# Electronic Supplementary Information: 

# Identifying Systematic DFT Errors in Catalytic Reactions 

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## S1 Computational method

Calculations have been performed using the VASP code with the projector augmented-wave (PAW) method. ${ }^{1-4}$ In general, calculational parameters have been chosen very cautiously to avoid inducing errors unrelated to the choice of functional, e.g. by using more accurate PAW potentials and higher plane wave energy cut-off than usually needed. The hard PAW potentials distributed with the code have been used for $\mathrm{C}, \mathrm{H}$ and O atoms and default potential for Cu . The potentials have been generated with the PBE functional and are used for all functionals. This is expected to give negligible errors. An energy cut-off at 650 eV has been used. The high cut-off value is required for convergence with the hard PAW potentials. For gas phase species, $\Gamma$-point calculations were performed. For adsorption energies, a $(4,4,1)$ Monkhorst-Pack k-point mesh was applied. Although not expected to be of importance, spin polarization has been included. Atomic configurations were optimized to a maximum force of $0.05 \mathrm{eV} / \AA$. Vibrational ground state energies have been calculated for geometries with a maximum force of $0.01 \mathrm{eV} / \AA$ using the RPBE functional and extrapolated to the other functionals. Vibrational energies match well with those found by Peterson et al. ${ }^{5}$ The approach for conversion to free energies has also been adapted from Peterson et al. ${ }^{5}$

For the Cu surface, a cell with three closed-pack layers with 9 atoms in each was used with periodic boundary conditions in the surface plane dimensions. Perpendicular to the surface a vacuum region of $12 \AA$ has been used with dipole corrections at the cell boundaries. The two lower layers have been constrained to simulate a large underlying bulk structure. The lattice constant has been optimized for each functional.

## S1.1 Examined reactions

Previously, ${ }^{5-7}$ reactions similar to reactions (1)-(10) in Table 1 of the main text with CO as reactant instead of $\mathrm{CO}_{2}$ have also been used. As they couple with those in the Primary Set through the reverse water-gas shift reaction, i.e. reaction (0), they do not add any additional
experimental data and have thus been omitted for simplicity.

## S2 Functional dependence on reactions

An extended analysis is conducted to confirm that the dominating functional dependence can be attributed to the carbon-oxygen double $(\mathrm{C}=\mathrm{O})$ bonds. With the assumption that $\mathrm{C}=\mathrm{O}$ bonds dominate functional dependence, the slope when plotting two reactions versus each other can be predicted by dividing the change in $\mathrm{C}=\mathrm{O}$ bonds in the reaction plotted on the y -axis with the change in $\mathrm{C}=\mathrm{O}$ bonds in the reaction plotted on the x -axis. All possible combinations of reactions (1)-(16) have been examined. In $66 \%$ of the cases the predicted slope will be different from 1. Slopes found through linear regression on the ensemble functionals are compared with predicted slopes. The differences between predicted and fitted slopes relative to the fitted slopes are depicted in Figure S1a.


Figure S1: Overview of analysis.

The difference between fitted and predicted slopes is at most $5 \%$ with few exceptions discussed below. The good agreement confirms that $\mathrm{C}=\mathrm{O}$ bonds are the major functional dependent molecular components. The exceptions are cases where reactions (2), (11) or
(12) are involved and most notably when they are used as independent reaction. In the products of these three reactions, the ratio of $\mathrm{C}=\mathrm{O}$ bonds to carbon atoms is 1 . Thus only one of the $\mathrm{C}=\mathrm{O}$ bonds present in the reactant $\mathrm{CO}_{2}$ is broken resulting in less functional dependent reaction enthalpies than for the other reactions. As the level of data noise is not reduced correspondingly, the slope of the line is less well-defined. This is exemplified in Figure S2. The linear regression for reaction (2) and (3) will give a slope of 1.67, where the predicted is 2.0 . As can be seen, the fitted slope is not significantly better in terms of describing functional dependence than a slope with 2.0 , which actually fits better with the 5 main functionals. The coefficient of determination $\left(\mathrm{R}^{2}\right)$ of the linear regressions (Figure S1b) can be used as an indicator for cases, where the slope found from linear regression is a sub-optimal measure for functional dependence. It is noteworthy, that cases where the fitted and predicted slopes differ the most all have relatively low $\mathrm{R}^{2}$ value. I.e., these cases are less well described by a linear relation.


