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Table 1. Crystal data and structure refinement.

Identification code	2013ncs0027 / CLJ/MA	AB/1.47R
Empirical formula	C ₆ H ₁₈ B ₅ NO ₁₀	
Formula weight	318.26	
Temperature	100(2) K	
Wavelength	0.71075 Å	
Crystal system	Triclinic	
Space group	<i>P</i> -1	
Unit cell dimensions	a = 9.166(4) Å	$\alpha = 64.88(2)^{\circ}$
	b = 9.380(5) Å	$\beta = 75.49(3)^{\circ}$
	c = 9.883(4) Å	$\gamma = 84.73(4)^{\circ}$
Volume	744.7(6) Å ³	,()
Ζ	2	
Density (calculated)	1.419 Mg / m ³	
Absorption coefficient	0.123 mm ⁻¹	
<i>F(000)</i>	332	
Crystal	Plate; Colourless	
Crystal size	$0.230 \times 0.100 \times 0.030$ m	m ³
θ range for data collection	3.081 - 27.478°	
Index ranges	$-11 \le h \le 10, -12 \le k \le 10$	$11, -12 \le l \le 12$
Reflections collected	9366	
Independent reflections	$3355 [R_{int} = 0.0428]$	
Completeness to $\theta = 25.242^{\circ}$	98.8 %	
Absorption correction	Semi-empirical from equ	uivalents
Max. and min. transmission	1.000 and 0.822	
Refinement method	Full-matrix least-squares	s on F^2
Data / restraints / parameters	3355 / 0 / 205	
Goodness-of-fit on F^2	1.084	
Final <i>R</i> indices $[F^2 > 2\sigma(F^2)]$	R1 = 0.0524, wR2 = 0.14	73
<i>R</i> indices (all data)	R1 = 0.0595, wR2 = 0.15	549
Extinction coefficient	n/a	
Largest diff. peak and hole	$0.362 \text{ and } -0.314 \text{ e} \text{\AA}^{-3}$	

Diffractometer: Rigaku AFC12 goniometer equipped with an enhanced sensitivity (HG) Saturn724+ detector mounted at the window of an FR-E+ SuperBright molybdenum rotating anode generator with HF Varimax optics (100µm focus). Cell determination and data collection: CrystalClear-SM Expert 3.1 b18 (Rigaku, 2012). Data reduction, cell refinement and absorption correction: CrystalClear-SM Expert 3.1 b18 (Rigaku, 2012). Structure solution: SHELXS97 (Sheldrick, G.M. (2008). Acta Cryst. A64, 112-122). Structure refinement: SHELXL-2012 (Sheldrick, G.M. (2008). Acta Cryst. A64, 112-122). Graphics: ORTEP3 for Windows (L. J. Farrugia, J. Appl. Crystallogr. 1997, 30, 565

Special details:

All hydrogen atoms were fixed using a standard riding model.

F	'urther	inf	forma	tion:	http:/	/www	soton.	ac.uk/	~xservi	ce/star	t.htm

Table 2. Atomic coordinates $[\times 10^4]$, equivalent isotropic displacement parameters $[Å^2 \times 10^3]$ and site occupancy factors. U_{eq} is defined as one third of the trace of the orthogonalized U^{ij} tensor.

Atom	x	у	Ζ	U_{eq}	S.o.f.	
B1	6938(2)	3895(2)	2483(2)	17(1)	1	
B2	8875(2)	6083(2)	1298(2)	19(1)	1	
B3	6794(2)	6104(2)	3308(2)	17(1)	1	
B4	6694(2)	1029(2)	3283(2)	19(1)	1	
B5	5308(2)	2760(2)	1489(2)	19(1)	1	
01	8372(1)	4691(1)	1446(1)	19(1)	1	
O2	8075(1)	6831(1)	2197(1)	21(1)	1	
O3	6279(1)	4694(1)	3512(1)	18(1)	1	
O4	7230(1)	2264(1)	3408(1)	18(1)	1	
O5	5708(1)	1246(1)	2356(1)	22(1)	1	
O6	5880(1)	4031(1)	1529(1)	19(1)	1	
O7	10177(1)	6802(1)	297(1)	26(1)	1	
08	6099(1)	6863(1)	4204(1)	21(1)	1	
09	7171(1)	-440(1)	4090(1)	24(1)	1	
O10	4350(1)	2916(1)	582(1)	26(1)	1	
C1	736(2)	7738(2)	4036(2)	30(1)	1	
C2	1426(2)	6354(2)	3664(2)	34(1)	1	
C3	2964(2)	6955(3)	2540(3)	41(1)	1	
C4	3144(2)	8612(2)	2425(3)	40(1)	1	
C5	915(2)	9566(2)	1320(2)	31(1)	1	
C6	1417(2)	10572(2)	3065(2)	34(1)	1	
N1	1543(2)	9167(2)	2701(2)	25(1)	1	

