

Electronic Supporting Information

Support Effects in Rare Earth Element Separation Using Diglycolamide-Functionalized Mesoporous Silica

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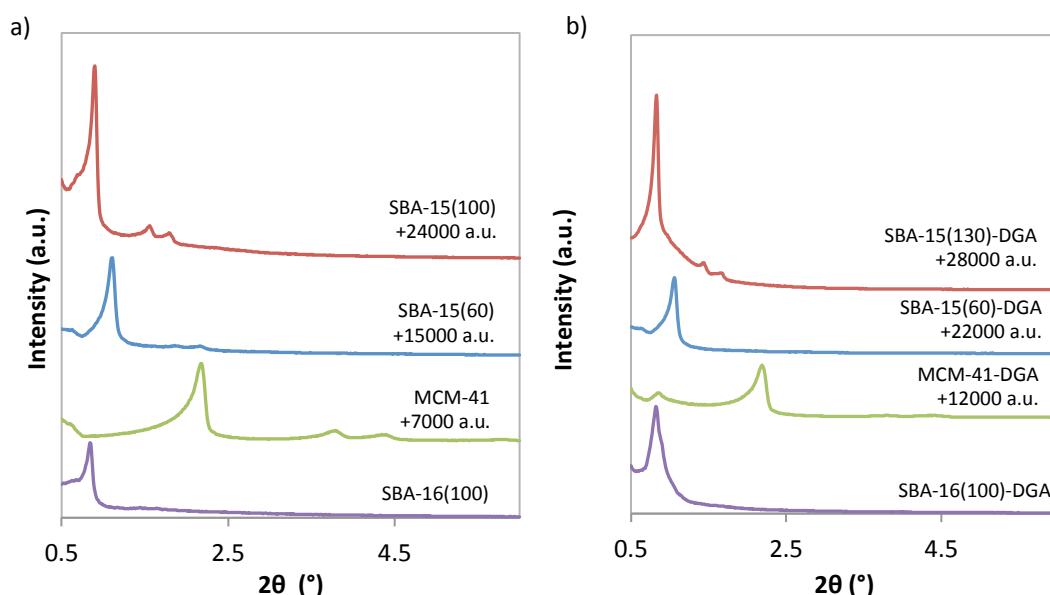


Figure S1: Low angle powder XRD patterns of a) the pure; b) the functionalized materials.

