

RAPID AND ACCURATE IC₅₀ DETERMINATION USING LOGARITHMIC CONCENTRATION GENERATOR

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ABSTRACT

This paper proposes an effective methodology for the determination of the half maximal (50%) inhibitory concentration (IC₅₀) by using microfluidic device that generates logarithmic concentration gradients. Dose-response curve is obtained with respect to the concentrations in a logarithmic scale. Although we have presented a high-throughput analysis of ATP binding cassette transporter (ABC-transporter) by using linear concentration generator [1] and fluorescent substrates [2], logarithmic concentration generator is demanded for rapid and accurate IC₅₀ determination as shown in Fig. 1. We designed a microfluidic device composed of branching micro-channels where samples are divided and mixed to generate designated concentrations. Finally inhibition analysis of substrate transport was conducted by linear and logarithmic concentration generators. We found that logarithmic concentration generators are useful for the accurate determination of IC₅₀ by a fewer number of tests than linear concentration generators.

KEYWORDS

IC₅₀, Microfluidics, Drug screening.

INTRODUCTION

In drug development process, the phenomena that depend on the logarithmic concentration are of great importance for safe and effective use of drugs, such as IC₅₀ that determines the concentration at which the transport of a drug is inhibited by the other one by 50% [3,4,5]. To determine IC₅₀, substrate transport at different concentrations must be evaluated. For the high-throughput IC₅₀ determination, microfluidic concentration gradient generator can be a smart approach [6,7]. Although IC₅₀ can be estimated by using linear gradient generators [1,8], the uneven concentration distribution in the logarithmic scale (Fig. 1(c,d)) causes less accuracy. To accomplish a rapid and accurate determination of IC₅₀, the logarithmic sampling device, which produces an even concentration distribution in the logarithmic scale (Fig. 1(c,d)), is useful and demanded.

In generally, the generation of logarithmic concentrations in the microfluidic devices was completed by a pyramidal network (T-shaped microchannel) [9], serial network [10,11], and combination of serial and volumetric

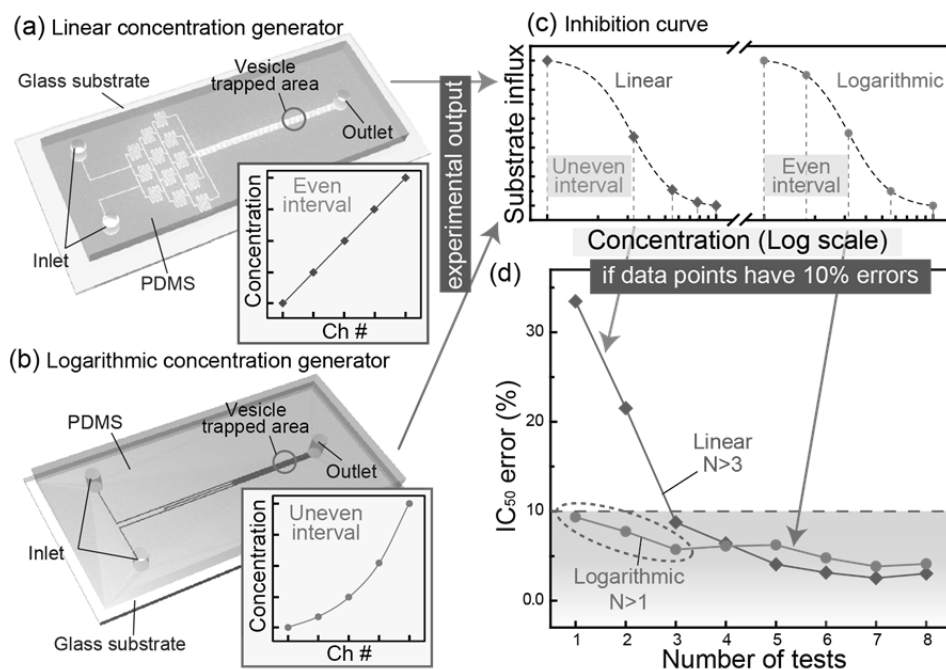


Fig. 1 (a-b) The conceptual illustrations of the (a) linear and (b) logarithmic concentration generator. Inset graphs show the dispersions of generated concentrations in the devices. (c) Examples of linear (blue) and logarithmic (red) concentration samplings that allow the same inhibition curve (dashed line). (d) Simulation of the percentages of IC₅₀ error, which is calculated by giving 10% errors in the sample concentration of each microfluidic channel. In contrast to linear gradient generator (blue), logarithmic gradient device (red) enables low IC₅₀ error in a few experimental tests.

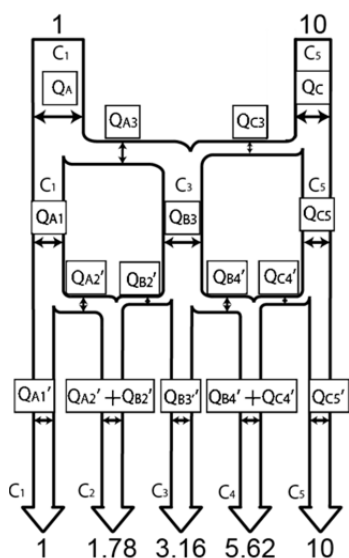


Fig. 2 Schematics of the flow rate distributions to generate the desired concentrations at the 5 outlets. We assumed that the ratio of branched channel width determines the distribution of the flow rate. Q indicates the flow rate and C is the concentration of compounds. The concentrations were expressed as C (1, 2, 3, 4, 5) = 10⁰, 0.25, 0.5, 0.75, 1 μ M.