Figure S2: Example of how the slope obtained through linear regression is not given to be a good description of functional dependence.

In addition to $\mathrm{C}=\mathrm{O}$ bonds, carbon-carbon double $(\mathrm{C}=\mathrm{C})$ bonds present in the $\mathrm{C}_{2} \mathrm{H}_{4}$ and $\mathrm{C}_{4} \mathrm{H}_{6}$ products of reactions (7) and (8), respectively, also display significant functional dependence. This can be found in a similar way as for $\mathrm{C}=\mathrm{O}$ bonds by considering the slope of reactions. To remove $\mathrm{CO}_{2}$ functional dependence from reactions, methane is used as reactant. $\mathrm{H}_{2}$ and hydrocarbons with different amounts of $\mathrm{C}=\mathrm{C}$ bonds are used as products. Two such cases are illustrated in Figure S3. In Figure S3(a), the reaction plotted on the x -axis displays little functional dependence as no $\mathrm{C}=\mathrm{C}$ bonds are formed. The reaction plotted on the y -axis displays significant functional dependence as one $\mathrm{C}=\mathrm{C}$ bond is formed. In Figure $\mathrm{S} 3(\mathrm{~b})$, two $\mathrm{C}=\mathrm{C}$ bonds are formed in the reaction on the x -axis and one in the reaction on the y-axis. The slope is observed to agree with the expected 0.5 .


Figure S3: Correlations between reactions with different number of $\mathrm{C}=\mathrm{C}$ bonds formed.

The functional dependence of the $\mathrm{C}=\mathrm{C}$ bond scales linearly with the $\mathrm{C}=\mathrm{O}$ bond, i.e. the error in $\mathrm{C}=\mathrm{O}$ and $\mathrm{C}=\mathrm{C}$ energy will for a given functional correlate. If this was not the case the presence of both $\mathrm{C}=\mathrm{O}$ and $\mathrm{C}=\mathrm{C}$ bonds in reactions (7) and (8) would result in an increasingly scattered ensemble pattern when plotted against other reactions. However, the $R^{2}$ values for the linear regressions involving reactions (7) and (8) are similar to those for other reactions. The functional dependence on $\mathrm{C}=\mathrm{C}$ bonds is included in prediction of
slopes. The functional dependence relative to $\mathrm{C}=\mathrm{O}$ bonds are determined by minimizing the mean of the relative differences shown in Figure S1a. It is found to be 0.72 , which corresponds to a correction of approximately 0.1 eV per $\mathrm{C}=\mathrm{C}$ bond. When determining optimal corrections for $\mathrm{C}=\mathrm{O}$ bonds and $\mathrm{H}_{2}$, addition of corrections specifically applied to $\mathrm{C}=\mathrm{C}$ bonds will with the used reactions not change the optimal corrections found for $\mathrm{H}_{2}$ and $\mathrm{C}=\mathrm{O}$ bonds. As $\mathrm{C}=\mathrm{C}$ bonds are less functional dependent and generally present in smaller numbers than $\mathrm{C}=\mathrm{O}$ bonds when considering $\mathrm{CO}_{2}$ reduction catalysts, e.g. $2 \mathrm{C}=\mathrm{O}$ bonds to $1 / 2 \mathrm{C}=\mathrm{C}$ bond in reaction (7) (formation of ethylene), the potential error associated with the $\mathrm{C}=\mathrm{C}$ bonds will in most cases be insignificant in comparison to other sources of error. It might, however, be important in studies of larger organic species.

