

Paper B800104A

Improving the Linearity of Spectroscopic Data Subjected to Fluctuations in External Variables by the Extended Loading Space Standardization

1) Spectral Standardization using LSS

Assume the rows of $\mathbf{X}_{I \times J}(t_1)$, $\mathbf{X}_{I \times J}(t_2)$, ..., and $\mathbf{X}_{I \times J}(t_N)$ are the corresponding spectra for the same I training mixture samples measured at training temperatures $t_1, t_2, \dots, t_N$ (I and J are the number of samples and discrete wavelength positions, respectively).

Suppose $\bar{\mathbf{X}} = \sum_{n=1}^N \mathbf{X}_{I \times J}(t_n) / N$, the singular value decomposition of $\bar{\mathbf{X}}$ can be expressed as:

$$\bar{\mathbf{X}} = [\mathbf{U}_c, \mathbf{U}_r] \begin{bmatrix} \Lambda_c^{1/2} & \\ & \Lambda_r^{1/2} \end{bmatrix} [\mathbf{V}_c, \mathbf{V}_r]' = \mathbf{T}_c \mathbf{P}_c + \mathbf{T}_r \mathbf{P}_r \quad (1)$$

$$\mathbf{T}_c = \mathbf{U}_c \Lambda_c^{1/2}, \quad \mathbf{T}_r = \mathbf{U}_r \Lambda_r^{1/2}, \quad \mathbf{P}_c = \mathbf{V}_c', \quad \mathbf{P}_r = \mathbf{V}_r' \quad (2)$$

Where the subscripts 'c' and 'r' signify the first C principal factors representing the spectral information and the rest factors representing noise, respectively. Superscript "'" denotes the transpose. Assuming Beer's law is valid, then $\bar{\mathbf{X}} = \bar{\mathbf{Y}}\bar{\mathbf{S}} + \mathbf{E}$ (where $\mathbf{Y}$ denotes the concentration matrix; $\bar{\mathbf{S}} = \sum_{n=1}^N \mathbf{S}(t_n) / N$ are the mean of the pure spectra matrices that are not available for grey chemical

systems; and $\mathbf{E}$ is the matrix of residuals). It can be proven that there exists a full rank matrix $\mathbf{R}$ that satisfies equation 3:

$$\mathbf{Y} = \mathbf{T}_c \mathbf{R} \quad (3)$$

Therefore, the following equation holds:

$$\mathbf{X}(t_n) = \mathbf{Y}\mathbf{S}(t_n) + \mathbf{E}(t_n) = \mathbf{T}_c \mathbf{R} \mathbf{S}(t_n) + \mathbf{E}(t_n) \quad (4)$$

Letting $\mathbf{P}(t_n) = \mathbf{R} \mathbf{S}(t_n)$ (matrix $\mathbf{P}(t_n)$ has a size of $C \times J$, where C is the number of principal components representing spectral information):

$$\mathbf{P}(t_n) = \mathbf{R} \mathbf{S}(t_n) \approx (\mathbf{T}_c)^+ \mathbf{X}(t_n), \quad n = 1, 2, \dots, N \quad (5)$$

Here, superscript '+' denotes the Moore-Penrose Matrix Inverse.

In order to model the temperature effects on loading matrixes, a polynomial can be fitted to each element of $\mathbf{P}(t_n)$ ($n = 1, 2, \dots, N$) against the temperature t_n :

$$p_{i,j}(t_n) = \alpha_{i,j} + \beta_{i,j} t_n + \gamma_{i,j} t_n^2, \quad i = 1, 2, \dots, C, \quad j = 1, 2, \dots, J, \quad n = 1, 2, \dots, N \quad (6)$$

Parameters $\alpha_{i,j}$, $\beta_{i,j}$ and $\gamma_{i,j}$ can be estimated out as follows:

$$\mathbf{p} = \mathbf{M} \mathbf{A} \quad (7)$$

$$\mathbf{p} = [p_{i,j}(t_1); \dots; p_{i,j}(t_n); \dots; p_{i,j}(t_N)], \quad \mathbf{t} = [t_1; \dots; t_n; \dots; t_N], \quad \mathbf{M} = [\mathbf{1}, \mathbf{t}, \mathbf{t}^2], \quad \mathbf{A} = [\alpha_{i,j}; \beta_{i,j}; \gamma_{i,j}]$$

Here, the regressor matrix $\mathbf{M}$ is known and expected to have full column rank, the parameter matrices $\mathbf{A}$ can then be simply calculated out as $\mathbf{A} = (\mathbf{M}' \mathbf{M})^{-1} \mathbf{M}' \mathbf{p}$.

