Electronic supporting Information

A vanadium(IV) pyrazolate metal organic polyhedron with permanent porosity and adsorption selectivity

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Experimental Section

Materials and methods

All materials including solvents were obtained from commercial sources, were of reagent grade and were used without further purification. Infrared (IR) spectra were acquired in transmission mode on a ATR unit (Diamond) spectrometer. Elemental analyses were carried out on a METTLER M-3Analyzer. EPR spectra were acquired in Bruker ELEXSYS E500 CW-EPR spectrometer. Microwaves frequencies: X-band (about 9.5 GHz with Frequency counter E 41 FC). Thermogravimetric analyses (TGA) were performed, under either nitrogen or a reactive air atmosphere, on a Shimadzu-TGA-50H equipment, at a heating rate of 20 °C min⁻¹. X-ray Powder Diffraction Structural Analysis (XRPD): except for the structural analysis, all the X-ray powder diffraction data were acquired on a D2 PHASER Bruker AXS diffractometer using CuK α radiation ($\lambda = 1.5418$ Å). X-ray Crystallography: the crystal structure of 1 was measured at room temperature on a Bruker Apex instrument using $\lambda MoK\alpha = 0.71073$ Å radiation, for details see Table S1. Gas Adsorption Measurements conventional adsorption isotherms were measured using a Micromeritics Tristar 3000 volumetric instrument under continuous adsorption conditions. Brunauer-Emmet-Teller (BET) and Langmuir analyses were carried out to determine the total specific surface areas for the N₂ isotherms at 77 K. In addition, CO₂ isotherms at 273 K were measured to evaluate the micropore region by means of the Dubinin-Radushkevich equation (Table 2). Prior to measurement, powdered samples were heated at 453 K for 12 h and outgassed to 10-6 Torr. Dynamic Gas Adsorption experiments: A 15 cm long glass tube with an inner diameter of 5 mm was packed with 0.35 g of 1 and subsequently was activated under a pure He flow (20 mL min⁻¹) at 423 K for 24 h and then used for evaluating the CO_2/N_2 separation performances of the materials. The desired gas mixture (10 mL min⁻¹) was prepared via mass flow controllers. For instance, CO₂/N₂ (0.14:0.86) mixtures were prepared to simulate the emission of flue gas from a power plant employing 1.4 mL min⁻¹ of CO₂ and 8.6 mL min⁻¹ of N₂ flows, and the breakthrough experiments were carried out at 273, K by step changes from He to CO_2/N_2 flow mixtures. In the case of cyclohexane/benzene separation a mixture of cyclohexane (2 μ L)/benzene (2 μ L)/methane (0.1 mL) was injected into a pure He flow (20 mL min⁻¹) and the mixture elution was analyzed by means of a Mass Spectrometer (Omnistar). The interaction of methane was considered negligible and taken as reference.

Synthesis of ligand

The 1,4-bis(1*H*-pyrazol-4-yl)benzene ligand (H_2BDP) was prepared as described in the literature.¹

Synthesis of [V₃(µ³-O)O(OH)₂(BPD)_{1,5}(HCOO)₃] 1

A mixture of VCl₃ (200 mg, 1.27 mmol) and 1.4-bi(1Hpyrazol-4-yl)benzene (134 mg, 0.64 mmol) in DMF (10 mL) was placed in a teflon line (20 mL), heated to 150 °C and held at this temperature for 24 h as shown in Scheme S1. The reaction mixture was slowly cooled to obtain a brown crystalline solid. The product was filtered, washed with DMF (2×5 mL), and dried in air vield 1 (190)44 %). to mg, Calc. for V₃O₂(OH)₂(C₁₂H₈N₄)_{1.5}(HCOO)₃(H₂O)₂(C₃NH₇O)_{1.5} C **37.72**, H **3.91**, N **12.93**; found C 37.72, H 3.78, N 12.97. FT-IR (ATR): 1647 (s), 1596 (vs), 1577 (vs), 1488 (w), 1429 (w), 1361 (vs), 1242 (m), 1173 (w), 1115 (m), 1038 (s), 1003 (w), 952 (m), 838 (s), 761 (m), 694 (m), 645 (m), 602 (m), 539 (m), 510 (vs), 423 (s) cm⁻¹.



[V₃(µ³-O)O(OH)₂(BPD)_{1,5}(HCOO)₃]

Scheme S1.



Fig. S1. IR-ATR spectra of H_2BDP spacer (doted line) and of as synthetized 1 (solid line).



Fig. S2. X-band EPR spectrum of solid sample of 1 at 295 K.



Fig. S3. X-ray powder patterns of 1: simulated from single crystal analysis (**black**), assynthesized (**blue**) and after activation (**red**)



Fig. S4. TG analysis of as-synthesized 1 in air.



Fig. S5. XPRD after activation and after separation

Table S1. Summary of crystal data, data collection and structural refinement parameters for 1

Parameters	[V ₃ (µ ³ -O)O(OH) ₂ (BPD) _{1,5} (HCOO) ₃]
Empirical formula	$C_{84}H_{68}N_{24}O_{40}V_{12}$
Formula weight (M)	2664.87
Temperature, T (K)	100(2)
Wavelength, Mo Ka (Å)	0.71069
Crystal sys tem	Cubic
Space group	<i>I-43m</i>
<i>a</i> (Å)	20.084(5)
<i>b</i> (Å)	20.084(5)
c (Å)	20.084(5)
α (°)	90.000(5)
β (°)	90.000(5)
γ (°)	90.000(5)
Volume, $V(Å^3)$	8101(3)
Ζ	2
Calculated density, ρ (mg m ⁻³)	1.084
Absorption coefficient, μ (mm ⁻¹)	0.720
F(000)	2632
Crystal size (mm ³)	0.1 x 0.1 x 0.1
Index ranges	$-16 \le h \le 16, -16 \le k \le 15, -16 \le l \le 16$
Independent reflections	9445
Data/restraints/parameters	497/0/68
Goodness-of-fit on F ²	1.250
Final <i>R</i> indices $[I > 2\sigma(I)]$	0.0683
<i>R</i> indices (all data)	0.0744
Largest diff. peak and hole (e Å ⁻³)	0.257/-0.300