## S3 Energies

Table S1 shows used electronic, ZPE, and $\int C_{p} \mathrm{~d} T$ energies.
Table S1: List of energies in eV. ZPE and $\int C_{p} \mathrm{~d} T$ computed from frequencies obtained with RPBE.

| Specie | BEEF- <br> vdW | PBE | RPBE | vdWDF | vdWDF2 | ZPE | $\int C_{p} \mathrm{~d} T$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{CO}_{2}$ | -18.52 | -23.10 | -22.51 | -17.20 | -17.79 | 0.31 | 0.10 |
| $\mathrm{H}_{2}$ | -7.46 | -6.76 | -7.04 | -7.37 | -7.55 | 0.32 | 0.09 |
| CO | -12.14 | -14.89 | -14.59 | -11.37 | -11.82 | 0.14 | 0.09 |
| $\mathrm{H}_{2} \mathrm{O}$ | -13.12 | -14.23 | -14.26 | -12.52 | -12.89 | 0.60 | 0.10 |
| $\mathrm{CH}_{4}$ | -23.77 | -23.99 | -24.14 | -23.12 | -23.65 | 1.17 | 0.10 |
| HCOOH | -25.80 | -29.92 | -29.42 | -24.34 | -25.07 | 0.90 | 0.11 |
| $\mathrm{CH}_{3} \mathrm{OH}$ | -28.27 | -30.19 | -30.08 | -27.16 | -27.86 | 1.36 | 0.11 |
| $\mathrm{CH}_{3} \mathrm{CH}_{2} \mathrm{OH}$ | -44.07 | -46.84 | -46.54 | -42.38 | -43.40 | 2.12 | 0.11 |
| $\mathrm{C}_{3} \mathrm{H}_{8}$ | -55.05 | -56.94 | -56.75 | -53.25 | -54.39 | 2.73 | 0.11 |
| $\mathrm{C}_{2} \mathrm{H}_{6}$ | -39.37 | -40.43 | -40.42 | -38.15 | -38.98 | 1.96 | 0.11 |
| $\mathrm{C}_{2} \mathrm{H}_{4}$ | -30.40 | -31.93 | -31.79 | -29.36 | -30.11 | 1.34 | 0.11 |
| $\mathrm{C}_{4} \mathrm{H}_{6}$ | -53.24 | -56.94 | -56.33 | -51.23 | -52.51 | 2.24 | 0.11 |
| $\mathrm{CH}_{3} \mathrm{COOH}$ | -41.76 | -46.75 | -46.07 | -39.74 | -40.77 | 1.62 | 0.11 |
| $\mathrm{HCOOCH}_{3}$ | -41.10 | -46.02 | -45.36 | -39.13 | -40.21 | 1.63 | 0.11 |
| $\mathrm{CH}_{2} \mathrm{O}$ | -19.82 | -22.15 | -21.91 | -18.88 | -19.40 | 0.70 | 0.10 |
| OCHCHO | -32.04 | -37.37 | -36.59 | -30.24 | -31.07 | 0.96 | 0.11 |
| $\mathrm{C}_{2} \mathrm{H}_{5} \mathrm{COOH}$ | -57.43 | -63.25 | -62.30 | -54.84 | -56.03 | 2.38 | 0.11 |
| $\mathrm{CH}_{3} \mathrm{COOCH}_{3}$ | -57.04 | -62.82 | -61.88 | -54.50 | -55.75 | 2.35 | 0.11 |
| $\mathrm{CH}_{3} \mathrm{OCH}_{3}$ | -43.61 | -46.33 | -45.99 | -41.96 | -42.92 | 2.10 | 0.11 |
| $\mathrm{CH}_{3} \mathrm{CHO}$ | -35.90 | -39.11 | -38.67 | -34.37 | -35.17 | 1.47 | 0.11 |
| $\mathrm{Cu}(111)$ surf | -9.00 | - | - | - | - | - | - |
| $\mathrm{COOH}^{*}$ | -30.54 | -118.30 | -105.77 | -15.12 | -24.69 | 0.59 | 0.10 |
| $\mathrm{CH}_{3}{ }^{*}$ | -27.81 | -111.75 | -99.91 | -13.23 | -22.61 | 0.92 | 0.10 |