$\begin{split} & \text{Bi-Od} & \text{I} 457(2) & \text{Cl}-\text{C2} & \text{I} 135(c) \\ & \text{Bi-O6} & \text{I} 476(2) & \text{Cl}-\text{H1A} & 0.9900 \\ & \text{Bi-O1} & \text{I} 4889(19) & \text{C2}-C3 & \text{I} 159(3) \\ & \text{Bi-O3} & \text{I} 4889(19) & \text{C2}-C3 & \text{I} 159(3) \\ & \text{B2-O7} & \text{I} 359(2) & \text{C2}-\text{H2A} & 0.9900 \\ & \text{B2-O2} & \text{I} 358(2) & \text{C3}-\text{H3A} & 0.9900 \\ & \text{B2-O2} & \text{I} 388(2) & \text{C3}-\text{H3A} & 0.9900 \\ & \text{B3-O8} & \text{I} 365(19) & \text{C3}-\text{H3B} & 0.9900 \\ & \text{B3-O8} & \text{I} 365(2) & \text{C3}-\text{H3B} & 0.9900 \\ & \text{B3-O8} & \text{I} 365(2) & \text{C3}-\text{H3B} & 0.9900 \\ & \text{B3-O2} & \text{I} 384(2) & \text{C4}-\text{H4} & 0.9900 \\ & \text{B4-O4} & \text{I} 362(2) & \text{C4}-\text{H4A} & 0.9900 \\ & \text{B4-O3} & \text{I} 362(2) & \text{C4}-\text{H4A} & 0.9900 \\ & \text{B4-O5} & \text{I} 384(2) & \text{C5}-\text{H5} & 0.9800 \\ & \text{B5-O6} & \text{I} 362(2) & \text{C5}-\text{H5} & 0.9800 \\ & \text{B5-O6} & \text{I} 364(2) & \text{C5}-\text{H5} & 0.9800 \\ & \text{D5}-O5 & \text{I} 384(2) & \text{C5}-\text{H5} & 0.9800 \\ & \text{D5}-O5 & \text{I} 384(2) & \text{C5}-\text{H5} & 0.9800 \\ & \text{D5}-O5 & \text{I} 384(2) & \text{C5}-\text{H5} & 0.9800 \\ & \text{D5}-O5 & \text{I} 384(2) & \text{C5}-\text{H5} & 0.9800 \\ & \text{O1-H1} & 0.8400 & \text{C6}-\text{H6} & 0.9800 \\ & \text{O1-H10} & 0.8400 & \text{C6}-\text{H6} & 0.9800 \\ & \text{O1-H10} & 0.8400 & \text{C6}-\text{H6} & 0.9800 \\ & \text{O1-H10} & 0.8440 & \text{C6}-\text{H6} & 0.9800 \\ & \text{O1-H10} & 0.8440 & \text{C6}-\text{H6} & 0.9800 \\ & \text{O1-B1-O3} & 109.29(13) & \text{C3}-\text{C2}-\text{H2} & 110.5 \\ & \text{O4}=\text{B1}-O1 & 109.18(13) & \text{C3}-\text{C2}-\text{H2} & 110.5 \\ & \text{O4}=\text{B1}-O1 & 109.18(13) & \text{C3}-\text{C2}-\text{H2} & 110.5 \\ & \text{O4}=\text{B1}-O1 & 109.8(413) & \text{C1}-\text{C2}-\text{H2} & 110.5 \\ & \text{O4}=\text{B1}-O1 & 109.8(413) & \text{C1}-\text{C2}-\text{H2} & 110.8 \\ & \text{O1}=\text{B2}-O2 & 12.66(14) & \text{C4}-\text{C3}-\text{H3} & 110.8 \\ & \text{O1}=\text{B2}-O2 & 12.66(14) & \text{C4}-\text{C3}-\text{H3} & 110.8 \\ & \text{O1}=\text{B2}-O2 & 12.66(14) & \text{C4}-\text{C3}-\text{H3} & 110.8 \\ & \text{O1}=\text{B2}-O2 & 116.50(13) & \text{C2}-\text{C3}-\text{H3} & 110.8 \\ & \text{O1}=\text{B2}-O2 & 116.50(13) & \text{C2}-\text{C3}-\text{H3} & 110.8 \\ & \text{O1}=\text{B2}-O2 & 116.50(13) & \text{C3}-\text{C3}-\text{H3} & 110.8 \\ & \text{O1}=\text{B2}-O2 & 116.50(13) & \text{C3}-\text{C3}-\text{H3} & 110.8 \\ & \text{O1}=\text{B2}-O5 & 12.054(14) & \text{N}-\text{C4}-\text{H4} & 111.0 \\ & \text{O1}=\text{B}-O5 &$				
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	B1-O4	1.452(2)	C1–C2	1.535(3)
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	B1-O6	1.476(2)	C1–H1A	0.9900