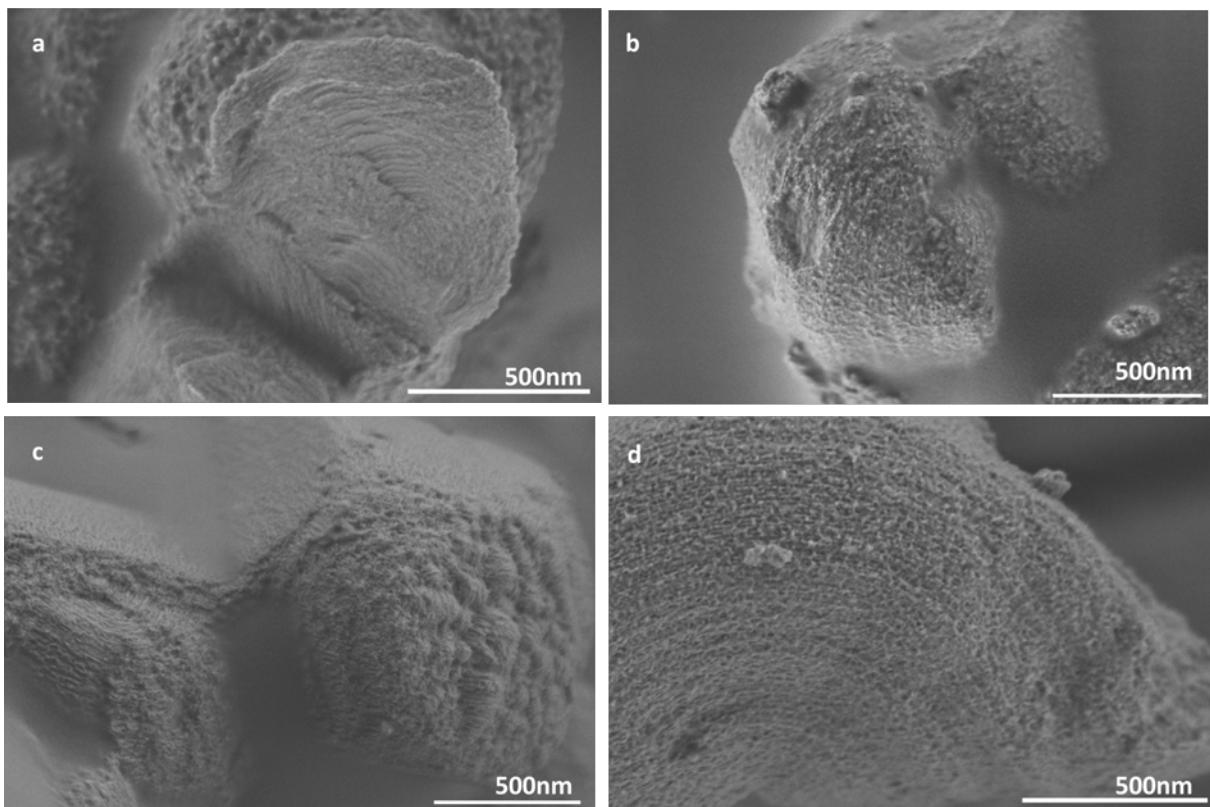


Figure S2: Representative HRSEM images of MCM-41-DGA (a), SBA-15(60)-DGA (b) and SBA-15(100)-DGA (c, d).

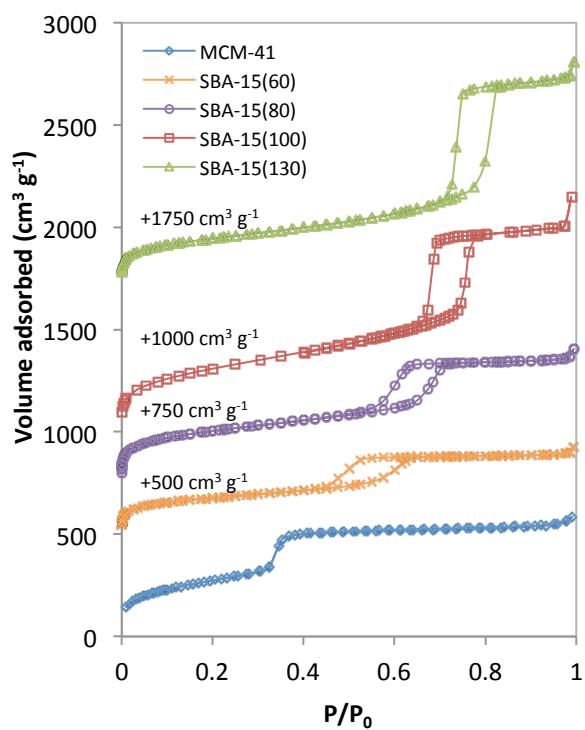


Figure S3: N₂ sorption isotherms (-196°C) of the pure SBA-15 materials aged at different temperatures and MCM-41, as indicated.