Bond lengths	(Å)	Bond angles	(°)
V(1) - N(1)	2.08(1)	O(1) -V(1) - O(3)	91.1(4)
V(1) – O(3)	2.041(8)	O(1) -V(1) -O(3)	91.1(4)
V(1) – O(1)	1.93(1)	O(3) -V(1) -O(3)	88.3(5)
V(1) – O(2)	2.11(1)	O(1) -V(1) -N(1)	87.5(5)
V(1) - N(1)	2.08(1)	O(3) -V(1) -N(1)	176.7(4)
V(1) – O(3)	2.041(8)	O(3) -V(1) -N(1)	88.7(3)
C(2) - C(3)	1.51(2)	O(1) -V(1) -N(1)	87.5(5)
C(2) - C(1)	1.34(2)	O(3) -V(1) -N(1)	88.7(3)
C(2) - C(1)	1.34(2)	O(3) -V(1) -N(1)	176.7(4)
C(3) - C(4)	1.33(2)	N(1) -V(1) -N(1)	94.1(5)
C(3) - C(4)	1.33(2)	O(1) -V(1) -O(2)	176.5(6)
C(4) - H(3)	0.93	O(3) -V(1) -O(2)	91.4(3)
C(4) - C(4)	1.41(2)	O(3) -V(1) -O(2)	91.4(3)
N(1) - C(1)	1.35(2)	N(1) -V(1) -O(2)	90.1(4)
N(1) - N(1)	1.39(1)	N(1) -V(1) -O(2)	90.1(4)
C(1) - H(1)	0.93	C(1) –C(2) –C(1)	105.7(17)
C(5) - O(3)	1.26(2)	C(1) –C(2) –C(3)	127.1(9)
C(5) - O(3)	1.26(2)	C(1) –C(2) –C(3)	127.1(9)
O(1) – V(1)	1.93(1)	C(4) -C(3) -C(4)	115.7(17)
O(1) – V(1)	1.93(1)	C(4) –C(3) –C(2)	122.1(8)
C(4) – H(3)	0.93	C(4) –C(3) –C(2)	122.1(8)
C(4) - C(4)	1.41(2)	C(3) –C(4) –C(4)	122.1(8)
N(1) – C(1)	1.35(2)	C(1) –N(1) –N(1)	106.1(7)

