## **Electronic supplementary information**

## CO Tolerance of Pt<sub>3</sub>Sn(111) Catalyst in Ethanol Decomposition

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## 1. Elementary reaction

*Acetyl Oxidation.* Under the oxidative conditions, CH<sub>3</sub>CO can oxidize easily by OH group to form CH<sub>3</sub>COOH. As shown on Figure S2 (f1), this process starts with the CH<sub>3</sub>CO fragment and OH group locating at T<sup>Pt</sup> site as the IS, ends with the CH<sub>3</sub>COOH remaining at T<sup>Pt</sup> site as the FS. In the TS, the OH group are close to the CH<sub>3</sub>CO fragment, and the O atom of OH group and the C atom of CH<sub>3</sub>CO form a newly C<sup> $\alpha$ </sup>–O bond with the length of 1.81 Å. The energy barrier of this reaction is only 0.38 eV and the reaction energy is exothermic by 1.09 eV.

 $H + H \rightarrow H_2$ . As shown in the Figure S2, the two H atoms are adsorbed at adjacent H<sup>3Pt</sup> and F<sup>3Pt</sup> sites as the IS. The diffusions of both H atoms form the TS, in which the two H atoms bind at top site with H–H distance of 1.144 Å. After the TS, the two H atoms approach each other forming FS. This process has an energy barrier of 0.71 eV, and is endothermic by 0.75 eV. For the newly-formed H<sub>2</sub> molecule, it is easy to escape from the Pt<sub>3</sub>Sn(111) surface due to the weak adsorption energy about 0.1 eV at different adsorption sites.

## 2. Microkinetic model

We applied the microkinetic modeling technique to examine the oxidation of ethanol on Pt<sub>3</sub>Sn(111). All of steps included in the microkinetic model are summarized in Table 4 (see the main manuscripts). Step 1 were assumed to be in equilibrium and the equilibrium constant *K* was estimated according to  $K = \exp[-(\Delta E_{ads} - T\Delta S)/k_BT]$ , in which  $\Delta E_{ads}$  is the binding energy of CH<sub>3</sub>CH<sub>2</sub>OH on Pt<sub>3</sub>Sn(111), while  $\Delta S$  is the entropy change of the corresponding adsorbate induced by adsorption. The other steps were described by the forward rate.

The site balance of intermediate species included in the reaction can be written in terms of coverage ( $\theta_x$ ; X = surface species):

$$\theta_{CH_3CH_2OH} + \theta_{CH_3CH_2O} + \theta_{CH_3CHO} + \theta_{CH_3CO} + \theta_{CH_2CO} + \theta_{CO} + \theta_{CH_2} + \theta_{CH_3} + \theta_{CH_4} + \theta_{H} + \theta_{H_2} + \theta_* = 1(1)$$

The coverage of CH<sub>3</sub>CH<sub>2</sub>OH is  $\theta_{CH_3CH_2OH} = p_{CH_3CH_2OH}K_1\theta_*$ , respectively. Other surface species including CH<sub>3</sub>CH<sub>2</sub>O, CH<sub>3</sub>CHO, CH<sub>3</sub>CO, CH<sub>2</sub>CO, CO, CH<sub>2</sub>, CH<sub>3</sub>, CH<sub>4</sub> and H can be described according to the steady-state approximation as summarized below, where the production and consumption rates of each species are assumed to be equal:

1. 
$$\frac{d\theta_{CH_{3}CH_{2}O}}{dt} = r_{2} - r_{3} = k_{2}\theta_{CH_{3}CH_{2}OH}\theta_{*} - k_{3}\theta_{CH_{3}CH_{2}O}\theta_{*} = 0$$
$$\theta_{CH_{3}CH_{2}O} = \frac{k_{2}}{k_{3}}p_{CH_{3}CH_{2}OH}K_{1}\theta_{*}$$
(2)

2. 
$$\frac{d\theta_{CH_3CHO}}{dt} = r_3 - r_4 = k_3 \theta_{CH_3CH_2O} \theta_* - k_4 \theta_{CH_3CHO} \theta_* = 0$$
$$\theta_{CH_3CHO} = \frac{k_2}{k_4} p_{CH_3CH_2OH} K_1 \theta_*$$
(3)

3. 
$$\frac{d\theta_{CH_3CO}}{dt} = r_4 - r_5 = k_4 \theta_{CH_3CHO} \theta_* - k_5 \theta_{CH_3CO} \theta_* = 0$$
$$\theta_{CH_3CO} = \frac{k_2}{k_5} p_{CH_3CH_2OH} K_1 \theta_*$$
(4)

4. 
$$\frac{d\theta_{CH_2CO}}{dt} = r_5 - r_6 = k_5 \theta_{CH_3CO} \theta_* - k_6 \theta_{CH_2CO} \theta_* = 0$$
$$\theta_{CH_2CO} = \frac{k_2}{k_6} p_{CH_3CH_2OH} K_1 \theta_*$$
(5)

