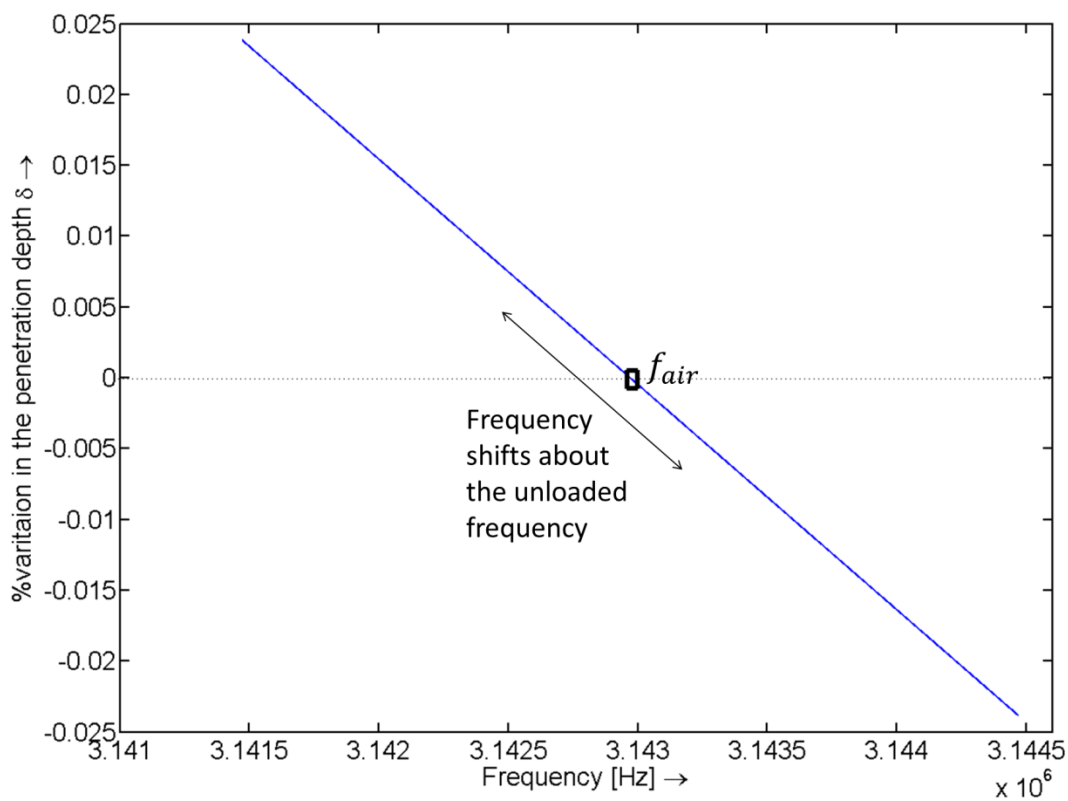


## Supplementary Material

### A.1 Relationship between penetration depth and resonance frequency



$$\frac{\delta_L - \delta_{air}}{\delta_{air}} * 100 = \left( \sqrt{\frac{f_{air}}{f_{air} + \delta f}} - 1 \right) * 100$$

For the given  $f_{air} = 3142969 \text{ Hz}$ , if we assume that the  $\Delta f = \pm 1500 \text{ Hz}$ , then the variation in the penetration depth  $\delta_L (= 318.5 \text{ nm})$  is within 0.025% and insignificant.

### A.2 Mass and volume calculations

$$\delta_L = \text{penetration depth (constant)} [m] = 0.32 * 10^{-6}$$

$$r_c = \text{contact radius} [m]$$

$$L = \text{side - length of the resonator} [m] = 1400 * 10^{-6}$$

$$r_s = \text{radius of the spherical cap} [m]$$

$$V_c = \text{volume of the thin shear layer of liquid} [m^3]$$

$$V_s = \text{volume of the spherical cap (droplet)} [m^3]$$

$$m_c = \text{mass of the thin liquid layer} [kg]$$

$$m_s = \text{mass of the droplet} [kg]$$

$$H = \text{height of the droplet} [m]$$

$$d_L = \text{density of water} [kgm^{-3}] = 1000$$

$$\theta = \text{contact angle} [deg] = 48.85^\circ$$

For a spherical cap geometry:

$$r_s = \frac{r_c}{\sin \theta}$$

$$V_c = \pi r_c^2 \delta_L$$

$$m_c = V_c d_L$$

$$H = r_s (1 - \cos \theta)$$

$$V_s = \frac{\pi}{6} H (3r_c^2 + H^2)$$

$$m_s = V_s d_L$$

Case 1: Maximum contact radius

$$r_c = \frac{L}{2} = 700 * 10^{-6} [m]$$

$$V_c = 4.92 * 10^{-13} [m^3] \text{ or } 0.492 \text{ nL}, m_c = 4.92 * 10^{-10} [kg] \text{ or } 492 \text{ ng}$$

$$r_s = 929 * 10^{-6}, H = 318 * 10^{-6}, V_s = 4.48 * 10^{-10} [m^3] \text{ or } 448 \text{ nL}, m_s = 4.48 * 10^{-7} [kg] \text{ or } 448 \mu g$$

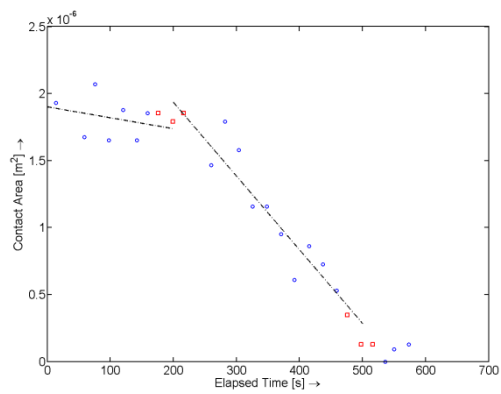
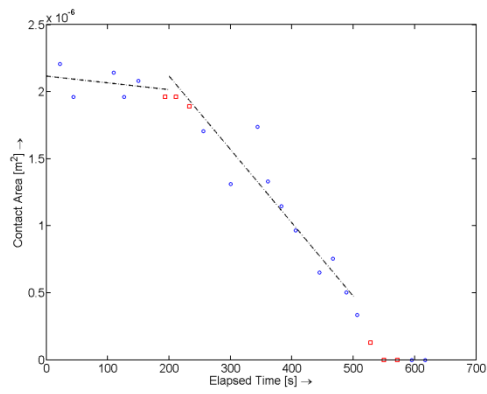
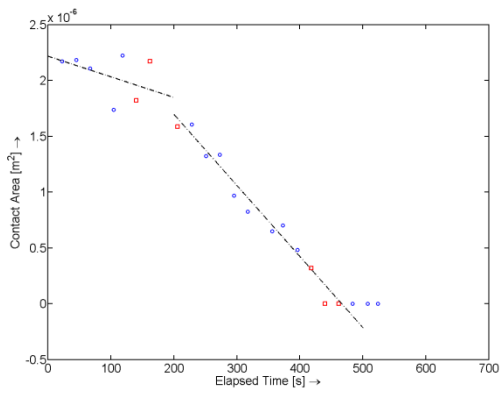
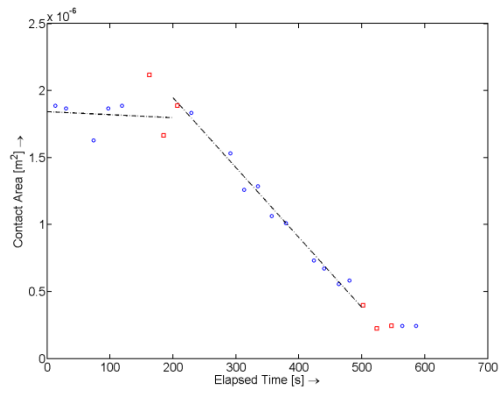
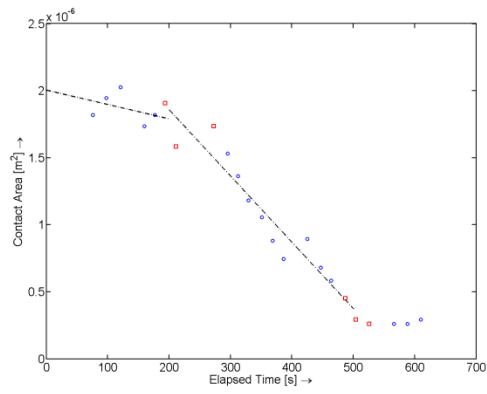
Case 2: Minimum observed radius from the microscope

$$r_c = 250 * 10^{-6}$$

$$V_c = 6.28 * 10^{-14} [m^3] \text{ or } 0.062 \text{ nL}, m_c = 6.28 * 10^{-11} [kg] \text{ or } 62.8 \text{ ng}$$