Table S2. Bond length (Å) and bond angles (°) for 1

N(1) - V(1) $2.08(1)$ $C(1) -N(1) -V(1)$ $136.0(9)$ $C(1) - H(1)$ 0.93 $N(1) -N(1) -V(1)$ $117.8(3)$ $C(2) - C(3)$ $1.51(2)$ $C(2) -C(1) -N(1)$ $111.0(13)$ $C(2) - C(1)$ $1.34(2)$ $O(3) -C(5) -O(3)$ $124.5(18)$ $C(2) - C(1)$ $1.34(2)$ $C(5) -O(3) -V(1)$ $133.1(11)$ $C(3) - C(4)$ $1.33(2)$ $V(1) -O(1) -V(1)$ $118.88(18)$ $C(3) - C(4)$ $1.33(2)$ $V(1) -O(1) -V(1)$ $118.88(18)$ $C(4) - H(3)$ 0.93 $V(1) -O(1) -V(1)$ $118.88(18)$ $N(1) - C(1)$ $1.35(2)$ $O(1) -V(1) -O(3)$ $91.1(4)$ $N(1) - N(1)$ $1.39(1)$ $O(1) -V(1) -O(3)$ $91.1(4)$ $N(1) - N(1)$ $1.39(1)$ $O(1) -V(1) -O(3)$ $88.3(5)$ $C(1) - H(1)$ 0.93 $O(1) -V(1) -N(1)$ $87.5(5)$ $C(4) - H(3)$ 0.93 $O(3) -V(1) -N(1)$ $87.5(5)$ $C(4) - H(3)$ 0.93 $O(3) -V(1) -N(1)$ $87.5(5)$ $C(1) - H(1)$ 0.93 $O(3) -V(1) -N(1)$ $87.5(5)$ $V(1) - O(3)$ $2.041(8)$ $N(1) -V(1) -N(1)$ $94.1($	N(1) - V(1)	2.08(1)	O(1) $N(1)$ $V(1)$	12(0(0)
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		2.00(1)	C(1) - N(1) - V(1)	136.0(9)
C(2) - C(3) $1.51(2)$ $C(2) -C(1) -N(1)$ $111.0(13)$ $C(2) - C(1)$ $1.34(2)$ $O(3) -C(5) -O(3)$ $124.5(18)$ $C(2) - C(1)$ $1.34(2)$ $C(5) -O(3) -V(1)$ $133.1(11)$ $C(3) - C(4)$ $1.33(2)$ $V(1) -O(1) -V(1)$ $118.88(18)$ $C(3) - C(4)$ $1.33(2)$ $V(1) -O(1) -V(1)$ $118.88(18)$ $C(3) - C(4)$ $1.33(2)$ $V(1) -O(1) -V(1)$ $118.88(18)$ $C(4) - H(3)$ 0.93 $V(1) -O(1) -V(1)$ $118.88(18)$ $N(1) - C(1)$ $1.35(2)$ $O(1) -V(1) -O(3)$ $91.1(4)$ $N(1) - N(1)$ $1.39(1)$ $O(1) -V(1) -O(3)$ $91.1(4)$ $N(1) - N(1)$ $2.08(1)$ $O(3) -V(1) -O(3)$ $88.3(5)$ $C(1) - H(1)$ 0.93 $O(3) -V(1) -N(1)$ $87.5(5)$ $C(4) - H(3)$ 0.93 $O(3) -V(1) -N(1)$ $87.5(5)$ $C(4) - H(3)$ 0.93 $O(3) -V(1) -N(1)$ $87.5(5)$ $C(1) - H(1)$ 0.93 $O(3) -V(1) -N(1)$ $87.5(5)$ $V(1) - O(3)$ $2.041(8)$ $N(1) -V(1) -N(1)$ $91.4(3)$ $V(1) - O(2)$ $2.11(1)$ $O(3) -V(1) -O(2)$ 9	C(1) - H(1)	0.93	N(1) -N(1) -V(1)	117.8(3)
$\begin{array}{c ccccc} C(2) - C(1) & 1.34(2) & O(3) - C(5) - O(3) & 124.5(18) \\ \hline C(2) - C(1) & 1.34(2) & C(5) - O(3) - V(1) & 133.1(11) \\ \hline C(3) - C(4) & 1.33(2) & V(1) - O(1) - V(1) & 118.88(18) \\ \hline C(3) - C(4) & 1.33(2) & V(1) - O(1) - V(1) & 118.88(18) \\ \hline C(4) - H(3) & 0.93 & V(1) - O(1) - V(1) & 118.88(18) \\ \hline C(4) - H(3) & 0.93 & V(1) - O(1) - V(1) & 118.88(18) \\ \hline N(1) - C(1) & 1.35(2) & O(1) - V(1) - O(3) & 91.1(4) \\ \hline N(1) - N(1) & 1.39(1) & O(1) - V(1) - O(3) & 91.1(4) \\ \hline N(1) - V(1) & 2.08(1) & O(3) - V(1) - O(3) & 88.3(5) \\ \hline C(1) - H(1) & 0.93 & O(1) - V(1) - N(1) & 87.5(5) \\ \hline C(4) - H(3) & 0.93 & O(3) - V(1) - N(1) & 87.5(5) \\ \hline C(4) - H(3) & 0.93 & O(3) - V(1) - N(1) & 88.7(3) \\ \hline N(1) - V(1) & 2.08(1) & O(1) - V(1) - N(1) & 88.7(3) \\ \hline N(1) - V(1) & 2.08(1) & O(1) - V(1) - N(1) & 88.7(3) \\ \hline O(3) - V(1) & 2.041(8) & O(3) - V(1) - N(1) & 88.7(3) \\ \hline O(3) - V(1) & 2.041(8) & O(3) - V(1) - N(1) & 94.1(5) \\ \hline V(1) - O(3) & 2.041(8) & N(1) - V(1) - O(2) & 91.4(3) \\ \hline V(1) - O(2) & 2.11(1) & O(3) - V(1) - O(2) & 91.4(3) \\ \hline V(1) - O(3) & 2.041(8) & N(1) - V(1) - O(2) & 91.4(3) \\ \hline V(1) - O(3) & 2.041(8) & N(1) - V(1) - O(2) & 90.1(4) \\ \hline C(5) - O(3) & 1.26(2) & N(1) - V(1) - O(2) & 90.1(4) \\ \hline C(5) - O(3) & 1.26(2) & C(1) - C(2) - C(3) & 127.1(9) \\ \hline O(1) - V(1) & 1.93(1) & C(1) - C(2) - C(3) & 127.1(9) \\ \hline O(1) - V(1) & 1.93(1) & C(1) - C(2) - C(3) & 127.1(9) \\ \hline O(1) - V(1) & 1.93(1) & C(1) - C(2) - C(3) & 127.1(9) \\ \hline O(1) - V(1) & 1.93(1) & C(1) - C(2) - C(3) & 127.1(9) \\ \hline O(1) - V(1) & 1.93(1) & C(1) - C(2) - C(3) & 127.1(9) \\ \hline O(1) - V(1) & 1.93(1) & C(1) - C(2) - C(3) & 127.1(9) \\ \hline O(1) - V(1) & 1.93(1) & C(1) - C(2) - C(3) & 127.1(9) \\ \hline O(1) - V(1) & 1.93(1) & C(1) - C(2) - C(3) & 127.1(9) \\ \hline O(1) - V(1) & 1.93(1) & C(1) - C(2) - C(3) & 127.1(9) \\ \hline O(1) - V(1) & 1.93(1) & C(1) - C(2) - C(3) & 127.1(9) \\ \hline O(1) - V(1) & 1.93(1) & C(1) - C(2) - C(3) & 127.1(9) \\ \hline O(1) - V(1) & 1.93(1) & C(1) - C(2) - C(3) & 127.1(9) \\ \hline O(1) - V(1) & 1.93(1) & C(1) - C(2) - C(3) & 127.1(9) \\ \hline O(1) - V(1) & 1.93$	C(2) - C(3)	1.51(2)	C(2) –C(1) –N(1)	111.0(13)
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	C(2) - C(1)	1.34(2)	O(3) -C(5) -O(3)	124.5(18)
$\begin{array}{c ccccc} C(3)-C(4) & 1.33(2) & V(1)-O(1)-V(1) & 118.88(18)\\ \hline C(3)-C(4) & 1.33(2) & V(1)-O(1)-V(1) & 118.88(18)\\ \hline C(4)-H(3) & 0.93 & V(1)-O(1)-V(1) & 118.88(18)\\ \hline N(1)-C(1) & 1.35(2) & O(1)-V(1)-O(3) & 91.1(4) \\ \hline N(1)-N(1) & 1.39(1) & O(1)-V(1)-O(3) & 91.1(4) \\ \hline N(1)-N(1) & 2.08(1) & O(3)-V(1)-O(3) & 88.3(5) \\ \hline C(1)-H(1) & 0.93 & O(1)-V(1)-N(1) & 87.5(5) \\ \hline C(4)-H(3) & 0.93 & O(3)-V(1)-N(1) & 176.7(4) \\ \hline N(1)-C(1) & 1.35(2) & O(3)-V(1)-N(1) & 88.7(3) \\ \hline N(1)-V(1) & 2.08(1) & O(1)-V(1)-N(1) & 88.7(3) \\ \hline N(1)-V(1) & 2.08(1) & O(1)-V(1)-N(1) & 88.7(3) \\ \hline O(3)-V(1) & 2.041(8) & O(3)-V(1)-N(1) & 88.7(3) \\ \hline O(3)-V(1) & 2.041(8) & N(1)-V(1)-N(1) & 94.1(5) \\ \hline V(1)-O(3) & 2.041(8) & N(1)-V(1)-O(2) & 91.4(3) \\ \hline V(1)-O(3) & 2.041(8) & N(1)-V(1)-O(2) & 91.4(3) \\ \hline V(1)-N(1) & 2.08(1) & O(3)-V(1)-O(2) & 91.4(3) \\ \hline V(1)-O(3) & 2.041(8) & N(1)-V(1)-O(2) & 91.4(3) \\ \hline V(1)-O(3) & 2.041(8) & N(1)-V(1)-O(2) & 91.4(3) \\ \hline V(1)-O(3) & 2.041(8) & N(1)-V(1)-O(2) & 91.4(3) \\ \hline V(1)-O(3) & 2.041(8) & N(1)-V(1)-O(2) & 90.1(4) \\ \hline C(5)-O(3) & 1.26(2) & C(1)-C(2)-C(1) & 105.7(17) \\ \hline O(1)-V(1) & 1.93(1) & C(1)-C(2)-C(3) & 127.1(9) \\ \hline O(1)-V(1) & 1.93(1) & C(1)-C(2)-C(3) & 127.1(9) \\ \hline O(1)-V(1) & 1.93(1) & C(1)-C(2)-C(3) & 127.1(9) \\ \hline O(1)-V(1) & 1.93(1) & C(1)-C(2)-C(3) & 127.1(9) \\ \hline O(1)-V(1) & 1.93(1) & C(1)-C(2)-C(3) & 127.1(9) \\ \hline O(1)-V(1) & 1.93(1) & C(1)-C(2)-C(3) & 127.1(9) \\ \hline O(1)-V(1) & 1.93(1) & C(1)-C(2)-C(3) & 127.1(9) \\ \hline O(1)-V(1) & 1.93(1) & C(1)-C(2)-C(3) & 127.1(9) \\ \hline O(1)-V(1) & 1.93(1) & C(1)-C(2)-C(3) & 127.1(9) \\ \hline O(1)-V(1) & 1.93(1) & C(1)-C(2)-C(3) & 127.1(9) \\ \hline O(1)-V(1) & 1.93(1) & C(1)-C(2)-C(3) & 127.1(9) \\ \hline O(1)-V(1) & 1.93(1) & C(1)-C(2)-C(3) & 127.1(9) \\ \hline O(1)-V(1) & 1.93(1) & C(1)-C(2)-C(3) & 127.1(9) \\ \hline O(1)-V(1) & 1.93(1) & C(1)-C(2)-C(3) & 127.1(9) \\ \hline O(1)-V(1) & 1.93(1) & C(1)-C(2)-C(3) & 127.1(9) \\ \hline O(1)-V(1) & 1.93(1) & C(1)-C(2)-C(3) & 127.1(9) \\ \hline O(1)-V(1) & 1.93(1) & C(1)-C(2)-C(3) & 127.1(9) \\ \hline O(1)-V(1) & 1.93(1) & C(1)-C(2)-C(3) & 127.1(9) \\ \hline O(1)-V(1) & 1.93(1$	C(2) - C(1)	1.34(2)	C(5) –O(3) –V(1)	133.1(11)
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	C(3) - C(4)	1.33(2)	V(1) -O(1) -V(1)	118.88(18)
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	C(3) - C(4)	1.33(2)	V(1) -O(1) -V(1)	118.88(18)