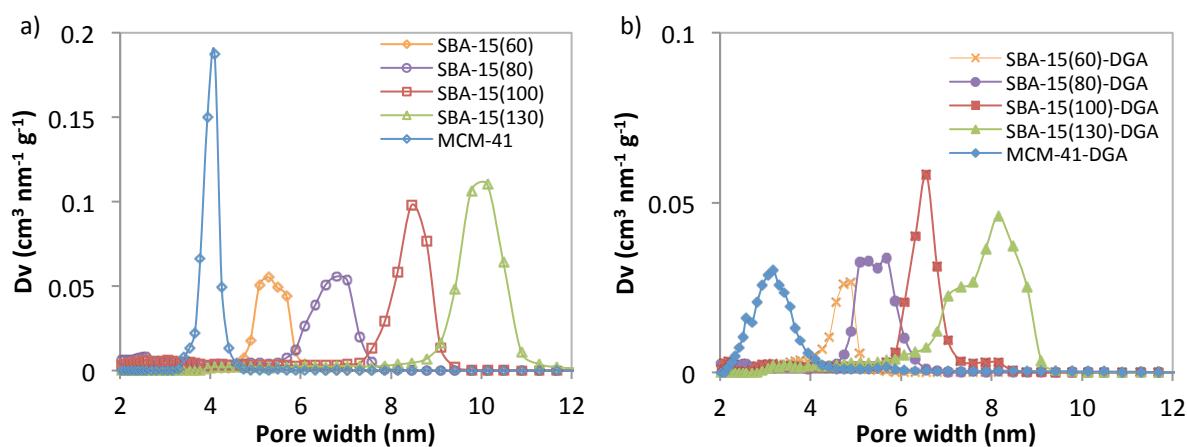


Figure S4: NLDFT pore size distributions calculated from the desorption branch for cylindrical pore model of a) the pure SBA-15 and MCM-41 materials b) the corresponding grafted silica materials.

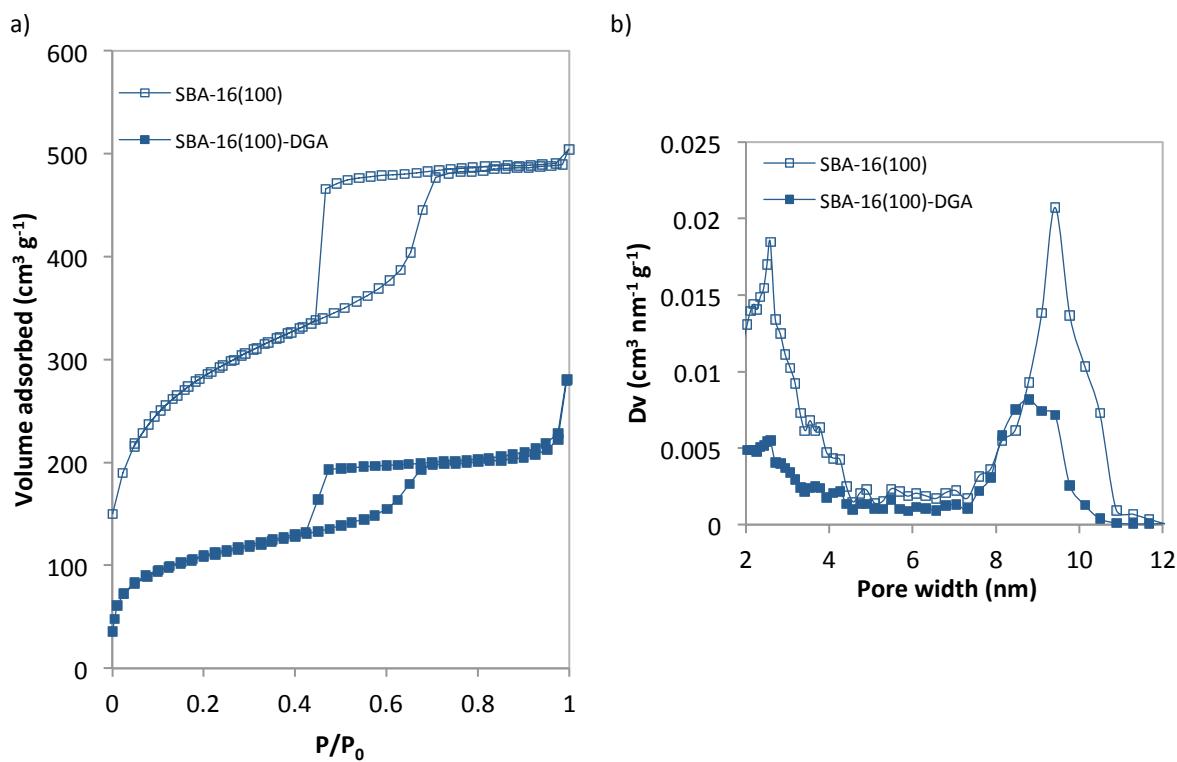


Figure S5: a) N_2 physisorption isotherms of pure SBA-16 and the corresponding grafted SBA-16-DGA measured at -196°C . b) NLDFT pore size distributions of SBA-16 and SBA-16-DGA calculated from the adsorption branch for spherical pore model.

