# 1 Electronic Supplementary Information (ESI):

- 2 An insight into the solvent effect on the positional selectivity of the immobilized lipase from
- 3 Burkholderia cepacia in 1,3-diolein synthesis
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#### 13 Experimental section

#### 14 Biological and chemical materials

- 15 The lipase from Burkholderia cepacia (PSL-C, immobilized on ceramics, 35.8 U g<sup>-1</sup>, one unit was
- 16 defined as the amount of enzyme which catalyzed the esterification of 1 mmol oleic acid with
- 17 glycerol per minute at 50 °C) was a gift from Amano Enzyme China Ltd.. 1-Monoolein, 2-
- 18 monoolein, 1,2-diolein, 1,3-diolein and triolein were purchased from Sigma-Aldrich. All other
- 19 chemicals and reagents were of the highest purity commercially available.
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## 21 General procedure for 1,3-diolein preparation

22 In a typical experiment, the PSL-C-catalyzed esterification of oleic acid with glycerol proceeded

in a 50 mL flask on a rotary shaker at 200 rpm at 50 °C. The reaction mixtures contained oleic
 acid, glycerol, solvent and PSL-C. Certain amount of 4 Å molecular sieves was employed to
 remove the generated water online. Samples were withdrawn, centrifuged to obtain the upper layer
 and analyzed by HPLC and GC.

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## 6 Analysis of the samples

7 1-Monoolein, 2-monoolein, 1,2-diolein, 1,3-diolein and triolein contents in the reaction mixture were analyzed using the methods described by us previously.<sup>1</sup> Shimadzu 20A HPLC system 8 9 (Shimadzu, Kyoto, Japan) with a low temperature evaporative light scattering detector was 10 employed. External standards of 1-monoolein, 2-monoolein, 1,2-diolein, 1,3-diolein and triolein 11 were used to prepare calibration solutions at eight different concentrations. 2  $\mu$ L sample and 1 mL 12 acetone were precisely measured and mixed thoroughly. 20  $\mu$ L of the aforementioned mixture was injected. The stationary and mobile phases were a C18 column (5  $\mu$ m, 250 mm × 4.6 mm) (Dikma 13 Technology, PLATISIL ODS, China) and a gradient elution program (Table 1s) by acetonitrile 14 15 and dichloromethane at 1.5 mL min<sup>-1</sup>, respectively. The column temperature and drift pipe temperature were controlled at 40 °C and 70 °C, respectively, and the nitrogen pressure was 16 controlled at 320 kPa. The retention times were 3.75 min, 4.54 min, 23.12 min, 23.90 min, and 17 18 42.91 min for 2-monoolein, 1-monoolein, 1,3-diolein, 1,2-diolein and triolein, respectively. The 19 oleic acid and glycerol concentrations were detected using the methods described by Du.<sup>2</sup> The oleic acid content was analyzed by GC-14B gas chromatograph (Shimadzu, Kyoto, Japan) 20 21 equipped with a FFAP capillary column ( $0.32 \text{ mm} \times 25 \text{ m}$ ) and FID detector. The column 22 temperature was kept at 150 °C for 0.5 min, raised to 250 °C at 15 °C min<sup>-1</sup>, and maintained at this temperature for 10 min. The temperatures of the injector and detector were set at 245 and 250 °C,
 respectively. The glycerol concentration was measured by HPLC using a SCL-10A system
 (Shimadzu, Kyoto, Japan) equipped with a refractive index detector and an Aminex HPX-87H
 column thermostated at 65 °C. Elution was carried out with a 5 mM H<sub>2</sub>SO<sub>4</sub> mobile phase at a flow
 rate of 0.8 mL min<sup>-1</sup>. All reported data are averages of experiments performed at least in duplicate.



Table 1s Gradient elution pro	gram
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Time (min)	Flow rate (mL min <sup>-</sup> <sup>1</sup> )	Acetonitrile-acetic acid (99.85:0.15) (V/V, %)	Dichloromethane (V/V, %)
0	1.50	100	0
4	1.50	100	0
12	1.50	90	10
25	1.50	90	10
30	1.50	70	30
35	1.50	70	30
45	1.50	20	80
55	1.50	20	80
60	1.50	100	0
65	1.50	100	0

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## 8 Rate constants identified<sup>1</sup>

9 For investigating the kinetic behaviors during PSL-C-catalyzed synthesis of 1,3-diolein in these 10 solvent systems, the synthetic scheme shown in Scheme 1 was adopted in which oleic acid and the 11 byproduct water was neglected for simplification. The esterification reaction rates would follow 12 second-order kinetics with respect to the concentration of each substrate involved in the respective 13 reaction step;<sup>3,4</sup> the mass transfer limitation in the reaction system could be neglected. Based on 1 the above assumptions, the differential equations characterizing the whole reaction process were

- 2 listed as follows and in the equations, OA, 1-MO, 2-MO, 1,3-DO, 1,2-DO, TO and Gly referred to
- 3 oleic acid, l-monoolein, 2-monoolein, 1,3-diolein, 1,2-diolein, triolein and glycerol, respectively.

$$\frac{d[OA]}{dt} = k_2[1 - MO] + k_{10}[2 - MO] + k_4[1, 3 - DO] + (k_6 + k_{12})[1, 2 - DO] + (k_8 + k_{14})[TO] - ((k_1 + k_9)[Gly] + (k_3 + k_{11})[1 - MO] + k_5[2 - MO] + k_7[1, 2 - DO] + k_{13}[1, 3 - DO])[OA]$$

$$\frac{d[1 - MO]}{dt} = k_1[OA][Gly] + k_4[1, 3 - DO] + k_{12}[1, 2 - DO] + k_{16}[2 - MO] - (k_2 + k_5 + (k_3 + k_{11})[OA])[1 - MO]$$

$$4 \quad \frac{d[2 - MO]}{dt} = k_6[1, 2 - DO] + k_9[OA][Gly] + k_{15}[1 - MO] - (k_5[OA] + k_{10} + k_{16})[2 - MO]$$

$$\frac{d[1, 3 - DO]}{dt} = k_3[1 - MO][OA] + k_{14}[TO] + k_{18}[1, 2 - DO] - (k_4 + k_{13}[OA] + k_{17})[1, 3 - DO]$$

$$\frac{d[1, 2 - DO]}{dt} = (k_5[2 - MO] + k_{11}[1 - MO])[OA] + k_8[TO] + k_{17}[1, 3 - DO] - (k_6 + k_7[OA] + k_{12} + k_{18})[1, 2 - DO]$$

$$\frac{d[TO]}{dt} = (k_7[1, 2 - DO] + k_{13}[1, 3 - DO])[OA] - (k_8 + k_{14})[TO]$$





#### 9 References

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