BI-O3 $1.489(19)$ $C2-C3$ $1.539(2)$ $B2-O1$ $1.359(2)$ $C2+B2A$ 0.9900 $B2-O2$ $1.388(2)$ $C3-C4$ $1.511(3)$ $B3-O3$ $1.362(2)$ $C3+H3A$ 0.9900 $B3-O2$ $1.384(2)$ $C4-H3A$ 0.9900 $B3-O2$ $1.384(2)$ $C4-H4A$ 0.9900 $B4-O3$ $1.362(2)$ $C4-H4B$ 0.9900 $B4-O5$ $1.384(2)$ $C5-H5A$ 0.9800 $B5-O6$ $1.362(2)$ $C5-H5A$ 0.9800 $B5-O5$ $1.384(2)$ $C5-H5C$ 0.9800 $D5-D5$ $1.384(2)$ $C5-H5C$ 0.9800 $O7-H7$ 0.8400 $C6-H6B$ 0.9800 $O1-H10$ 0.8400 $C6-H6B$ 0.9800 $O1-H10$ 0.8400 $C6-H6B$ 0.9800 $O1-H10$ 0.8400 $C4-H6C$ 0.9800 $O1-H10$ 0.8400 $C4-H6C$ 0.9800 $O1-B1-O3$ $0.929(13)$ </td <td>B1-O1</td> <td>1.480(2)</td> <td>C1–H1B</td> <td>0.9900</td>	B1-O1	1.480(2)	C1–H1B	0.9900
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	B1–O3	1.4889(19)	C2–C3	1.539(3)
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	B2-O7	1.359(2)	C2–H2A	0.9900
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	B2-01	1.361(2)	C2–H2B	0.9900
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	B2-02	1 388(2)	C3-C4	1 531(3)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	B3-03	1.362(2)	C3–H3A	0.9900
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	B3-08	1 3655(19)	C3-H3B	0.9900
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	B3-02	1 384(2)	C4-N1	1 509(2)
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	B3-02 B4-04	1.367(2)	C4–H4A	0.9900
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	B4-09	1.362(2)	C4–H4B	0.9900
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	B4-05	1.302(2) 1.386(2)	C5–N1	1 501(2)
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	B5-010	1.360(2)	C5-H5A	0.9800
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	B5-06	1.365(2)	C5_H5R	0.9800
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	B5_05	1.303(2) 1.384(2)	C5_H5C	0.9800
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	07 H7	0.8400	C6 N1	1.405(2)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		0.8400	C6 H6A	0.0200
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	08-118	0.8400	C6 H6P	0.9800
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	010 410	0.8400		0.9800
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		0.8400	Со-пос	0.9800
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	CI-INI	1.509(2)		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	04-B1-06	111.94(12)	С1_С2_Н2А	110.5
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	04 - B1 - 00	111.94(12) 100.18(12)	$C_1 - C_2 - H_2 A$	110.5
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	04-BI-01	109.10(13) 109.14(12)	$C_3 - C_2 - H_2 A$	110.5
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	06-B1-01 04 B1 02	108.14(13) 100.20(12)	C1 - C2 - H2B	110.5
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	04-B1-03	109.29(13)	$C_3 - C_2 - H_2 B$	110.5
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	06-B1-03	108.59(12)	$H_2A - C_2 - H_2B$	108.7
$\begin{array}{llllllllllllllllllllllllllllllllllll$	01-81-03	109.68(12)	C4 - C3 - C2	104.68(17)
$\begin{array}{llllllllllllllllllllllllllllllllllll$	07-B2-01	122.66(14)	C4-C3-H3A	110.8
$\begin{array}{llllllllllllllllllllllllllllllllllll$	07-B2-02	116.50(13)	$C_2 - C_3 - H_3 A$	110.8