## S4 Atomic configurations

Below (Section S5) the applied atomic configurations used with the BEEF-vdW functional, and thus also for the ensemble, are written in Cartesian coordinates in units of $\AA$. For the other functionals, the atomic configurations are similar, but have been relaxed resulting in slightly different bond lengths (Table S3). It also includes the bond lengths in $\mathrm{COOH}^{*}$ and HCOOH between the non-hydrogenated oxygen atom and the carbon atom. For the surface calculations different interatomic distances for the Cu atoms simulating bulk have been used.

Table S3: Distance in $\AA$ between atoms for various bonds with the used functionals.

| Bond | Specie | BEEF-vdW | PBE | RPBE | vdW-DF | vdW-DF2 |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{H}-\mathrm{H}$ | $\mathrm{H}_{2}$ | 0.738 | 0.752 | 0.749 | 0.740 | 0.736 |
| $\mathrm{O}-\mathrm{H}$ | $\mathrm{H}_{2} \mathrm{O}$ | 0.963 | 0.969 | 0.970 | 0.969 | 0.968 |
| $\mathrm{C}=\mathrm{O}$ | $\mathrm{CO}_{2}$ | 1.167 | 1.170 | 1.174 | 1.174 | 1.170 |
| $\mathrm{C}=\mathrm{O}$ | $\mathrm{COOH}^{*}$ | 1.211 | 1.214 | 1.219 | 1.217 | 1.212 |
| $\mathrm{C}=\mathrm{O}$ | HCOOH | 1.202 | 1.206 | 1.210 | 1.209 | 1.206 |
| $\mathrm{C} \equiv \mathrm{O}$ | CO | 1.133 | 1.135 | 1.139 | 1.136 | 1.132 |
| $\mathrm{C}-\mathrm{O}$ | $\mathrm{CH}_{3} \mathrm{OH}$ | 1.435 | 1.433 | 1.441 | 1.445 | 1.453 |
| $\mathrm{C}-\mathrm{H}$ | $\mathrm{CH}_{3} \mathrm{OH}$ | 1.096 | 1.103 | 1.104 | 1.099 | 1.095 |
| $\mathrm{C}-\mathrm{C}$ | $\mathrm{C}_{2} \mathrm{H}_{6}$ | 1.528 | 1.527 | 1.536 | 1.538 | 1.539 |
| $\mathrm{C}=\mathrm{C}$ | $\mathrm{C}_{2} \mathrm{H}_{4}$ | 1.332 | 1.334 | 1.339 | 1.336 | 1.331 |
| $\mathrm{Cu}-\mathrm{Cu}$ | bulk Cu | 2.595 | 2.567 | 2.602 | 2.623 | 2.645 |

## References

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## S5 Positions



| HCOOH |  |  |  |
| :---: | :---: | :---: | :---: |
| H | 5.3377 | 4.6609 | 6.0000 |
| H | 5.6218 | 7.4528 | 6.0000 |
| C | 6.0091 | 6.4250 | 6.0000 |
| O | 4.9625 | 5.5569 | 6.0000 |
| O | 7.1700 | 6.1134 | 6.0000 |
| $\mathrm{CH}_{3} \mathrm{OH}$ |  |  |  |
| H | 4.9058 | 6.9725 | 6.0000 |
| H | 6.8758 | 4.9443 | 6.0000 |
| H | 6.4363 | 7.0821 | 6.8932 |
| H | 6.4363 | 7.0821 | 5.1068 |
| C | 5.9525 | 6.6712 | 6.0000 |
| O | 5.9589 | 5.2358 | 6.0000 |
| $\mathrm{CH}_{3} \mathrm{CH}_{2} \mathrm{OH}$ |  |  |  |
| H | 4.0448 | 6.3950 | 6.0000 |
| H | 6.0395 | 7.2020 | 6.8883 |
| H | 6.0395 | 7.2020 | 5.1117 |
| H | 8.1131 | 6.1500 | 6.0000 |
| H | 7.1456 | 4.9574 | 6.8857 |
| H | 7.1456 | 4.9574 | 5.1143 |
| C | 7.1724 | 5.5950 | 6.0000 |
| C | 6.0024 | 6.5577 | 6.0000 |
| O | 4.7868 | 5.7817 | 6.0000 |