N(1) - C(1) $1.35(2)$ $O(1) -V(1) - O(3)$ $91.1(4)$ $N(1) - N(1)$ $1.39(1)$ $O(1) -V(1) -O(3)$ $91.1(4)$ $N(1) - V(1)$ $2.08(1)$ $O(3) -V(1) -O(3)$ $88.3(5)$ $C(1) - H(1)$ 0.93 $O(1) -V(1) -N(1)$ $87.5(5)$ $C(4) - H(3)$ 0.93 $O(3) -V(1) -N(1)$ $176.7(4)$ $N(1) - C(1)$ $1.35(2)$ $O(3) -V(1) -N(1)$ $88.7(3)$ $N(1) - C(1)$ $1.35(2)$ $O(3) -V(1) -N(1)$ $88.7(3)$ $N(1) - V(1)$ $2.08(1)$ $O(1) -V(1) -N(1)$ $87.5(5)$ $C(1) - H(1)$ 0.93 $O(3) -V(1) -N(1)$ $88.7(3)$ $O(3) - V(1)$ $2.041(8)$ $O(3) -V(1) -N(1)$ $176.7(4)$ $V(1) - O(3)$ $2.041(8)$ $N(1) -V(1) -N(1)$ $94.1(5)$ $V(1) - O(1)$ $1.93(1)$ $O(1) -V(1) -O(2)$ $91.4(3)$ $V(1) - O(3)$ $2.041(8)$ $N(1) -V(1) -O(2)$ $90.1(4)$ $C(5) - O(3)$ $1.26(2)$ $N(1) -V(1) -O(2)$ $90.1(4)$ $C(5) - O(3)$ $1.26(2)$ $C(1) -C(2) -C(3)$ $127.1(9)$ $O(1) - V(1)$ $1.93(1)$ $C(1) -C(2) -C(3)$ $127.1(9)$ $O(1) - V(1)$ $1.93(1)$ $C(1) -C(2) -C(3)$ $127.1(9)$	C(4) - H(3)	0.93	V(1)-O(1)-V(1)	118.88(18)
N(1) - N(1) $1.39(1)$ $O(1) -V(1) -O(3)$ $91.1(4)$ $N(1) - V(1)$ $2.08(1)$ $O(3) -V(1) -O(3)$ $88.3(5)$ $C(1) - H(1)$ 0.93 $O(1) -V(1) -N(1)$ $87.5(5)$ $C(4) - H(3)$ 0.93 $O(3) -V(1) -N(1)$ $176.7(4)$ $N(1) - C(1)$ $1.35(2)$ $O(3) -V(1) -N(1)$ $88.7(3)$ $N(1) - V(1)$ $2.08(1)$ $O(1) -V(1) -N(1)$ $88.7(3)$ $N(1) - V(1)$ $2.08(1)$ $O(1) -V(1) -N(1)$ $87.5(5)$ $C(1) - H(1)$ 0.93 $O(3) -V(1) -N(1)$ $88.7(3)$ $O(3) - V(1)$ $2.041(8)$ $O(3) -V(1) -N(1)$ $88.7(3)$ $O(3) - V(1)$ $2.041(8)$ $N(1) -V(1) -N(1)$ $94.1(5)$ $V(1) - O(3)$ $2.041(8)$ $N(1) -V(1) -O(2)$ $91.4(3)$ $V(1) - O(1)$ $1.93(1)$ $O(3) -V(1) -O(2)$ $91.4(3)$ $V(1) - O(3)$ $2.041(8)$ $N(1) -V(1) -O(2)$ $90.1(4)$ $C(5) - O(3)$ $1.26(2)$ $N(1) -V(1) -O(2)$ $90.1(4)$ $C(5) - O(3)$ $1.26(2)$ $C(1) -C(2) -C(3)$ $127.1(9)$ $O(1) - V(1)$ $1.93(1)$ $C(1) -C(2) -C(3)$ $127.1(9)$ $O(1) - V(1)$ $1.93(1)$ $C(1) -C(2) -C(3)$ $127.1(9)$	N(1) - C(1)	1.35(2)	O(1) -V(1) - O(3)	91.1(4)
N(1) - V(1)2.08(1) $O(3) -V(1) -O(3)$ 88.3(5) $C(1) - H(1)$ 0.93 $O(1) -V(1) -N(1)$ 87.5(5) $C(4) - H(3)$ 0.93 $O(3) -V(1) -N(1)$ 176.7(4) $N(1) - C(1)$ 1.35(2) $O(3) -V(1) -N(1)$ 88.7(3) $N(1) - V(1)$ 2.08(1) $O(1) -V(1) -N(1)$ 88.7(3) $C(1) - H(1)$ 0.93 $O(3) -V(1) -N(1)$ 88.7(3) $O(3) - V(1)$ 2.041(8) $O(3) -V(1) -N(1)$ 88.7(3) $O(3) - V(1)$ 2.041(8) $O(3) -V(1) -N(1)$ 176.7(4) $V(1) - O(3)$ 2.041(8) $N(1) -V(1) -N(1)$ 94.1(5) $V(1) - O(1)$ 1.93(1) $O(3) -V(1) -O(2)$ 91.4(3) $V(1) - N(1)$ 2.08(1) $O(3) -V(1) -O(2)$ 91.4(3) $V(1) - O(3)$ 2.041(8) $N(1) -V(1) -O(2)$ 90.1(4) $C(5) - O(3)$ 1.26(2) $C(1) -C(2) -C(1)$ 105.7(17) $O(1) - V(1)$ 1.93(1) $C(1) -C(2) -C(3)$ 127.1(9) $O(1) - V(1)$ 1.93(1) $C(1) -C(2) -C(3)$ 127.1(9)	N(1) - N(1)	1.39(1)	O(1) -V(1) -O(3)	91.1(4)
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	N(1) – V(1)	2.08(1)	O(3) -V(1) -O(3)	88.3(5)
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	C(1) - H(1)	0.93	O(1) -V(1) -N(1)	87.5(5)
N(1) - C(1) $1.35(2)$ $O(3) -V(1) -N(1)$ $88.7(3)$ $N(1) - V(1)$ $2.08(1)$ $O(1) -V(1) -N(1)$ $87.5(5)$ $C(1) - H(1)$ 0.93 $O(3) -V(1) -N(1)$ $87.5(5)$ $O(3) - V(1)$ $2.041(8)$ $O(3) -V(1) -N(1)$ $176.7(4)$ $V(1) - O(3)$ $2.041(8)$ $N(1) -V(1) -N(1)$ $94.1(5)$ $V(1) - O(1)$ $1.93(1)$ $O(1) -V(1) -O(2)$ $176.5(6)$ $V(1) - O(2)$ $2.11(1)$ $O(3) -V(1) -O(2)$ $91.4(3)$ $V(1) - N(1)$ $2.08(1)$ $O(3) -V(1) -O(2)$ $91.4(3)$ $V(1) - N(1)$ $2.08(1)$ $O(3) -V(1) -O(2)$ $91.4(3)$ $V(1) - O(3)$ $2.041(8)$ $N(1) -V(1) -O(2)$ $90.1(4)$ $C(5) - O(3)$ $1.26(2)$ $N(1) -V(1) -O(2)$ $90.1(4)$ $C(5) - O(3)$ $1.26(2)$ $C(1) -C(2) -C(1)$ $105.7(17)$ $O(1) - V(1)$ $1.93(1)$ $C(1) -C(2) -C(3)$ $127.1(9)$ $O(1) - V(1)$ $1.93(1)$ $C(1) -C(2) -C(3)$ $127.1(9)$	C(4) - H(3)	0.93	O(3) -V(1) -N(1)	176.7(4)
N(1) - V(1) $2.08(1)$ $O(1) -V(1) -N(1)$ $87.5(5)$ $C(1) - H(1)$ 0.93 $O(3) -V(1) -N(1)$ $88.7(3)$ $O(3) - V(1)$ $2.041(8)$ $O(3) -V(1) -N(1)$ $176.7(4)$ $V(1) - O(3)$ $2.041(8)$ $N(1) -V(1) -N(1)$ $94.1(5)$ $V(1) - O(1)$ $1.93(1)$ $O(1) -V(1) -O(2)$ $176.5(6)$ $V(1) - O(2)$ $2.11(1)$ $O(3) -V(1) -O(2)$ $91.4(3)$ $V(1) - N(1)$ $2.08(1)$ $O(3) -V(1) -O(2)$ $91.4(3)$ $V(1) - N(1)$ $2.08(1)$ $O(3) -V(1) -O(2)$ $91.4(3)$ $V(1) - O(3)$ $2.041(8)$ $N(1) -V(1) -O(2)$ $90.1(4)$ $C(5) - O(3)$ $1.26(2)$ $N(1) -V(1) -O(2)$ $90.1(4)$ $C(5) - O(3)$ $1.26(2)$ $C(1) -C(2) -C(1)$ $105.7(17)$ $O(1) - V(1)$ $1.93(1)$ $C(1) -C(2) -C(3)$ $127.1(9)$ $O(1) - V(1)$ $1.93(1)$ $C(1) -C(2) -C(3)$ $127.1(9)$	N(1) - C(1)	1.35(2)	O(3) -V(1) -N(1)	88.7(3)
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	N(1) – V(1)	2.08(1)	O(1) -V(1) -N(1)	87.5(5)
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	C(1) - H(1)	0.93	O(3) -V(1) -N(1)	88.7(3)
V(1) - O(3) $2.041(8)$ $N(1) -V(1) -N(1)$ $94.1(5)$ $V(1) - O(1)$ $1.93(1)$ $O(1) -V(1) -O(2)$ $176.5(6)$ $V(1) - O(2)$ $2.11(1)$ $O(3) -V(1) -O(2)$ $91.4(3)$ $V(1) - N(1)$ $2.08(1)$ $O(3) -V(1) -O(2)$ $91.4(3)$ $V(1) - N(1)$ $2.08(1)$ $O(3) -V(1) -O(2)$ $91.4(3)$ $V(1) - O(3)$ $2.041(8)$ $N(1) -V(1) -O(2)$ $90.1(4)$ $C(5) - O(3)$ $1.26(2)$ $N(1) -V(1) -O(2)$ $90.1(4)$ $C(5) - O(3)$ $1.26(2)$ $C(1) -C(2) -C(1)$ $105.7(17)$ $O(1) - V(1)$ $1.93(1)$ $C(1) -C(2) -C(3)$ $127.1(9)$ $O(1) - V(1)$ $1.93(1)$ $C(1) -C(2) -C(3)$ $127.1(9)$	O(3) – V(1)	2.041(8)	O(3) -V(1) -N(1)	176.7(4)
V(1) - O(1) $1.93(1)$ $O(1) -V(1) -O(2)$ $176.5(6)$ $V(1) - O(2)$ $2.11(1)$ $O(3) -V(1) -O(2)$ $91.4(3)$ $V(1) - N(1)$ $2.08(1)$ $O(3) -V(1) -O(2)$ $91.4(3)$ $V(1) - O(3)$ $2.041(8)$ $N(1) -V(1) -O(2)$ $90.1(4)$ $C(5) - O(3)$ $1.26(2)$ $N(1) -V(1) -O(2)$ $90.1(4)$ $C(5) - O(3)$ $1.26(2)$ $C(1) -C(2) -C(1)$ $105.7(17)$ $O(1) - V(1)$ $1.93(1)$ $C(1) -C(2) -C(3)$ $127.1(9)$ $O(1) - V(1)$ $1.93(1)$ $C(1) -C(2) -C(3)$ $127.1(9)$	V(1) – O(3)	2.041(8)	N(1) -V(1) -N(1)	94.1(5)
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V(1) - N(1) $2.08(1)$ $O(3) -V(1) -O(2)$ $91.4(3)$ $V(1) - O(3)$ $2.041(8)$ $N(1) -V(1) -O(2)$ $90.1(4)$ $C(5) - O(3)$ $1.26(2)$ $N(1) -V(1) -O(2)$ $90.1(4)$ $C(5) - O(3)$ $1.26(2)$ $C(1) -C(2) -C(1)$ $105.7(17)$ $O(1) - V(1)$ $1.93(1)$ $C(1) -C(2) -C(3)$ $127.1(9)$ $O(1) - V(1)$ $1.93(1)$ $C(1) -C(2) -C(3)$ $127.1(9)$	V(1) – O(2)	2.11(1)	O(3) -V(1) -O(2)	91.4(3)
V(1) - O(3)2.041(8) $N(1) -V(1) -O(2)$ 90.1(4) $C(5) - O(3)$ 1.26(2) $N(1) -V(1) -O(2)$ 90.1(4) $C(5) - O(3)$ 1.26(2) $C(1) -C(2) -C(1)$ 105.7(17) $O(1) - V(1)$ 1.93(1) $C(1) -C(2) -C(3)$ 127.1(9) $O(1) - V(1)$ 1.93(1) $C(1) -C(2) -C(3)$ 127.1(9) $O(1) - V(1)$ 1.93(1) $C(1) -C(2) -C(3)$ 127.1(9)	V(1) - N(1)	2.08(1)	O(3) -V(1) -O(2)	91.4(3)
C(5) - O(3) $1.26(2)$ $N(1) - V(1) - O(2)$ $90.1(4)$ $C(5) - O(3)$ $1.26(2)$ $C(1) - C(2) - C(1)$ $105.7(17)$ $O(1) - V(1)$ $1.93(1)$ $C(1) - C(2) - C(3)$ $127.1(9)$ $O(1) - V(1)$ $1.93(1)$ $C(1) - C(2) - C(3)$ $127.1(9)$ $O(1) - V(1)$ $1.93(1)$ $C(1) - C(2) - C(3)$ $127.1(9)$	V(1) – O(3)	2.041(8)	N(1) -V(1) -O(2)	90.1(4)
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O(1) - V(1) $1.93(1)$ $C(1) - C(2) - C(3)$ $127.1(9)$ $O(1) - V(1)$ $1.93(1)$ $C(1) - C(2) - C(3)$ $127.1(9)$	O(1) – V(1)	1.93(1)	C(1) –C(2) –C(3)	127.1(9)
	O(1) – V(1)	1.93(1)	C(1) -C(2) -C(3)	127.1(9)
O(3) - V(1) 2.041(8) $C(4) - C(3) - C(4)$ 115.7(17)	O(3) – V(1)	2.041(8)	C(4) -C(3) -C(4)	115.7(17)
V(1) - N(1) 2.08(1) $C(4) - C(3) - C(2)$ 122.1(8)	V(1) - N(1)	2.08(1)	C(4) –C(3) –C(2)	122.1(8)