$\begin{array}{llllllllllllllllllllllllllllllllllll$	01-B2-02	120.83(14)	C4-C3-H3B	110.8
$\begin{array}{llllllllllllllllllllllllllllllllllll$	03-B3-08	122.11(14)	$C_2 - C_3 - H_3 B$	110.8
$\begin{array}{llllllllllllllllllllllllllllllllllll$	03-B3-02	121.53(14)	H3A-C3-H3B	108.9
$\begin{array}{llllllllllllllllllllllllllllllllllll$	08-B3-02	116.34(13)	NI-C4-C3	103.60(15)
$\begin{array}{llllllllllllllllllllllllllllllllllll$	04-B4-09	117.83(14)	NI-C4-H4A	111.0
$\begin{array}{llllllllllllllllllllllllllllllllllll$	04-B4-05	121.63(15)	C3–C4–H4A	111.0
$\begin{array}{llllllllllllllllllllllllllllllllllll$	09–B4–O5	120.54(14)	NI-C4-H4B	111.0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	O10-B5-O6	122.13(15)	C3–C4–H4B	111.0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	O10-B5-O5	117.00(14)	H4A–C4–H4B	109.0
$\begin{array}{llllllllllllllllllllllllllllllllllll$	O6–B5–O5	120.86(14)	N1–C5–H5A	109.5
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	B2-O1-B1	124.40(12)	N1–C5–H5B	109.5
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	B3-O2-B2	119.14(12)	H5A-C5-H5B	109.5
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	B3-O3-B1	123.44(12)	N1–C5–H5C	109.5
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	B4-O4-B1	123.03(13)	H5A-C5-H5C	109.5
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	B5-O5-B4	119.09(13)	H5B-C5-H5C	109.5
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	B5-O6-B1	123.19(12)	N1–C6–H6A	109.5
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	В2-07-Н7	109.5	N1-C6-H6B	109.5
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	В3-О8-Н8	109.5	H6A-C6-H6B	109.5
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	В4О9Н9	109.5	N1-C6-H6C	109.5
$\begin{array}{cccccc} N1-C1-C2 & 103.90(15) & H6B-C6-H6C & 109.5 \\ N1-C1-H1A & 111.0 & C6-N1-C5 & 108.81(14) \\ C2-C1-H1A & 111.0 & C6-N1-C4 & 112.50(14) \\ N1-C1-H1B & 111.0 & C5-N1-C4 & 110.51(15) \\ C2-C1-H1B & 111.0 & C6-N1-C1 & 112.22(14) \\ H1A-C1-H1B & 109.0 & C5-N1-C1 & 110.19(13) \\ C1-C2-C3 & 106.01(16) & C4-N1-C1 & 102.51(14) \\ \end{array}$	B5-O10-H10	109.5	H6A-C6-H6C	109.5
N1-C1-H1A111.0C6-N1-C5108.81(14)C2-C1-H1A111.0C6-N1-C4112.50(14)N1-C1-H1B111.0C5-N1-C4110.51(15)C2-C1-H1B111.0C6-N1-C1112.22(14)H1A-C1-H1B109.0C5-N1-C1110.19(13)C1-C2-C3106.01(16)C4-N1-C1102.51(14)	N1-C1-C2	103.90(15)	H6B-C6-H6C	109.5
C2-C1-H1A111.0C6-N1-C4112.50(14)N1-C1-H1B111.0C5-N1-C4110.51(15)C2-C1-H1B111.0C6-N1-C1112.22(14)H1A-C1-H1B109.0C5-N1-C1110.19(13)C1-C2-C3106.01(16)C4-N1-C1102.51(14)	N1-C1-H1A	111.0	C6-N1-C5	108.81(14)
N1-C1-H1B111.0C5-N1-C4110.51(15)C2-C1-H1B111.0C6-N1-C1112.22(14)H1A-C1-H1B109.0C5-N1-C1110.19(13)C1-C2-C3106.01(16)C4-N1-C1102.51(14)	C2-C1-H1A	111.0	C6-N1-C4	112.50(14)
C2-C1-H1B111.0C6-N1-C1112.22(14)H1A-C1-H1B109.0C5-N1-C1110.19(13)C1-C2-C3106.01(16)C4-N1-C1102.51(14)	N1-C1-H1B	111.0	C5-N1-C4	110.51(15)
H1A-C1-H1B109.0C5-N1-C1110.19(13)C1-C2-C3106.01(16)C4-N1-C1102.51(14)	C2-C1-H1B	111.0	C6-N1-C1	112.22(14)
C1-C2-C3 106.01(16) C4-N1-C1 102.51(14)	H1A-C1-H1B	109.0	C5-N1-C1	110.19(13)
	C1-C2-C3	106.01(16)	C4-N1-C1	102.51(14)