|  | H | 5.1239 | 6.0000 | 7.2378 |
| :---: | :---: | :---: | :---: | :---: |
|  | H | 6.8761 | 6.0000 | 7.2378 |
|  | H | 6.0000 | 8.1683 | 6.3724 |
|  | H | 6.0000 | 3.8317 | 6.3724 |
|  | H | 6.8831 | 7.3261 | 5.0958 |
|  | H | 5.1169 | 7.3261 | 5.0958 |
|  | H | 5.1169 | 4.6739 | 5.0958 |
|  | H | 6.8831 | 4.6739 | 5.0958 |
|  | C | 6.0000 | 6.0000 | 6.5801 |
|  | C | 6.0000 | 7.2775 | 5.7398 |
|  | C | 6.0000 | 4.7225 | 5.7398 |
| $\mathrm{C}_{2} \mathrm{H}_{6}$ |  |  |  |  |
|  | H | 6.0000 | 7.0185 | 7.1603 |
|  | H | 5.1185 | 5.4915 | 7.1609 |
|  | H | 6.8815 | 5.4915 | 7.1609 |
|  | H | 6.0000 | 4.9815 | 4.8397 |
|  | H | 5.1185 | 6.5085 | 4.8391 |
|  | H | 6.8815 | 6.5085 | 4.8391 |
|  | C | 6.0000 | 6.0004 | 6.7640 |
|  | C | 6.0000 | 5.9996 | 5.2360 |
| $\mathrm{C}_{2} \mathrm{H}_{4}$ |  |  |  |  |
|  | H | 6.0000 | 6.9211 | 7.2365 |


|  | H | 6.0000 | 5.0789 | 7.2365 |
| :---: | :---: | :---: | :---: | :---: |
|  | H | 6.0000 | 6.9211 | 4.7635 |
|  | H | 6.0000 | 5.0789 | 4.7635 |
|  | C | 6.0000 | 6.0000 | 6.6660 |
|  | C | 6.0000 | 6.0000 | 5.3340 |
| $\mathrm{C}_{4} \mathrm{H}_{6}$ |  |  |  |  |
|  | H | 5.5118 | 7.4739 | 6.0001 |
|  | H | 6.4884 | 4.5262 | 6.0001 |
|  | H | 3.2724 | 6.5050 | 6.0000 |
|  | H | 3.9885 | 4.8018 | 6.0000 |
|  | H | 8.7277 | 5.4954 | 6.0000 |
|  | H | 8.0113 | 7.1985 | 6.0000 |
|  | C | 5.3899 | 6.3934 | 6.0000 |
|  | C | 6.6102 | 5.6066 | 6.0000 |
|  | C | 4.1511 | 5.8737 | 6.0000 |
|  | C | 7.8489 | 6.1265 | 6.0000 |
| $\mathrm{CH}_{3} \mathrm{COOH}$ |  |  |  |  |
|  | H | 4.1215 | 6.3310 | 6.0000 |
|  | H | 8.0522 | 5.5861 | 6.0000 |
|  | H | 6.9732 | 4.4692 | 6.8791 |
|  | H | 6.9732 | 4.4692 | 5.1209 |
|  | C | 6.0017 | 6.1613 | 6.0000 |
|  | C | 7.0775 | 5.1075 | 6.0000 |