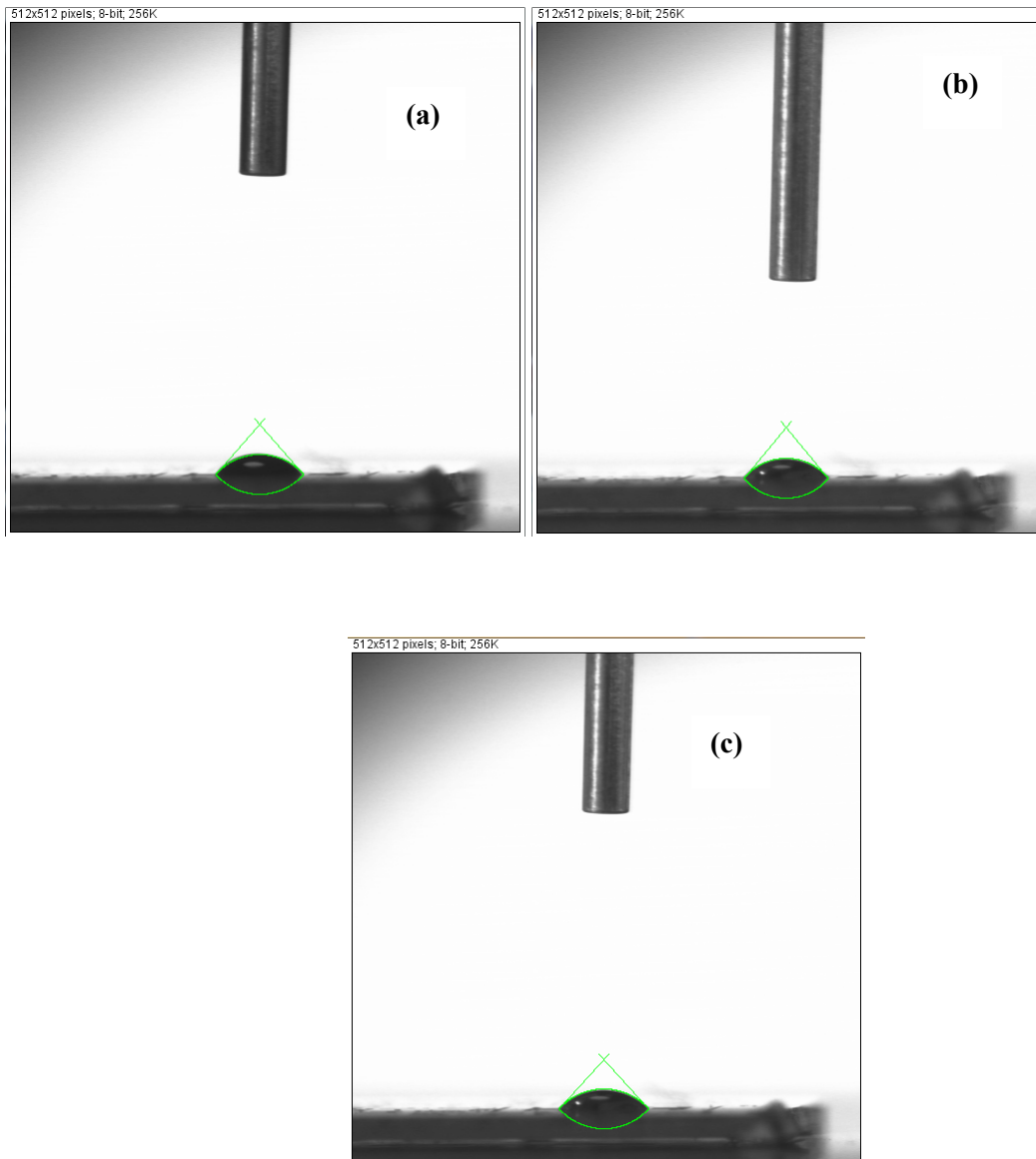
$$r_s = 332 * 10^{-6}, H = 113.5 * 10^{-6}, V_s = 2.04 * 10^{-11} [m^3] \text{ or } 20.4 \text{ nL}, m_s = 2.04 * 10^{-8} [kg] \text{ or } 20.4 \mu g$$

