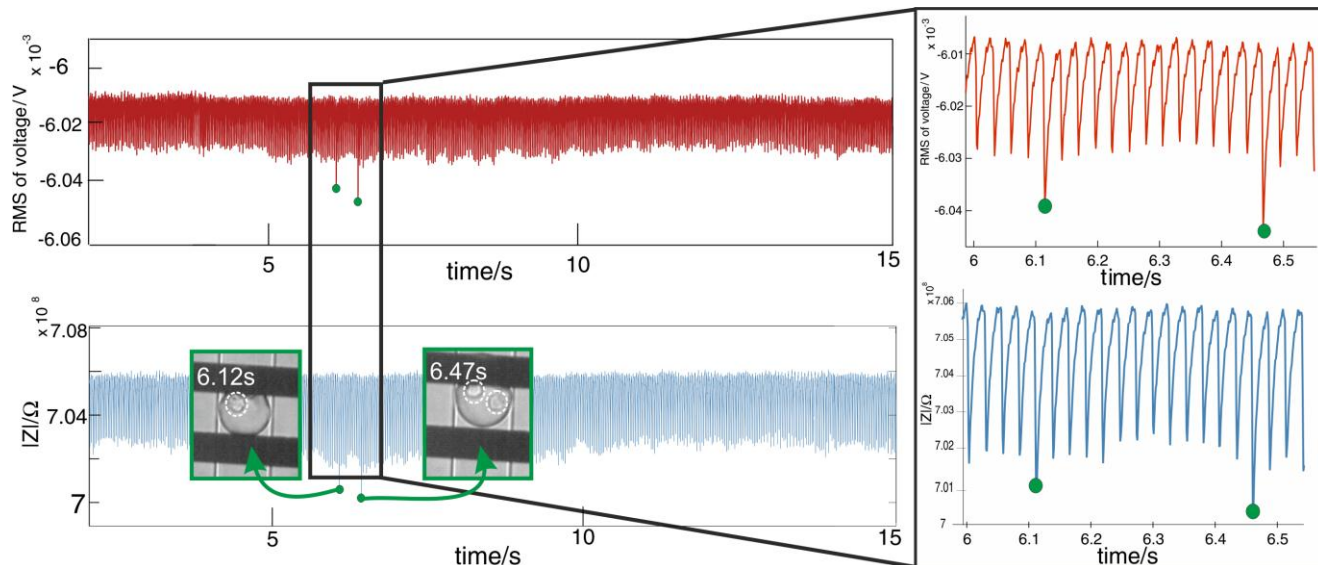


Figure 5: NS-1 cell in droplet detection using RMS voltage signal and the final impedance change. NS-1 cells in LC buffer were detected at a droplet frequency of 40 Hz. $F_{act} = 100\text{kHz}$ sample rate is 899Hz and $6 V_{pp}$.

CONCLUSION

This is the first time that label-free detection of cells in droplets is shown. The device enables us to measure the individual volume, frequency and even content of the droplets. Moreover, cells can be discriminated based on their viability.

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