10^{0.25}, 10^{0.5}, 10^{0.75}, and 10¹. The initial flow rates (Q_A and Q_C), concentrations, and the channel width are the design parameters while the lengths of the channels were set to be long enough to allow complete diffusion-based mixing of the samples. We assumed that the ratio of the branched channel widths determines the distribution of the volumetric flow rate as depicted in Fig. 2. Then, we tried the COMSOL simulation to verify our design principle. As a result, when inlet flow rates (Q_A and Q_C) are 1.0 μ L/min and 0.8 μ L/min, respectively, the desired concentrations at the outlets can be generated.

EXPERIMENT

Our device consists of a polydimethylsiloxane (PDMS) microfluidic channel and a glass substrate. The microfluidic devices were fabricated by conventional soft lithography [15]. The PDMS chip was attached to an aldehyde-coated glass with single-strand DNA tethers using oxygen plasma treatment. To prevent DNA removal at the plasma-exposure step, we placed PDMS masks on the glass [1]. After the device preparation, a cholesterol-modified single-strand DNA (ssDNA) was applied to the channels to form duplexes with the ssDNA tethered to the glass surface. ABC-transporter vesicles were then injected into microfluidic channels to be immobilized [2,16], and incubated with quinidine (inhibitor) and 50 nM Rhodamine123 (Rh123) solutions at different concentrations for 1 hour and 37 °C. Here, the inlet concentrations of quinidine, C_1 and C_5 , were 0.3 and 3.0 μ M, respectively. The fluorescence intensities of ABC transporter vesicles after rinsing with buffer were detected by microscopic images.

RESULT AND DISCUSSION

After device preparation, some experiments were conducted by using Rh123 to verify that our logarithmic device could generate logarithmic concentration gradients. The concentration distributions were estimated by the fluorescence intensity from the channel. The concentration generated in our logarithmic device was well matched with the result of COMSOL simulation (Table 1). Finally, we analyzed the Rh123 transport inhibition with quinidine by linear [1] or logarithmic concentration generator. The IC_{50} was determined by the inhibition curve drawn by the different fluorescence intensity from ABC transporter vesicles. As a result, the IC_{50} values of logarithmic and linear concentration generator were $0.80 \pm 0.01 \mu$ M and $1.06 \pm 0.01 \mu$ M, respectively. Fig. 3 represents that IC_{50} can be determined with less than 10% errors by using logarithmic concentration generator. This result indicates that our

Table 1 Comparison table of the outlet concentrations with desired value, simulation, and experiment. This table shows that simulation and experiment value are agreed well.

	Ch 1	Ch 2	Ch 3	Ch 4	Ch 5
Desired	1.00	1.78	3.16	5.62	10.00
Simulation	1.00	1.69	3.30	8.12	10.00
Experiment	0.98 ± 0.18	1.79 ± 0.25	3.85 ± 0.70	8.18 ± 0.81	10.36 ± 0.24

network [12]. The principle of these network designs can be theoretically formulated considering the flow resistance by analogy with electrical circuits [13]. In microfluidic devices, the mixing ratios of two solutions were controlled by adjusting channel length because the flow resistance is purely proportional to the channel length [14]. Therefore, the conventional logarithmic concentration generators have very long channel, multi-inlets, or 3-dimensionals structure to obtain the desired concentrations and become complicated design.

In this report, we developed the simple and useful microfluidics network design to generate logarithmic concentration gradients by unique approach. To control the flow resistance, the channel widths at each branching point are adjusted. Then, the generation of logarithmic concentration gradients was confirmed by COMSOL simulation and fluorescence images in the device. Finally, taking advantage of our previous study [1,2], we performed the IC_{50} assays using ATP-binding cassette transporter (ABC transporter) vesicles. As a result, we found that our logarithmic concentration devices were succeeded in the rapid and accurate IC_{50} determination by a fewer number of tests than linear concentration devices.

DESIGN PRINCIPLE

We designed a simple logarithmic concentration generator (Fig. 2) that produces concentrations of 10⁰,

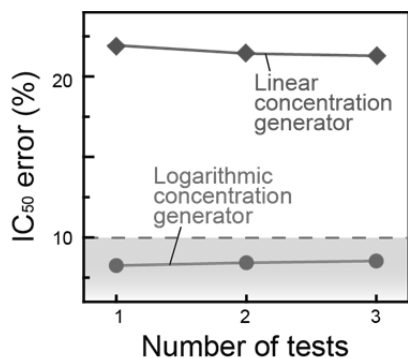


Fig. 3 IC₅₀ error of two devices. The percentages were calculated from the each experimental value.

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logarithmic sampling device is readily applicable for the accurate determination of the IC₅₀ by ABC transporters.

CONCLUSION

In this study, we developed the platform for the rapid and accurate IC₅₀ determination by logarithmic concentration gradient generator. We believe that our approach would accelerate a high-throughput drug screening using MEMS technology.

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