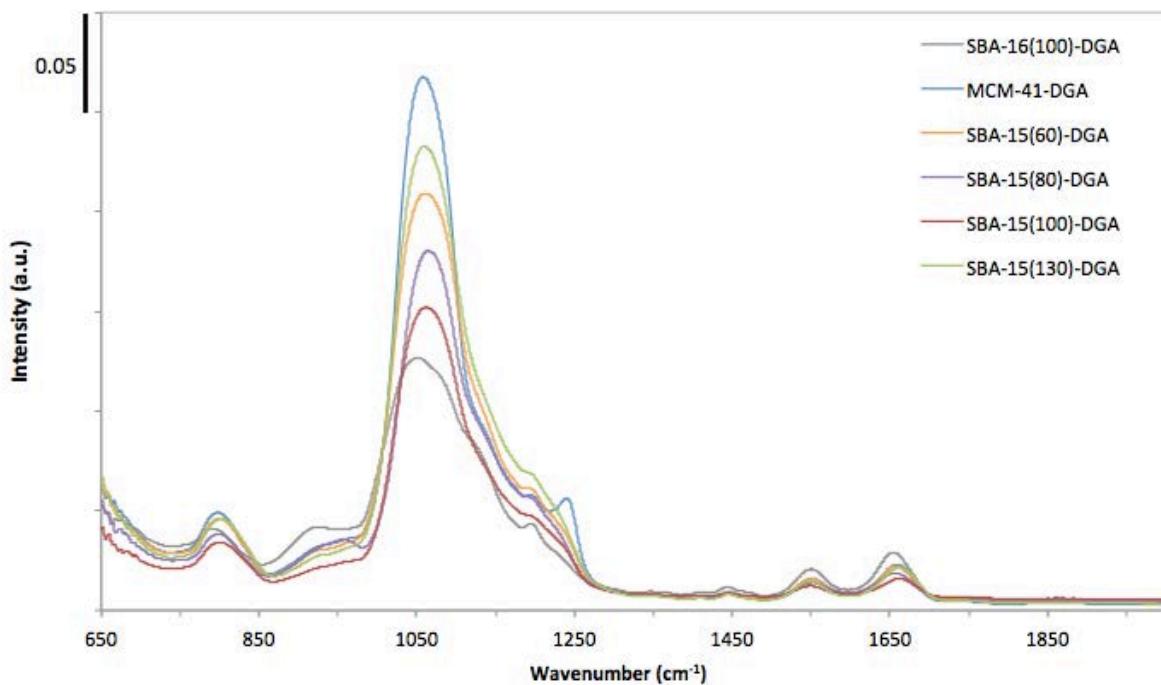


Figure S6: IR spectra of all the DGA-functionalized samples.