V(1) - O(3)	2.041(8)	C(4) -C(3) -C(2)	122.1(8)
V(1) – O(2)	2.11(1)	C(3) -C(4) -C(4)	122.1(8)
V(1) - N(1)	2.08(1)	C(1) –N(1) –N(1)	106.1(7)
C(2) - C(3)	1.51(2)	C(1) –N(1) –V(1)	136.0(9)
C(2) - C(1)	1.34(2)	N(1) –N(1) –V(1)	117.8(3)
C(2) - C(1)	1.34(2)	C(2) –C(1) –N(1)	111.0(13)
C(3) – C(4)	1.33(2)	O(3) -C(5) -O(3)	124.5(18)
C(3) - C(4)	1.33(2)	C(5) –O(3) –V(1)	133.1(11)
C(4) – H(3)	0.93	V(1) –O(1) –V(1)	118.88(18)
C(4) - C(4)	1.41(2)	V(1) –O(1) –V(1)	118.88(18)
N(1) - C(1)	1.35(2)	V(1)-O(1)-V(1)	118.88(18)
N(1) – N(1)	1.39(1)	O(1) -V(1) - O(3)	91.1(4)
C(1) - H(1)	0.93	O(1) -V(1) -O(3)	91.1(4)
C(5) - O(3)	1.26(2)	O(3) -V(1) -O(3)	88.3(5)
C(5) - O(3)	1.26(2)	O(1) -V(1) -N(1)	87.5(5)
C(4) – H(3)	0.93	O(3) –V(1) –N(1)	176.7(4)
C(4) - C(4)	1.41(2)	O(3) –V(1) –N(1)	88.7(3)
N(1) - C(1)	1.35(2)	O(1) –V(1) –N(1)	87.5(5)
C(1) – H(1)	0.93	O(3) –V(1) –N(1)	88.7(3)
C(2) – C(3)	1.51(2)	O(3) –V(1) –N(1)	176.7(4)
C(2) - C(1)	1.34(2)	N(1) –V(1) –N(1)	94.1(5)
C(2) - C(1)	1.34(2)	O(1) -V(1) -O(2)	176.5(6)
C(3) – C(4)	1.33(2)	O(3) –V(1) –O(2)	91.4(3)
C(3) – C(4)	1.33(2)	O(3) –V(1) –O(2)	91.4(3)
C(4) – H(3)	0.93	N(1) -V(1) -O(2)	90.1(4)
N(1) – C(1)	1.35(2)	N(1) -V(1) -O(2)	90.1(4)
N(1) – N(1)	1.39(1)	C(1) -C(2) -C(1)	105.7(17)
N(1) – V(1)	2.08(1)	C(1) -C(2) -C(3)	127.1(9)
1	1	1	1