### A.3 Individual fitting of contact area plots



While linear fitting, transition points/corner points (red squares) are ignored

#### A.4 Contact angle measurements



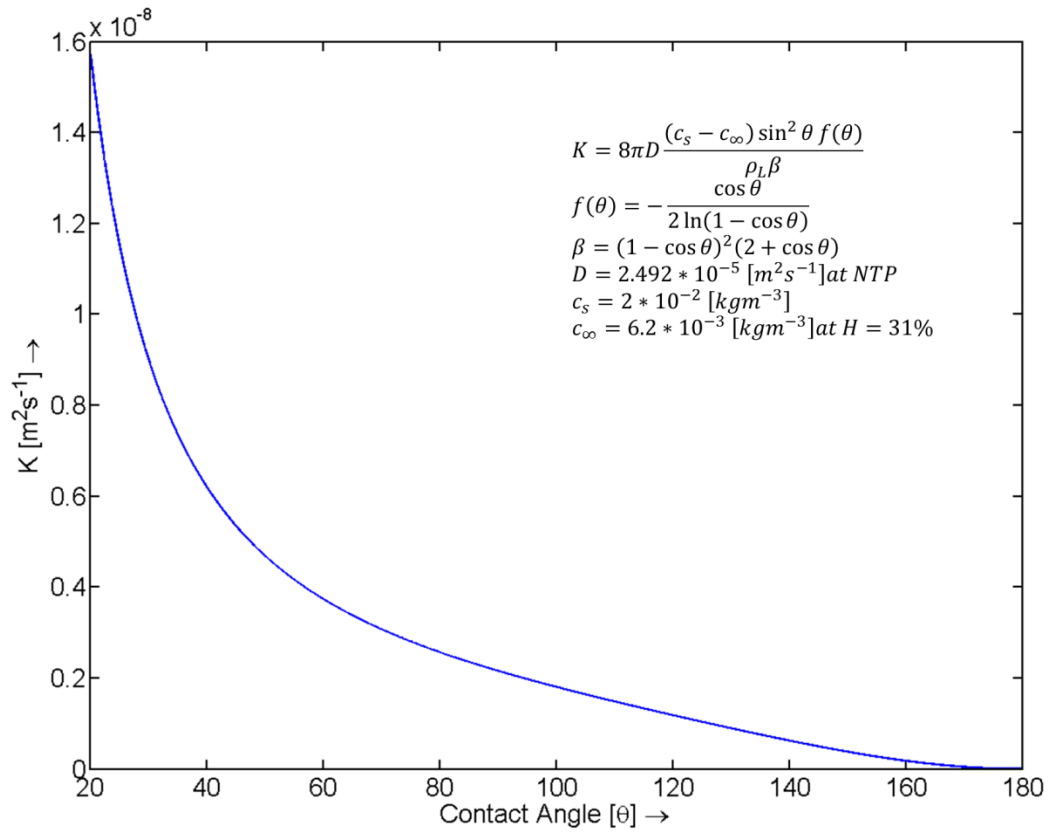
To determine receding contact angles for the device, CAM200 (KSV NIMA) Goniometer instrument was used. To extract CA values from the images, ‘drop\_analysis’<sup>1</sup> ImageJ plug-in was used. Low-bond Axisymmetric Drop shape analysis (LBADSA) option was used which involves optimizing the shape of the fitting spherical cap (green) so that it completely encloses the droplet.

$$CA_{avg} = \frac{CA_a + CA_b + CA_c}{3}$$

$$CA_{avg} = \frac{48.232^\circ + 50.52^\circ + 47.811^\circ}{3} = 48.854^\circ$$

#### A.5 Relationship of K vs. contact angle

<sup>1</sup> [http://mmrc.caltech.edu/Gniometeer/drop\\_analysis/drop\\_analysis.pdf](http://mmrc.caltech.edu/Gniometeer/drop_analysis/drop_analysis.pdf)



As the CA decreases (more hydrophilic), value of K increases rapidly. From the figure, it is clear that this rate is relatively smaller for hydrophobic cases.