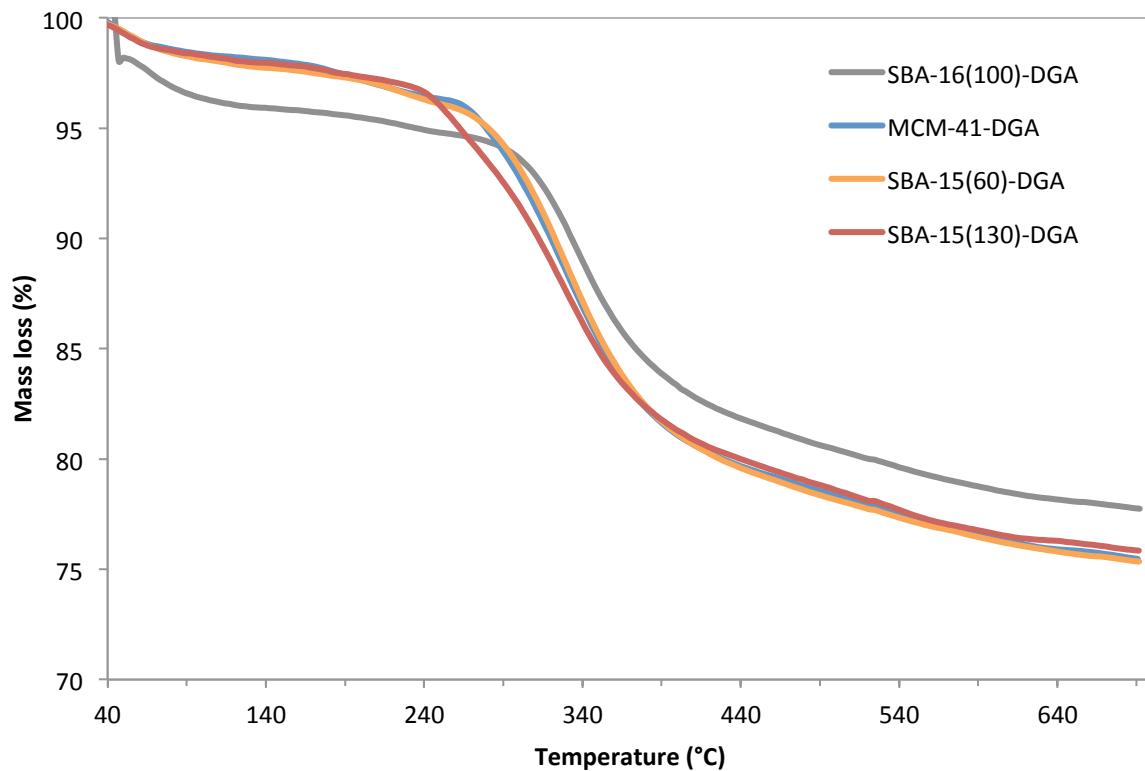


Figure S7: Mass loss profiles obtained from the TGA analysis with the air flow 40 mL min^{-1} for the representative DGA functionalized silica materials.

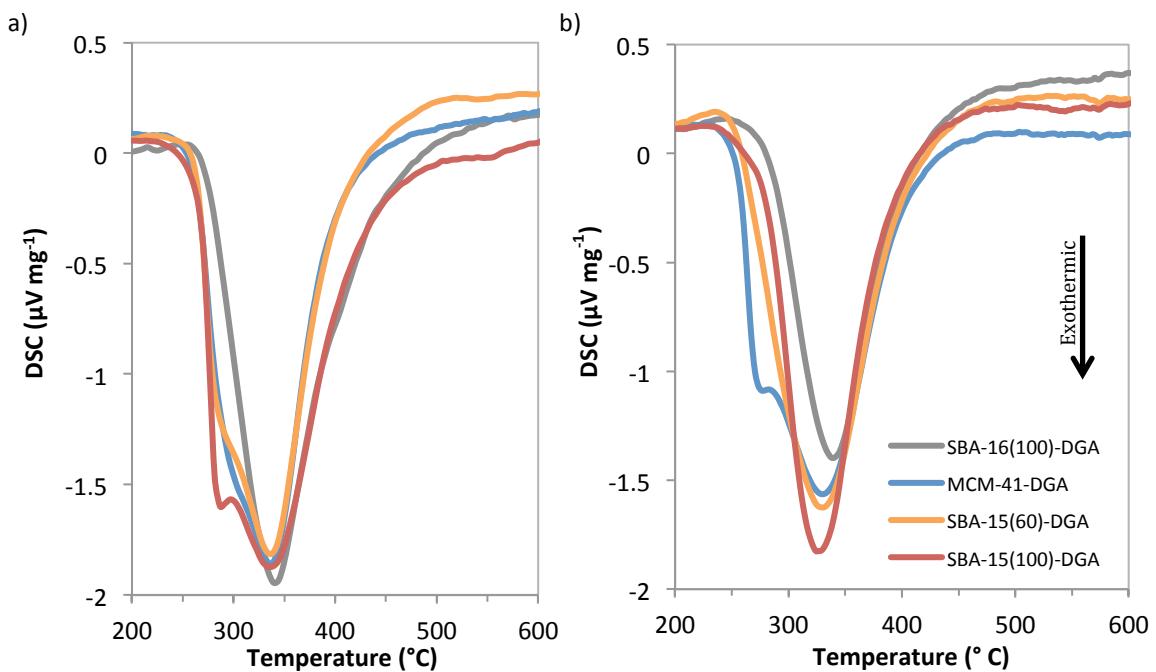


Figure S8: DSC profile of the samples SBA-16(100)-DGA, MCM-41-DGA, SBA-15(60)-DGA and SBA-15(100)-DGA obtained with a) air flow of 20 mL min^{-1} and b) air flow of 40 mL min^{-1} .

