

Supplemental information

Initial estimates for the film mass transport coefficient (k_f) were based on the Gnielinski correlation²³:

$$k_f = \frac{[1 + 1.5(1 - \varepsilon)] \times D_l}{d_p} \times \left(2 + 0.644 \times \text{Re}^{1/2} \times \text{Sc}^{1/3} \right) \quad (\text{Equation S.1})$$

$$\text{Re} = \frac{\rho_l \times \Phi \times d_p \times v_l}{\varepsilon \times \mu_l} \quad (\text{Equation S.2})$$

$$\text{Sc} = \frac{\mu_l}{\rho_l \times D_l} \quad (\text{Equation S.3})$$

Constraints: $\text{Re} \times \text{Sc} > 500$; $0.6 \leq \text{Sc} \leq 10^4$; $1 \leq \text{Re} < 100$; $0.26 < \varepsilon < 0.935$

where $k_f \equiv$ the film mass transport coefficient (calculated $k_f \approx 4.36 \times 10^{-3} \text{ m s}^{-1}$ for arsenate and $k_f \approx 5.23 \times 10^{-3} \text{ m s}^{-1}$ for nitrate); Re is the Reynolds number (unitless); Sc is the Schmidt number (unitless); d_p is the adsorbent particle diameter ($d_p = 0.700 \times 10^{-3} \text{ m}$); D_l is the free liquid diffusivity for arsenate or nitrate ($D_{l-As} = 9.05 \times 10^{-10} \text{ m}^2 \text{ s}^{-1}$; $D_{l-NO_3} = 1.90 \times 10^{-9} \text{ m}^2 \text{ s}^{-1}$)^{38, 39}; ε is the bed void fraction ($\varepsilon = 0.634$); μ_l is the dynamic viscosity of water at 20 °C ($1.002 \times 10^{-3} \text{ N s m}^{-2}$); ρ_l is the density of water at 20 °C ($\rho_l = 998.2 \text{ kg m}^{-3}$); Φ is the sphericity of the particle ($\Phi = 1$); and v_l is the liquid superficial velocity ($v_l \approx 0.00208 \text{ m s}^{-1}$).

Considering that the material was very porous (the particle porosity $\varepsilon_p \approx 0.75$), the impact of surface diffusion was assumed to be negligible. As suggested by Sontheimer et al.³⁸, the pore diffusion coefficient was estimated using Equation S.4:

$$D_p = \frac{\varepsilon_p \times D_l}{\tau} \quad (\text{Equation S.4})$$

The tortuosity was estimated using the correlation suggested by Mackie and Meares (Equation S.5) for electrolyte solutions⁴⁰:

$$\tau = \frac{(2 - \varepsilon_p)^2}{\varepsilon_p} \quad (\text{Equation S.5})$$

where τ is the tortuosity factor and ε_p is the particle porosity ($\varepsilon_p \approx 0.75$). The estimated tortuosity value was $\tau \approx 2.1$. The estimated value for the pore diffusion coefficients were $D_{P-As} \approx 3.5 \times 10^{-6} \text{ cm}^2 \text{ s}^{-1}$ for arsenate and $D_{P-NO_3} \approx 6.85 \times 10^{-6} \text{ cm}^2 \text{ s}^{-1}$.

The model breakthrough predictions were compared with the experimental data. Correlations between the model predictions and experimental data characterized by $R^2 > 0.9$ were considered to be sufficient for hypothesis validation.