Table 3. Bond lengths [Å] and angles [°].

Symmetry transformations used to generate equivalent atoms:

Table 4. Anisotropic displacement parameters $[Å^2 \times 10^3]$. The anisotropic disp	lacement
factor exponent takes the form: $-2\pi^{2}[h^{2}a^{*2}U^{1}] + + 2hka^{*}h^{*}U^{12}]$	

Atom	U^{11}	U^{22}	U^{33}	U^{23}	U^{13}	U^{12}	
B1	17(1)	16(1)	21(1)	-9(1)	-6(1)	-2(1)	
B2	18(1)	20(1)	22(1)	-10(1)	-6(1)	-1(1)	
B3	17(1)	16(1)	19(1)	-7(1)	-6(1)	-1(1)	
B4	16(1)	20(1)	23(1)	-10(1)	-5(1)	-1(1)	
B5	16(1)	20(1)	23(1)	-9(1)	-7(1)	-2(1)	
01	17(1)	19(1)	24(1)	-12(1)	-2(1)	-3(1)	
02	21(1)	19(1)	26(1)	-13(1)	-1(1)	-5(1)	
03	18(1)	17(1)	20(1)	-9(1)	-3(1)	-3(1)	
04	20(1)	16(1)	24(1)	-9(1)	-10(1)	-1(1)	
05	25(1)	17(1)	29(1)	-8(1)	-15(1)	-2(1)	
06	20(1)	17(1)	22(1)	-8(1)	-9(1)	0(1)	
07	23(1)	25(1)	31(1)	-18(1)	4(1)	-8(1)	
08	20(1)	19(1)	25(1)	-12(1)	0(1)	-5(1)	
09	28(1)	16(1)	33(1)	-11(1)	-17(1)	0(1)	
010	29(1)	21(1)	32(1)	-6(1)	-18(1)	-3(1)	
C1	28(1)	31(1)	29(1)	-7(1)	-11(1)	-4(1)	
C2	34(1)	33(1)	38(1)	-10(1)	-19(1)	2(1)	
C3	31(1)	47(1)	47(1)	-20(1)	-13(1)	9(1)	
C4	18(1)	45(1)	53(1)	-16(1)	-7(1)	-2(1)	
C5	40(1)	30(1)	28(1)	-12(1)	-15(1)	-2(1)	
C6	42(1)	33(1)	35(1)	-18(1)	-16(1)	-5(1)	
N1	21(1)	28(1)	29(1)	-12(1)	-10(1)	-2(1)	

Table 5. Hydrogen coordinates [$\times 10^4$] and isotropic displacement parameters [Å ² × 10 ³].	