OCHCHO

| H | 5.5272 | 6.8970 | 5.3120 |
| :--- | :--- | :--- | :--- |
| H | 6.9387 | 4.4871 | 6.8353 |
| C | 5.5410 | 6.0275 | 6.0041 |
| C | 6.8762 | 5.2769 | 6.0564 |
| O | 4.5912 | 5.6744 | 6.6605 |


| O | 7.7716 | 5.5194 | 5.2833 |
| :---: | :---: | :---: | :---: |
| $\mathrm{C}_{2} \mathrm{H}_{5} \mathrm{COOH}$ |  |  |  |
| H | 6.4888 | 4.6500 | 5.1198 |
| H | 6.4854 | 4.6308 | 6.8620 |
| H | 8.6739 | 5.5088 | 6.0065 |
| H | 7.8351 | 6.8018 | 5.1359 |
| H | 7.8298 | 6.7853 | 6.8961 |
| H | 3.3780 | 5.9013 | 6.0120 |
| C | 6.5256 | 5.3026 | 5.9984 |
| C | 7.7918 | 6.1510 | 6.0098 |
| O | 5.2537 | 6.1221 | 6.0040 |
| O | 4.1457 | 5.3092 | 6.0108 |

## $\mathrm{CH}_{3} \mathrm{COOCH}_{3}$

| H | 3.9182 | 5.6801 | 6.9354 |
| :--- | :--- | :--- | :--- |
| H | 3.8746 | 5.5965 | 5.1790 |
| H | 4.0385 | 4.0946 | 6.1217 |
| H | 8.0221 | 6.4186 | 5.0583 |
| H | 8.1238 | 6.3627 | 6.8329 |
| C | 7.7244 | 7.9050 | 6.0136 |
| C | 5.8157 | 5.2683 | 6.0157 |
|  | 4.3130 | 5.1445 | 6.0711 |


|  | 6.1891 | 6.5827 | 6.0595 |
| :---: | :---: | :---: | :---: |
|  | 6.6013 | 4.3518 | 5.9337 |
| $\mathrm{CH}_{3} \mathrm{OCH}_{3}$ |  |  |  |
| H | 7.8506 | 5.6162 | 6.8688 |
| H | 6.6866 | 4.7439 | 5.8339 |
| H | 7.3992 | 6.2828 | 5.2754 |
| H | 4.1428 | 7.2206 | 6.5709 |
| H | 5.1461 | 7.2599 | 5.0948 |
| H | 4.4367 | 5.7189 | 5.6516 |
| C | 7.0352 | 5.7352 | 6.1561 |
| C | 4.8762 | 6.6704 | 5.9823 |
| O | 6.0042 | 6.4547 | 6.8223 |
| $\mathrm{CH}_{3} \mathrm{CHO}$ |  |  |  |
| H | 4.7169 | 5.4698 | 6.7716 |
| H | 4.8623 | 6.6386 | 5.4228 |
| H | 5.2867 | 4.9112 | 5.2094 |
| H | 7.2390 | 5.1702 | 6.8003 |
| C | 5.3047 | 5.7639 | 5.8959 |
| C | 6.7231 | 6.0334 | 6.3183 |
| O | 7.3014 | 7.0852 | 6.1687 |

Empty

| Cu | 2.5955 | 0.0013 | 7.8835 |
| :---: | :---: | :---: | :---: |
| Cu | 5.1900 | 0.0013 | 7.8834 |
| Cu | 9.0830 | 2.2483 | 7.8833 |
| Cu | 3.8928 | 2.2489 | 7.8854 |
| Cu | 6.4879 | 2.2483 | 7.8834 |
| Cu | 10.3805 | 4.4963 | 7.8834 |
| Cu | 5.1904 | 4.4963 | 7.8834 |
| Cu | 7.7854 | 4.4954 | 7.8821 |
| Cu | 1.2975 | 0.7491 | 5.7949 |
| Cu | 3.8926 | 0.7491 | 5.7949 |
| Cu | 6.4877 | 0.7491 | 5.7949 |
| Cu | 2.5951 | 2.9965 | 5.7949 |
| Cu | 5.1902 | 2.9965 | 5.7949 |
| Cu | 7.7852 | 2.9965 | 5.7949 |
| Cu | 3.8926 | 5.2439 | 5.7949 |
| Cu | 6.4877 | 5.2439 | 5.7949 |
| Cu | 9.0828 | 5.2439 | 5.7949 |
| Cu | 2.5951 | 1.4983 | 3.6760 |
| Cu | 5.1902 | 1.4983 | 3.6760 |
| Cu | 7.7852 | 1.4983 | 3.6760 |
| Cu | 3.8926 | 3.7457 | 3.6760 |
| Cu | 6.4877 | 3.7457 | 3.6760 |
| Cu | 9.0828 | 3.7457 | 3.6760 |
| Cu | 5.1902 | 5.9931 | 3.6760 |
| Cu | 7.7852 | 5.9931 | 3.6760 |