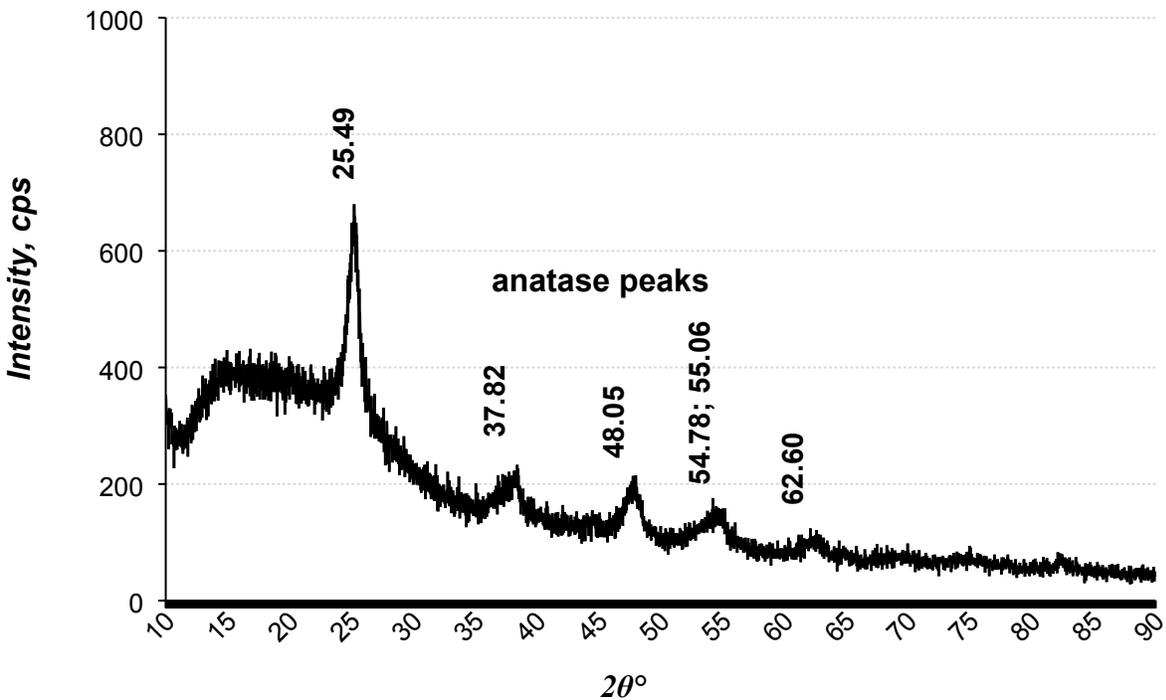


Figure S1. X-ray diffraction peaks indicate existence of anatase crystalline structure of the synthesized titanium dioxide nanoparticles within the hybrid ion-exchange media.

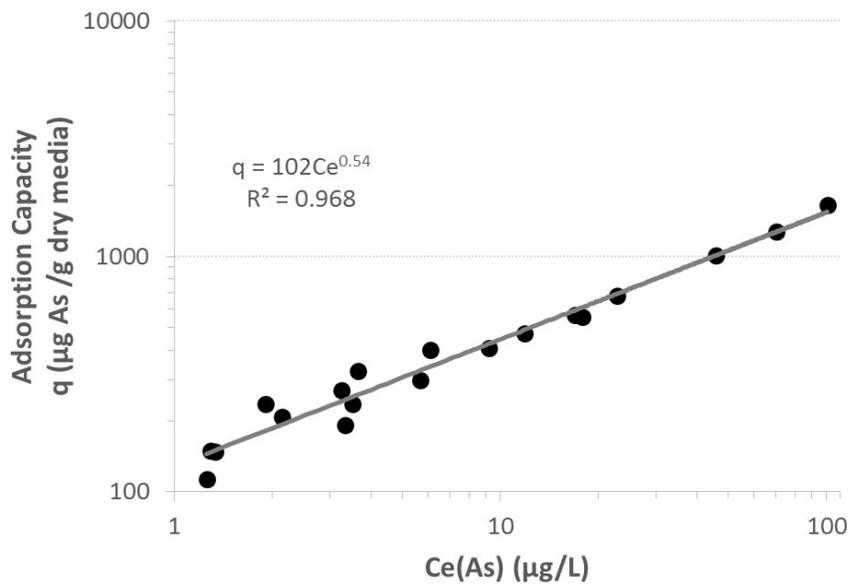


Figure S2. Arsenic sorption isotherms for the Ti-HIX media in 5 mM NaHCHO_3 buffered ultrapure water at final $\text{pH} = 7.2 \pm 0.3$ and contact time of 3 days ;($C_0 \approx 108 \mu\text{g L}^{-1} \text{As}$)