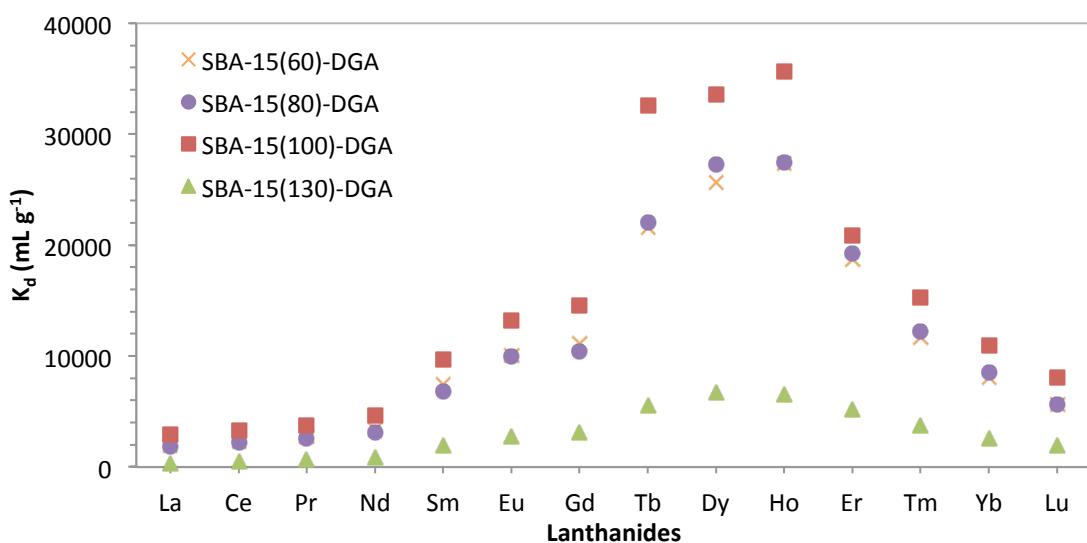


Figure S9: Ln extraction (K_d) of the DGA grafted SBA-15 materials with various pore sizes.