5. 
$$\frac{d\theta_{CO}}{dt} = r_6 - r_{10} = k_6 \theta_{CH_2CO} \theta_* - k_{10} \theta_{CO} = 0$$
$$\theta_{CO} = \frac{k_2}{k_{10}} p_{CH_3CH_2OH} K_1 \theta_*^2$$
(6)

6. 
$$\frac{d\theta_{CH_2}}{dt} = r_6 - r_7 = k_6 \theta_{CH_2CO} \theta_* - k_7 \theta_{CH_2} \theta_H = 0$$

$$\theta_{CH_2} = \frac{k_2 \theta_*}{k_7 \theta_H} p_{CH_3 CH_2 OH} K_1 \theta_*$$
(7)

(9)

7. 
$$\frac{d\theta_{CH_3}}{dt} = r_7 - r_8 = k_7 \theta_{CH_2} \theta_H - k_8 \theta_{CH_3} \theta_H = 0$$
$$\theta_{CH_3} = \frac{k_2 \theta_*}{k_8 \theta_H} p_{CH_3 CH_2 OH} K_1 \theta_*$$
(8)

8. 
$$\frac{d\theta_{H}}{dt} = r_{2} + r_{3} + r_{4} + r_{5} - r_{7} - r_{8} - 2r_{9}$$
$$= k_{2}\theta_{CH_{3}CH_{2}OH}\theta_{*} + k_{3}\theta_{CH_{3}CH_{2}O}\theta_{*} + k_{4}\theta_{CH_{3}CHO}\theta_{*} + k_{5}\theta_{CH_{3}CO}\theta_{*} - k_{7}\theta_{CH_{2}}\theta_{H} - k_{8}\theta_{CH_{3}}\theta_{H} - 2k_{9}\theta_{H}^{2} = 0$$
$$\theta_{H} = \sqrt{\frac{k_{2}P_{CH_{3}CH_{2}OH}K_{1}}{k_{9}}}\theta_{*}$$
(9)

9. 
$$\frac{d\theta_{CH_4}}{dt} = r_8 - r_{11} = k_8 \theta_{CH_3} \theta_H - k_{11} \theta_{CH_4} = 0$$
$$\theta_{CH_4} = \frac{k_2}{k_{11}} p_{CH_3 CH_2 OH} K_1 \theta_* \theta_H$$
(10)

10. 
$$\frac{d\theta_{H_2}}{dt} = r_9 - r_{12} = k_9 \theta_H^2 - k_{12} \theta_{H_2} = 0$$
$$\theta_{H_2} = \frac{k_2}{k_{12}} p_{CH_3 CH_2 OH} K_1 \theta_*^2$$
(11)

By putting all the coverage expressions into eq. 1, we can calculate  $\theta_*$  and other surface coverages.

To test the effect of different partial pressure on the coverages, the calculations of the microkinetic model at 1, 2 and 3 atm are carried out in the range of 100 to 300 K, as shown in Table S1. These results show that with the pressure increases, the number of vacant sites  $\theta^*$  decreases at the same temperature above 200 K; the coverage of  $CH_2CO$  increase at the same temperature from 100 to 300 K; and the  $\theta\_CH_2$  can reach the higher peak at higher ethanol partial pressure. These results indicate that the small increasing pressure has a minor effect on the coverages in the range of 100 to 300 K.

T (K)	1 atm			2 atm				3 atm		
	θ*	$\theta_{CH_2CO}$	$\theta_{CH_2}$	θ*	$\theta\_CH_2CO$	$\theta_{CH_2}$		$\theta^*$	$\theta\_CH_2CO$	$\theta\_CH_2$
100	0.000	1.000	0.000	0.000	1.000	0.000		0.000	1.000	0.000
150	0.000	0.724	0.273	0.000	0.787	0.210		0.000	0.819	0.179
200	0.433	0.070	0.495	0.339	0.110	0.549		0.287	0.140	0.570
250	0.958	0.001	0.041	0.941	0.002	0.057		0.928	0.003	0.069
300	0.995	0.000	0.005	0.993	0.000	0.007		0.992	0.000	0.008

**Table S1.** Effect of temperature and ethanol partial pressure on the coverages of CH<sub>2</sub>CO ( $\theta$ \_CH<sub>2</sub>CO), CH<sub>2</sub> ( $\theta$ \_CH<sub>2</sub>) as well as vacant site ( $\theta$ \*).

Figure S1. Configurations of reaction intermediates along reaction pathway of ethanol decomposition to CO on  $Pt_3Sn(111)$ .





Figure S2. Calculated structures of the initial state, transition state, and final state involved in ethanol decomposition routes on  $Pt_3Sn(111)$ .



CH<sub>3</sub>CH<sub>2</sub>OH-T<sup>Pt</sup>-*cis* TS ( $\tilde{v} = i \ 1329 \ \text{cm}^{-1}$ )





CH<sub>3</sub>CH<sub>2</sub>OH-T<sup>Sn</sup>-cis

 $CH_2CH_2OH + H$ 







**Figure S3.** Calculated structures of the initial state, transition state, and final state involved in the CH<sub>2</sub>CO decomposition on  $Pt_3Sn(111)$  with a large (4 × 4) cell.