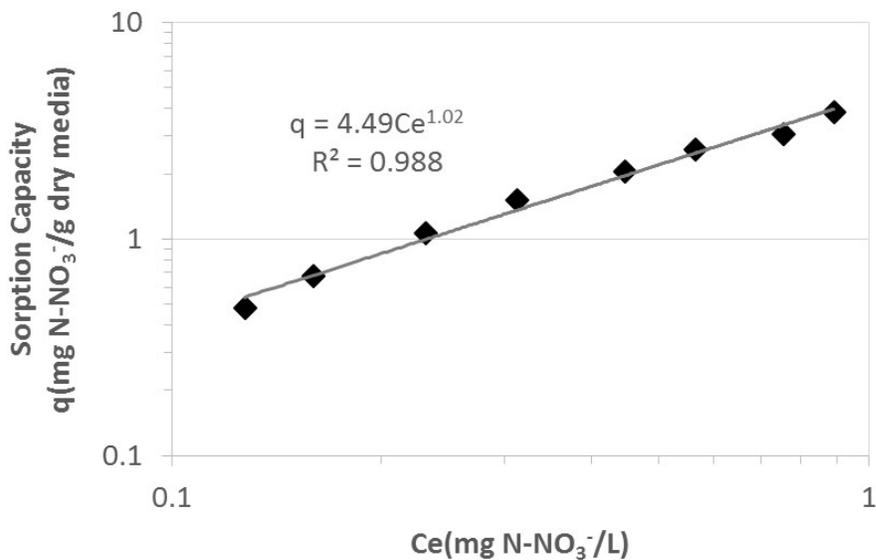


Figure S3. Nitrate sorption isotherms for the Ti-HIX media in 5 mM NaHCHO_3 buffered ultrapure water at final $\text{pH} = 7.2 \pm 0.3$ and contact time of 3 days; ($C_0 \approx 1.1 \text{ mg L}^{-1} \text{N-NO}_3^-$).

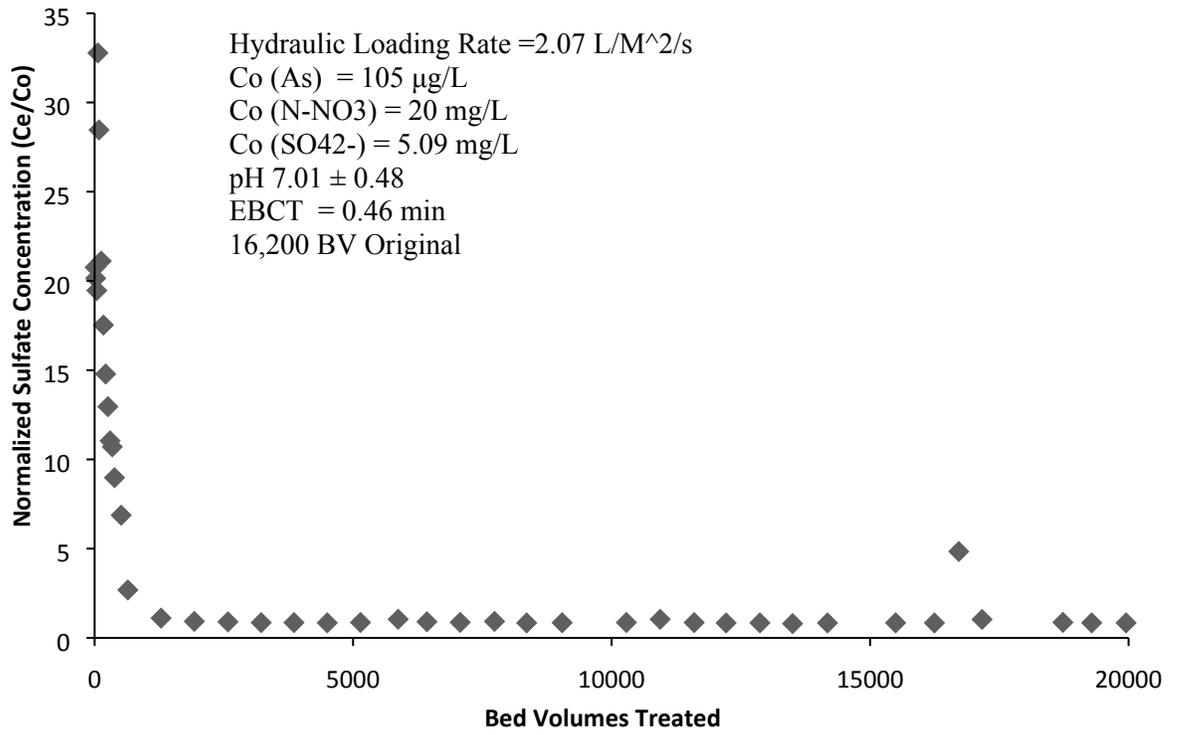


Figure S4. Sulfate breakthrough curves for titanium dioxide nanomaterial-enhanced hybrid ion exchange media under continuous flow regime.