The above procedure can be applied to all the elements of loading matrices $\mathbf{P}(t_n)$ ($n = 1, 2, \dots, N$). After all the parameters $\alpha_{i,j}$, $\beta_{i,j}$ and $\gamma_{i,j}$ ($i=1,2,\dots,C$, $j=1,2,\dots,J$) have been estimated out, the loading matrix $\mathbf{P}(t)$ at any temperature t ($t_1 \leq t \leq t_N$) (which should be measured along with the spectrum of the sample) can be calculated out as: $p_{i,j}(t) = \alpha_{i,j} + \beta_{i,j}t + \gamma_{i,j}t^2$

For a spectrum $\mathbf{x}(t)$ measured at temperature t , it can then be standardized into an arbitrarily selected reference temperature t_{ref} ($t_1 \leq t_{ref} \leq t_K$) as if it were measured under the reference temperature:

$$p_{i,j}(t_{ref}) = \alpha_{i,j} + \beta_{i,j}t_{ref} + \gamma_{i,j}t_{ref}^2, \quad \mathbf{z}(t_{ref}) = \mathbf{x}(t)\mathbf{P}(t)^+ (\mathbf{P}(t_{ref}) - \mathbf{P}(t)) + \mathbf{x}(t) \quad (8)$$

Where $\mathbf{z}(t_{ref})$ denotes the standardized spectrum.

2) MATLAB code for the estimation of multiplicative parameters by OPLEC

```
% [b] = OPLEC(Z, y, CompNumb);
% This is an m-file to find the multiplicative scattering parameter vector b for calibration samples;
% Z contains z_i in its rows; z_i (i=1,2,...,m) are the standardized spectra of calibration samples.
% y is the concentration vector of the target chemical component in calibration samples;
% CompNumb is the number of chemical components in mixture samples;
% b is a vector containing the multiplicative scattering parameters for calibration samples;
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```
function [b]=OPLEC(Z,y,CompNumb);
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```
[m,n]=size(Z);
Y=[ones(m,1),y];
b=zeros(m,m);
```

```
for i=1:m
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```
    OriginalPositionIndex=(1:m)';
    Z1=Z(i,:);
    PositionIndex=i;
```

```
    for j=1:(CompNumb-1)
        NormVect=sqrt(sum(Z.^2,2));
        ResMatrix=diag(1./NormVect)*Z*(eye(n,n)-pinv(Z1)*Z1);
        ResVect=diag(ResMatrix*ResMatrix');
```

```

[MaxRes,MaxPosition]=max(ResVect);
Z1=[Z1;Z(MaxPosition,:)];
PositionIndex=[PositionIndex,MaxPosition];

end

OriginalPositionIndex(PositionIndex)=[];

ZZ=Z;
ZZ(PositionIndex,:)=[];
Z2=ZZ;

Y11=Y(PositionIndex,1);
Y21=Y(PositionIndex,2);
YY=Y;
YY(PositionIndex,:)=[];
Y12=YY(:,1);
Y22=YY(:,2);

Regv=Z2*pinv(Z1);
P1=diag(Y22)*Regv*diag(Y11);
P2=Regv*diag(Y21);
P11=P1(:,1);
P12=P1(:,2:CompNumb);
P21=P2(:,1);
P22=P2(:,2:CompNumb);

b0=lsqnonneg(P12-P22,P21-P11);
b1=[1;b0];

Q1=Regv*diag(Y11);
Q2=Regv*diag(Y21);
b2=diag(1./(Y12+Y22))*(Q1+Q2)*b1;

b(PositionIndex,i)=b1;
b(OriginalPositionIndex,i)=b2;

end

b=mean(b,2);

% After obtaining the model parameter vector b for calibration samples, two calibration models are
built by standard PLS toolbox. One is between the concentration vector (y) of the target

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chemical component and the spectral data $\mathbf{Z}$, the other is between $\text{diag}(\mathbf{y})\mathbf{b}$ and $\mathbf{Z}$. The multiplicative effect on the test sample can then be corrected through dividing the prediction of the second calibration model by the prediction of the first calibration model.