C(1) - H(1)	0.93	C(1) - C(2) - C(3)	127.1(9)
C(4) - H(3)	0.93	C(4) -C(3) -C(4)	115.7(17)
N(1) - C(1)	1.35(2)	C(4) –C(3) –C(2)	122.1(8)
N(1) – V(1)	2.08(1)	C(4) –C(3) –C(2)	122.1(8)
C(1) - H(1)	0.93	C(3) –C(4) –C(4)	122.1(8)
O(3) – V(1)	2.041(8)	C(1) –N(1) –N(1)	106.1(7)
V(1) - N(1)	2.08(1)	C(1) –N(1) –V(1)	136.0(9)
V(1) – O(3)	2.041(8)	N(1) –N(1) –V(1)	117.8(3)
V(1) – O(2)	2.11(1)	C(2) - C(1) - N(1)	111.0(13)
C(2) - C(3)	1.51(2)	O(3) -C(5) -O(3)	124.5(18)
C(2) - C(1)	1.34(2)	C(5) –O(3) –V(1)	133.1(11)
C(2) - C(1)	1.34(2)	V(1) –O(1) –V(1)	118.88(18)
C(3) - C(4)	1.33(2)	V(1) –O(1) –V(1)	118.88(18)
C(3) - C(4)	1.33(2)	V(1)-O(1)-V(1)	118.88(18)
C(4) - H(3)	0.93	O(1) -V(1) - O(3)	91.1(4)
C(4) - C(4)	1.41(2)	O(1) -V(1) -O(3)	91.1(4)
N(1) - C(1)	1.35(2)	O(3) -V(1) -O(3)	88.3(5)
N(1) - N(1)	1.39(1)	O(1) -V(1) -N(1)	87.5(5)
C(1) - H(1)	0.93	O(3) -V(1) -N(1)	176.7(4)
C(5) - O(3)	1.26(2)	O(3) -V(1) -N(1)	88.7(3)
C(5) - O(3)	1.26(2)	O(1) -V(1) -N(1)	87.5(5)
C(4) - H(3)	0.93	O(3) -V(1) -N(1)	88.7(3)
C(4) - C(4)	1.41(2)	O(3) -V(1) -N(1)	176.7(4)
N(1) - C(1)	1.35(2)	N(1) -V(1) -N(1)	94.1(5)
C(1) – H(1)	0.93	O(1) -V(1) -O(2)	176.5(6)
C(2) – C(3)	1.51(2)	O(3) -V(1) -O(2)	91.4(3)
C(2) – C(1)	1.34(2)	O(3) -V(1) -O(2)	91.4(3)
C(2) – C(1)	1.34(2)	N(1) -V(1) -O(2)	90.1(4)
1	1	1	1