$\left.\begin{array}{cccc} & \mathrm{Cu} & 10.3803 & 5.9931\end{array}\right] 3.6760$

|  | Cu | 2.5951 | 1.4983 | 3.6760 |
| :---: | :---: | :---: | :---: | :---: |
|  | Cu | 5.1902 | 1.4983 | 3.6760 |
|  | Cu | 7.7852 | 1.4983 | 3.6760 |
|  | Cu | 3.8926 | 3.7457 | 3.6760 |
|  | Cu | 6.4877 | 3.7457 | 3.6760 |
|  | Cu | 9.0828 | 3.7457 | 3.6760 |
|  | Cu | 5.1902 | 5.9931 | 3.6760 |
|  | Cu | 7.7852 | 5.9931 | 3.6760 |
|  | Cu | 10.3803 | 5.9931 | 3.6760 |
| $\mathrm{CH}_{3}{ }^{*}$ |  |  |  |  |
|  | H | 4.8252 | 2.5275 | 10.3552 |
|  | H | 3.7204 | 1.1325 | 10.2975 |
|  | H | 3.0611 | 2.7857 | 10.3590 |
|  | C | 3.8701 | 2.1634 | 9.9737 |
|  | Cu | 7.7861 | 0.0059 | 7.8358 |
|  | Cu | 6.4728 | 6.7253 | 7.8247 |
|  | Cu | 9.0964 | 6.7217 | 7.8282 |
|  | Cu | 9.0719 | 2.2455 | 7.8316 |
|  | Cu | 3.8914 | 2.2637 | 7.9397 |
|  | Cu | 6.5025 | 2.2486 | 7.8287 |
|  | Cu | 10.3688 | 4.5113 | 7.8302 |
|  | Cu | 5.2024 | 4.5098 | 7.8290 |
|  | Cu | 7.7849 | 4.4932 | 7.8329 |
|  | Cu | 1.2975 | 0.7491 | 5.7949 |


| Cu | 3.8926 | 0.7491 | 5.7949 |
| :--- | :--- | :--- | :--- |
| Cu | 6.4877 | 0.7491 | 5.7949 |
| Cu | 2.5951 | 2.9965 | 5.7949 |
| Cu | 5.1902 | 2.9965 | 5.7949 |
| Cu | 7.7852 | 2.9965 | 5.7949 |
| Cu | 3.8926 | 5.2439 | 5.7949 |
| Cu | 6.4877 | 5.2439 | 5.7949 |
| Cu | 9.0828 | 5.2439 | 5.7949 |
| Cu | 2.5951 | 1.4983 | 3.6760 |
| Cu | 5.1902 | 1.4983 | 3.6760 |
| Cu | 7.7852 | 1.4983 | 3.6760 |
| Cu | 3.8926 | 3.7457 | 3.6760 |
| Cu | 6.4877 | 3.7457 | 3.6760 |
| Cu | 9.0828 | 3.7457 | 3.6760 |
| Cu | 5.1902 | 5.9931 | 3.6760 |
| Cu | 7.7852 | 5.9931 | 3.6760 |
| 10.3803 | 5.9931 | 3.6760 |  |