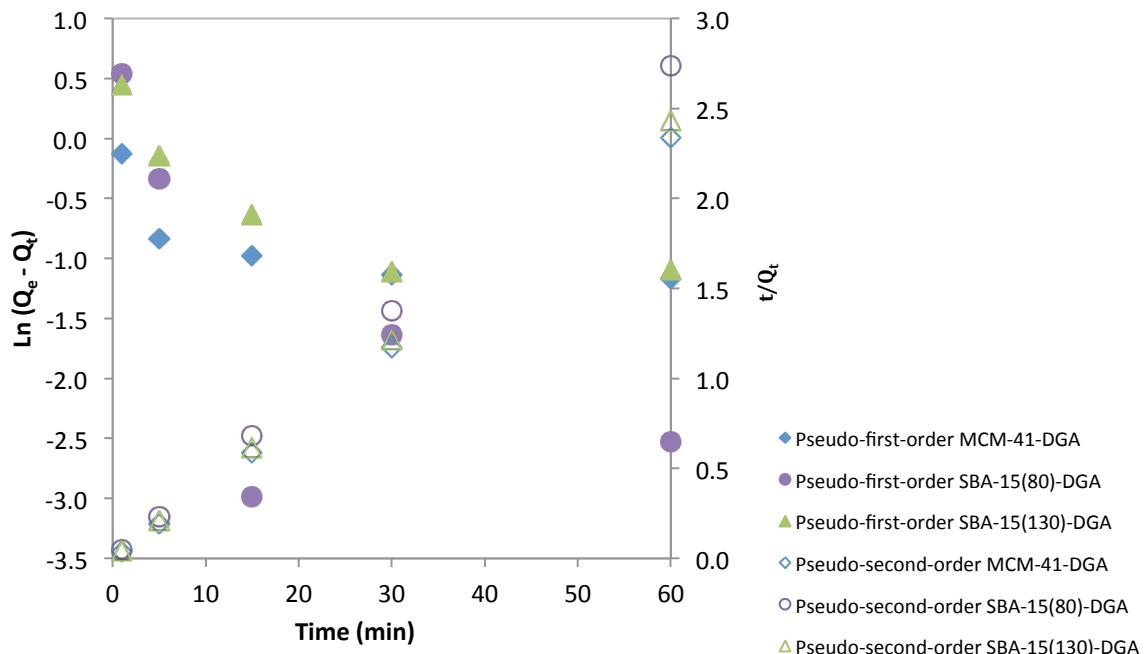


Figure S10: Linear regression of the pseudo-first- order and the pseudo-second-order of SBA-15(80)-DGA, SBA-15(130)-DGA and MCM-41-DGA.

$Q_t = Q_e(1 - e^{-k_1 t})$: Pseudo-first-order equation where Q_t ($\mu\text{g g}^{-1}$) and Q_e ($\mu\text{g g}^{-1}$) represent the amount of REEs captured at time t and at equilibrium, respectively and k_1 represents the rate constant (L min^{-1});

$Q_t = \frac{k_2 Q_e^2 t}{1 + k_2 Q_e t}$: Pseudo-second-order equation where Q_t ($\mu\text{g g}^{-1}$) and Q_e ($\mu\text{g g}^{-1}$) represent the amount of REEs captured at time t and at equilibrium, respectively and k_2 represents the rate constant (L min^{-1}).

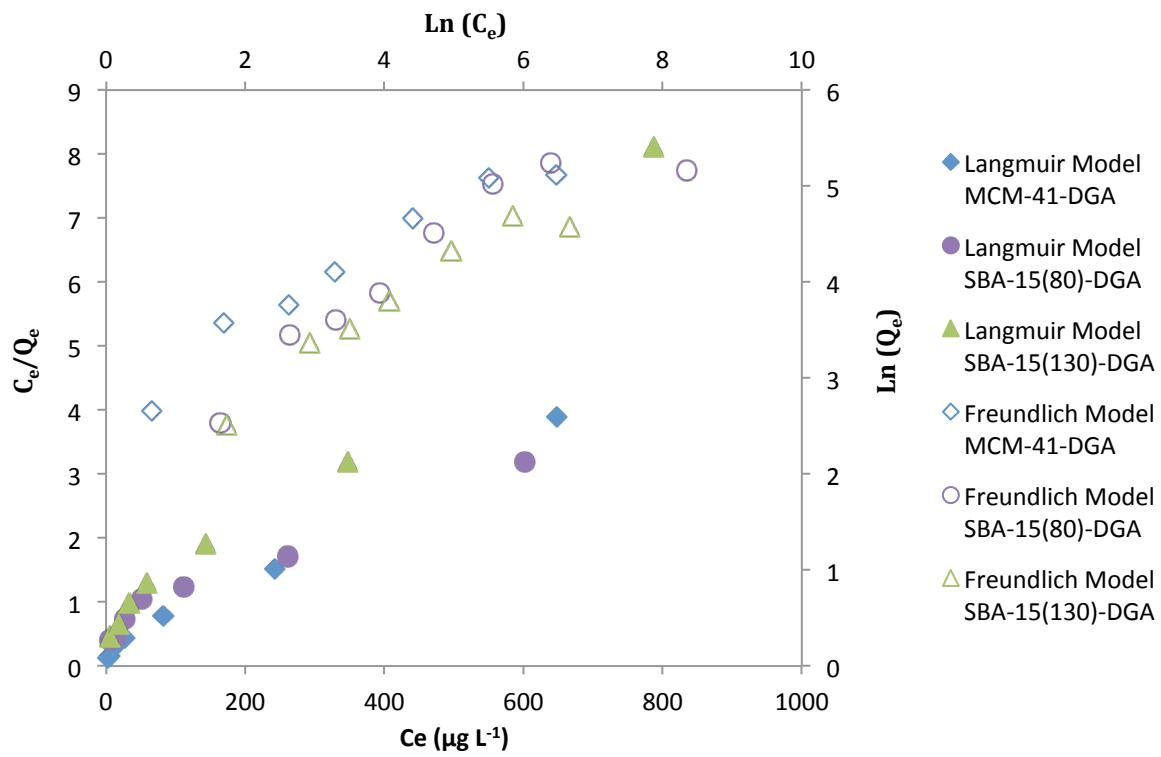


Figure S11: Linear regression of the Langmuir and the Freundlich models used for the adsorption isotherms experiments