C(3) - C(4)	1.33(2)	N(1) -V(1) -O(2)	90.1(4)
C(3) - C(4)	1.33(2)	C(1) –C(2) –C(1)	105.7(17)
C(4) – H(3)	0.93	C(1) –C(2) –C(3)	127.1(9)
N(1) - C(1)	1.35(2)	C(1) –C(2) –C(3)	127.1(9)
N(1) - N(1)	1.39(1)	C(4) –C(3) –C(4)	115.7(17)
N(1) – V(1)	2.08(1)	C(4) –C(3) –C(2)	122.1(8)
C(1) - H(1)	0.93		
C(4) – H(3)	0.93		
N(1) - C(1)	1.35(2)		
N(1) – V(1)	2.08(1)		
C(1) - H(1)	0.93		
V(1) - N(1)	2.08(1)		
V(1) – O(3)	2.041(8)		
V(1) – O(2)	2.11(1)		
V(1) – N(1)	2.08(1)		
C(2) - C(3)	1.51(2)		
C(2) - C(1)	1.34(2)		
C(2) - C(1)	1.34(2)		
C(3) - C(4)	1.33(2)		
C(3) - C(4)	1.33(2)		
C(4) – H(3)	0.93		
C(4) - C(4)	1.41(2)		
N(1) - C(1)	1.35(2)		
N(1) – N(1)	1.39(1)		
C(1) – H(1)	0.93		
C(5) – O(3)	1.26(2)		
C(5) – O(3)	1.26(2)		
C(4) – H(3)	0.93		