Atom	x	У	Z	U_{eq}	S.o.f.	
H7	10564	6278	-210	38	1	
H8	5371	6309	4877	32	1	
H9	6754	-1105	3943	35	1	
H10	4269	3875	22	40	1	
H1A	-363	7789	4107	36	1	
H1B	916	7643	5017	36	1	
H2A	769	6029	3184	41	1	
H2B	1555	5442	4611	41	1	
H3A	3784	6268	2940	50	1	
H3B	2976	6990	1522	50	1	
H4A	3645	8582	3215	48	1	
H4B	3737	9306	1395	48	1	
H5A	920	8628	1119	47	1	
H5B	1535	10400	425	47	1	
H5C	-121	9930	1515	47	1	
H6A	1967	11465	2175	50	1	
H6B	1847	10332	3950	50	1	
H6C	353	10839	3310	50	1	

O7-B2-O1-B1	-177.89(14)
O2-B2-O1-B1	3.1(2)
O4-B1-O1-B2	-129.34(15)
O6-B1-O1-B2	108.65(15)
O3-B1-O1-B2	-9.6(2)
O3-B3-O2-B2	-1.8(2)
O8–B3–O2–B2	176.93(14)
O7–B2–O2–B3	-175.70(14)
O1-B2-O2-B3	3.4(2)
O8-B3-O3-B1	175.13(14)
O2-B3-O3-B1	-6.2(2)
O4-B1-O3-B3	130.75(14)
O6-B1-O3-B3	-106.88(15)
O1-B1-O3-B3	11.1(2)
O9-B4-O4-B1	173.14(12)
O5-B4-O4-B1	-6.1(2)
O6-B1-O4-B4	5.79(19)
O1-B1-O4-B4	-113.90(15)
O3-B1-O4-B4	126.14(14)
O10-B5-O5-B4	179.28(13)
O6-B5-O5-B4	0.6(2)
O4-B4-O5-B5	2.6(2)
O9–B4–O5–B5	-176.65(13)
O10-B5-O6-B1	-178.99(13)
O5-B5-O6-B1	-0.4(2)
O4-B1-O6-B5	-2.59(19)
O1-B1-O6-B5	117.72(15)
O3-B1-O6-B5	-123.34(14)
N1-C1-C2-C3	21.94(19)
C1-C2-C3-C4	4.6(2)
C2-C3-C4-N1	-29.5(2)
C3-C4-N1-C6	164.32(16)
C3-C4-N1-C5	-73.84(19)
C3-C4-N1-C1	43.57(19)
C2-C1-N1-C6	-161.33(14)
C2-C1-N1-C5	77.25(17)
C2-C1-N1-C4	-40.40(17)

Symmetry transformations used to generate equivalent atoms:

Table 7	TTdua a au	الم مع ما م	гå	J	oп	
Table 7.	Hydrogen	bonds	A	and	۲I	•

$D-\mathrm{H}\cdots A$	d(D-H)	$d(\mathbf{H}\cdots A)$	$d(D \cdots A)$	$\angle(DHA)$			
07–H7…O1 ⁱ	0.84	1.86	2.6933(18)	172.5			
O8-H8O3 ⁱⁱ	0.84	1.87	2.702(2)	171.4			
O9–H9…O8 ⁱⁱⁱ	0.84	1.94	2.746(2)	159.6			
O10-H10-06iv	0.84	1.93	2.763(2)	170.7			
C1-H1B····O4 ⁱⁱ	0.99	2.60	3.495(2)	149.6			
Symmetry transformations used to generate equivalent atoms:							
i) -x+2, -y+1, -z (ii) $-x+1, -y+1, -z+1$ (iii) $x, y-1, z$							

(iv) -x+1, -y+1, -z

