SUPPORTING INFORMATION

Microbial Fuel Cells with Separate Brush-Anode and Integrated-Spacer Dual Cathode Modules

Weihua He^a, Xiaoyuan Zhang^{b, c}, Jia Liu^{a, b}, Xiuping Zhu^b, Yujie Feng^a*, Bruce E. Logan^{a,b}*

 ^a State Key Laboratory of Urban Water Resource and Environment, Harbin Institute of Technology, No.73 Huanghe Road, Nangang District, Harbin 150090, P.R.China
^b Department of Civil & Environmental Engineering, Penn State University, 231Q Sackett Building, University Park, PA 16802, USA
^c State Key Joint Laboratory of Environment Simulation and Pollution Control, School of Environment, Tsinghua University, Beijing 100084, P.R.China

*Corresponding authors. Address: State Key Laboratory of Urban Water Resource

and Environment, No. 73 Huanghe Road, Nangang District, Harbin 150090, China.

Tel.: +86 451 86287017; fax: +86 451 86287017 (Y. Feng), tel.: +1 814 863 7908

(B.E. Logan).

E-mail addresses: <u>yujief@hit.edu.cn</u> (Y. Feng), <u>blogan@psu.edu</u> (B.E. Logan).



Figure S1. (a) Photograph and (b) schematic diagram of the air cathode modular MFC, showing the relative position of the dual-sided cathode cassette and the reference electrode placement.





Figure S2. (a) Photograph of cathode cassette with mesh spacers, (b) schematic showing dimensions of the column spacer, (c) the position of washers in the wire spacers, and (d) the dilute hydrochloric acid cleaned cathode module after wastewater operation.

Assembly explanation: In Figure S2c, two nylon washers (McMaster-Carr, standard washer, M5, off-white) with a thickness of 1.0 ± 0.2 mm were added at each screw hole between two rectangle frames on the top edge and passed through by screws. The nylon washers stabilized the structure and left air diffusion slit with a width of 2 mm.



Figure S3. (a) Cell voltage, and (b) COD removal and columbic efficiency of the MFC stack in fed batch mode during startup using acetate amended wastewater





Figure S4. Examples of the Nyquist plats for (a) the whole-cell, and (b) anode impedance of the MFC stack using acetate amended domestic wastewater, and (c) example of anode impedance of the MFC stack in the batch mode using original wastewater.



Figure S5. Polarization curve of the anode brushes in the MFC stacks, operated in fed batch mode, using domestic wastewater, for sides A and B.



Figure S6. Cell voltage and anode potentials of the MFC module in fed batch mode with an external resistance of 1.5Ω , using domestic wastewater.





Figure S7. The voltage generated by the anodes of (a) compartment A, and (b) compartment B in the MFCs in fed batch mode, and (c) in continuous mode (HRT = 8 h) using domestic wastewater. The voltage data of the MFC stack were obtained with the anode separately connected with cathode separately with an external resistance of 30 Ω .



Figure S8. Columbic efficiencies in continuous flow mode measured using different external resistances.

Data explanation: The columbic efficiency (CE) is the ratio of the total coulombs transferred through the external circuit divided by the theoretical amount of coulombs for the measured change in COD. Higher CE indicated a higher percentage of substrate was removed with current generation. The CE of the MFC stack in continuous flow mode was up to $41 \pm 2\%$, which was among the highest CEs recorded in scaled up reactor for domestic wastewater in air–cathode MFCs, consistent with CEs increasing when current and power densities are increased.



Figure S9. Photographs of the MFC module fed domestic wastewater that was used to power a fan or charge an AT&T cellphone.

Whole-Cell resistance	Mesh Spacer					
R1 (Ω)	1.065	1.032	0.7965	0.7776		
R2 (Ω)	0.555	0.5821	0.9412	0.7067		
Rd2 (Ω)	0.1118	0.07295	0.06579	0.07489		
R3 (Ω)	0.9654	1.046	0.8644	0.88		
$\mathrm{TR}\left(\Omega\right)$	2.6972	2.73305	2.66789	2.43919		
Whole-Cell resistance	Column Spacer					
R1 (Ω)	1.061	1.02	1.091	1.049		
R2 (Ω)	0.7926	0.1736	0.626	0.5882		
Rd2 (Ω)	0.01986	0.09781	0.2784	0.302		
R3 (Ω)	0.1781	0.7734	0.0741	0.06277		
$\mathrm{TR}\left(\Omega\right)$	2.05156	2.06481	2.0695	2.00197		
Whole-Cell resistance	Wire Spacer					
R1 (Ω)	1.018	0.9892	1.118	1.097		
R2 (Ω)	0.5152	0.532	0.0415	0.0577		
Rd2 (Ω)	0.222	0.2249	0.08482	0.07123		
R3 (Ω)	0.1091	0.05583	0.9034	0.7717		
$\mathrm{TR}\left(\Omega\right)$	1.8643	1.80193	2.14772	1.99763		

Table S1: Simulation of whole-cell impedance changes of the MFC stack by using

three kinds of spacers with acetate amended wastewater.

Anode Resistance	Mesh Spacer					
R1 (Ω)	0.1161	0.1159	0.06752	0.0672		
R2 (Ω)	0.241	0.2643	0.3171	0.3328		
$\mathrm{TR}\left(\Omega\right)$	0.3571	0.3802	0.38462	0.4		
Anode Resistance	Column Spacer					
R1 (Ω)	0.1526	0.1695	0.2288	0.2196		
R2 (Ω)	0.3311	0.3212	0.4117	0.3725		
$\mathrm{TR}\left(\Omega\right)$	0.4837	0.4907	0.6405	0.5921		
Anode Resistance	Wire Spacer					
R1	0.1928	0.195	0.09618	0.09558		
R2	0.1872	0.191	0.2278	0.2124		
TR	0.38	0.386	0.32398	0.30798		

Table S2: Simulation of anode impedance changes of the MFC stack by using three kinds of spacers with acetate amended wastewater.

Anode Resistance	Т	T1		T2		Т3	
R1 (Ω)	0.2136	0.1789	0.2358	0.1673	0.222	0.1647	
R2 (Ω)	0.56	0.647	0.4264	0.595	0.4788	0.5482	
$\mathrm{TR}\left(\Omega\right)$	0.7736	0.8259	0.6622	0.7623	0.7008	0.7129	

Table S3: Simulation of anode impedance of the MFC stack in the batch mode using original domestic wastewater.

Anode Resistance	T4		Т5		Т6	
R1 (Ω)	0.2137	0.1627	0.2378	0.1626	0.2276	0.1619
R2 (Ω)	0.5194	0.7217	0.6495	0.93	1.383	1.85
$\mathrm{TR}\left(\Omega\right)$	0.7331	0.8844	0.8873	1.0926	1.6106	2.0119