C(4) - C(4)	1.41(2)
N(1) - C(1)	1.35(2)
C(1) - H(1)	0.93
C(2) - C(3)	1.51(2)
C(2) - C(1)	1.34(2)
C(2) - C(1)	1.34(2)
C(3) - C(4)	1.33(2)
C(3) - C(4)	1.33(2)
C(4) - H(3)	0.93
N(1) - C(1)	1.35(2)
N(1) - N(1)	1.39(1)
N(1) - V(1)	2.08(1)
C(1) - H(1)	0.93
C(4) - H(3)	0.93
N(1) - C(1)	1.35(2)
N(1) - V(1)	2.08(1)
C(1) - H(1)	0.93
O(3) - V(1)	2.041(8)
V(1) – O(3)	2.041(8)
V(1) - O(1)	1.93(1)
V(1) – O(2)	2.11(1)
V(1) – O(3)	2.041(8)
V(1) - N(1)	2.08(1)
C(5) - O(3)	1.26(2)
C(5) – O(3)	1.26(2)
O(1) – V(1)	1.93(1)
O(1) – V(1)	1.93(1)
O(3) – V(1)	2.041(8)

V(1) – O(3)	2.041(8)
V(1) – O(1)	1.93(1)
V(1) – O(2)	2.11(1)
V(1) - N(1)	2.08(1)
V(1) – O(3)	2.041(8)
C(5) – O(3)	1.26(2)
C(5) - O(3)	1.26(2)
O(1) - V(1)	1.93(1)
O(1) - V(1)	1.93(1)
O(3) – V(1)	2.041(8)
V(1) - N(1)	2.08(1)
V(1) – O(3)	2.041(8)
V(1) – O(2)	2.11(1)
C(2) - C(3)	1.51(2)
C(2) - C(1)	1.34(2)
C(2) - C(1)	1.34(2)
C(3) - C(4)	1.33(2)
C(3) - C(4)	1.33(2)
C(4) - H(3)	0.93
C(4) - C(4)	1.41(2)
N(1) - C(1)	1.35(2)
N(1) - N(1)	1.39(1)
C(1) - H(1)	0.93
C(5) – O(3)	1.26(2)
C(5) – O(3)	1.26(2)
C(4) – H(3)	0.93
C(4) – C(4)	1.41(2)
N(1) - C(1)	1.35(2)

C(1) - H(1)	0.93	
C(2) - C(3)	1.51(2)	
C(2) - C(1)	1.34(2)	
C(2) - C(1)	1.34(2)	
C(3) - C(4)	1.33(2)	
C(3) - C(4)	1.33(2)	
C(4) - H(3)	0.93	
N(1) - C(1)	1.35(2)	
N(1) - N(1)	1.39(1)	
C(1) - H(1)	0.93	
C(4) - H(3)	0.93	
N(1) - C(1)	1.35(2)	
N(1) – V(1)	2.08(1)	
C(1) - H(1)	0.93	
V(1) – O(3)	2.041(8)	
V(1) – O(2)	2.11(1)	
V(1) – O(3)	2.041(8)	
C(5) - O(3)	1.26(2)	
C(5) - O(3)	1.26(2)	
V(1) – O(3)	2.041(8)	
V(1) – O(2)	2.11(1)	
V(1) - N(1)	2.08(1)	
C(5) - O(3)	1.26(2)	
C(5) – O(3)	1.26(2)	
O(3) – V(1)	2.041(8)	
V(1) – O(2)	2.11(1)	
V(1) – O(3)	2.041(8)	
V(1) – N(1)	2.08(1)	

C(5) - O(3)	1.26(2)	
C(5) - O(3)	1.26(2)	
O(3) - V(1)	2.041(8)	
C(5) - O(3)	1.26(2)	
C(5) - O(3)	1.26(2)	
V(1) - O(2)	2.11(1)	
V(1) - N(1)	2.08(1)	
C(2) - C(3)	1.51(2)	
C(2) - C(1)	1.34(2)	
C(2) - C(1)	1.34(2)	
C(3) - C(4)	1.33(2)	
C(3) - C(4)	1.33(2)	
C(4) - H(3)	0.93	
C(4) - C(4)	1.41(2)	
N(1) - C(1)	1.35(2)	
N(1) - N(1)	1.39(1)	
C(1) - H(1)	0.93	
C(4) - H(3)	0.93	
C(4) - C(4)	1.41(2)	
N(1) - C(1)	1.35(2)	
C(1) - H(1)	0.93	
C(2) - C(3)	1.51(2)	
C(2) - C(1)	1.34(2)	
C(2) - C(1)	1.34(2)	
C(3) – C(4)	1.33(2)	
C(3) – C(4)	1.33(2)	
C(4) – H(3)	0.93	
N(1) – C(1)	1.35(2)	

N(1) - N(1)	1.39(1)	
C(1) - H(1)	0.93	
C(4) - H(3)	0.93	
N(1) - C(1)	1.35(2)	
C(1) - H(1)	0.93	

References

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