$Q_e = Q_{max} \left(\frac{K_L C_e}{1 + K_L C_e} \right)$: Langmuir equation where Q_{max} ($\mu\text{g g}^{-1}$) is the maximum capacity of the materials, K_L ($\text{L } \mu\text{g}^{-1}$) is the Langmuir affinity constant;

$Q_e = K_F C_e^{1/n}$: Freundlich equation where K_F ($\mu\text{g g}^{-1}$) is the Freundlich adsorption capacity constant and $1/n$ refers to favorable adsorption if comprised in the interval $0 < 1/n < 1$.

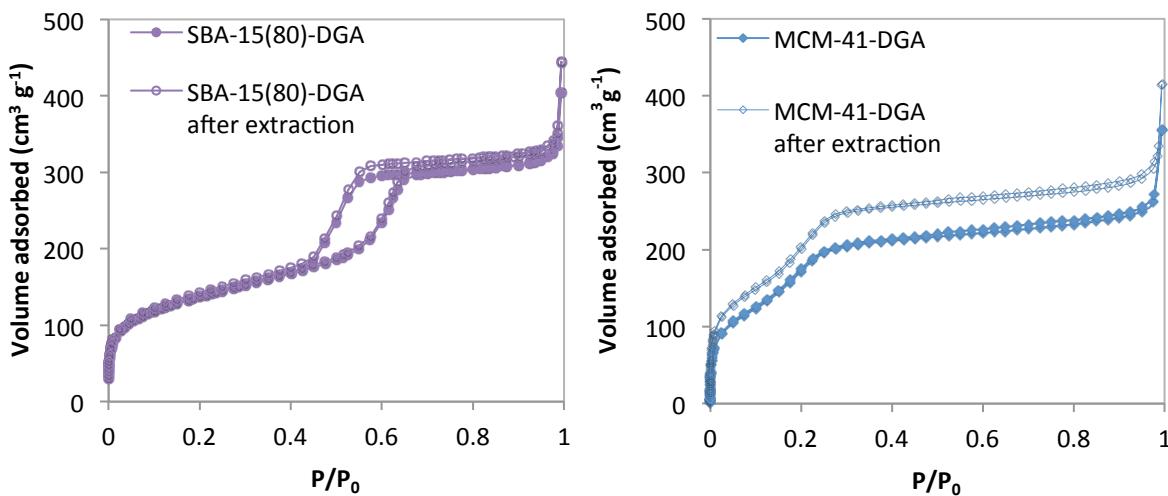


Figure S12: N_2 sorption isotherms (-196°C) of SBA-15(80)-DGA and MCM-41-DGA before and after being used 4 times.

Table S1: CHN analysis of the grafted samples.

Sample	Carbon (%)	Hydrogen (%)	Nitrogen (%)
SBA-16-DGA	9.32	2.53	2.03
SBA-15(60)-DGA	12.17	2.14	2.68
SBA-15(80)-DGA	12.08	2.48	2.58
SBA-15(100)-DGA	11.68	2.25	2.50
SBA-15(130)-DGA	11.36	2.02	2.55
MCM-41-DGA	12.40	2.36	2.74

Table S2: Parameters derived from the pseudo-first-order, pseudo-second-order, Langmuir and Freundlich models.

	SBA-15(80)-DGA	SBA-15(130)-DGA	MCM-41-DGA
Pseudo-first-order	$Q_{e,\text{th}}$	0.61	1,00
	k_1	0.040	0.023
	r^2	0.4293	0.6805
Pseudo-second-order	$Q_{e,\text{th}}$	21.95	24.70
	k_2	0.45	0.43
	r^2	0.9999	0.9999
Langmuir model	Q_m	261.8	106.5
	K_L	0.0058	0.018
	r^2	0.9901	0.9888
Freundlich model	K_F	6.68	7.13
	$1/n$	0.52	0.44
	r^2	0.9708	0.9389