Supplementary Information

Enhanced actuated strain of titanium dioxide/nitrile-butadiene rubber composite by biomimetic method

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| Material | Prestrain | Actuated strain ^a | Field Strength ^a | Ref. |
|---|-------------------|------------------------------|--------------------------------|------|
| | (x,y) (%) | (%) | (MV/m) | |
| VHB 4910 | 540, 75 | 215 | 239 | 1 |
| VHB 4905 | 300, 300 | 200 | 480 | 2 |
| Silicone ENP SEBS161 (5-30 wt%) | 300, 300 | 180-30 | 32-133 | 3 |
| Silicone ENP SEBS 217(5-30 wt%) | 300, 300 | 245-47 | 22-98 | 3 |
| VHB 4910 acrylic | 300, 300 | 158 | 412 | 1 |
| VHB4910/poly(1,6-hexanediol diacrylate) | 275, 275 | 233 | 300 | 4 |
| HS3 | 280, 0 | 117 | 128 | 1 |
| Silicone-based prototype | 200% ^b | 18.31 | 96 | 5 |
| TiO ₂ /SEBS | 100, 100 | 12 | 27.5 | 6 |
| PMMA-PnBA-PMMA | 100, 100 | 12 | 4.5 | 7 |
| Silicone+30 wt%TiO ₂ | 100, 100 | 11 | 10 | 8 |
| PDMS/PHT | 100, 100 | 7.6 | 8 | 9 |
| polyurethane-based prototype | 100% ^b | 2.04 | 127 | 5 |
| CF19-218 | 100, 0 | 63 | 181 | 1 |
| HS3 silicone | 68, 68 | 93 | 110 | 1 |
| CF19-2186 silicone | 45, 45 | 64 | 350 | 1 |
| DC 3481(5%81-R)/20 wt%CPO | 40, 40 | 11 | 27 | 10 |
| CF19-2186 silicone | 15, 15 | 33 | 160 | 1 |
| VHB 4910 acrylic | 15, 15 | 40 | 55 | 1 |

Table S1 Comparing actuated strain of 10 phr TiO_2 -PDA/NBR composite with other EAP actuators

| HS3 silicone | 14, 14 | 69 | 72 | 1 |
|----------------------------------|--------|-------|------|----|
| Allyl-cyano/SiR | 10, 10 | 7 | 20 | 11 |
| TiO ₂ /PDMS | 5, 5 | 18 | 50 | 12 |
| DOP/HNBR | 0, 0 | 22 | 30 | 13 |
| Dipole/PDMS | 0, 0 | 14.8 | 1.3 | 14 |
| TiO ₂ /PDMS/DMSO | 0, 0 | 13 | 30 | 15 |
| PANI@PDVB/PDMS | 0, 0 | 12 | 54 | 16 |
| PEG/PDMS | 0, 0 | 11.5 | 40 | 17 |
| BaTiO ₃ /CB/PDMS | 0, 0 | 7.46 | 30 | 18 |
| PANI-g-PolyCuPc-g-PU | 0, 0 | 7 | 23 | 19 |
| 23 wt%PANI/P(VDF-TrFE-CTFE) | 0, 0 | 1.5 ° | 9.5 | 20 |
| 14PANI/15PolyCuPc/85PU | 0, 0 | 9.3 ° | 20 | 21 |
| SEBS-MA grafted PANI | 0, 0 | 1.4 | 27 | 22 |
| NBR/TiO ₂ /DOP | 0, 0 | 3.04 | 20 | 23 |
| 18.26% v/v graphite/Polyurethane | 0, 0 | 0.037 | 0.75 | 24 |
| 5 wt% CNTs/PDMS | 0, 0 | 4.4 | 1.5 | 25 |
| P(VDF-TrFE)/40 wt%CuPc | 0, 0 | 1.91 | 13 | 26 |
| Silicone oil/PMN/PDMS | 0, 0 | 7.4 | 40 | 27 |
| CNT/P(VDF-TrFE-CFE) | 0, 0 | 2.5 | 72 | 28 |
| P(VDF-TrFE-CFE) | 0, 0 | 4.5 | 130 | 29 |
| LC gels | 0, 0 | 2.1 | 25 | 30 |
| Polyester elastomer | 0, 0 | 11.9 | 15.6 | 31 |
| 50 phr BT-PDA/HNBR | 0, 0 | 20 | 45 | 32 |
| m-BT/SR4 | 0, 0 | 26 | 12 | 33 |

| TiO ₂ /PDMS/MDSO | 0, 0 | 13 | 30 | 34 |
|----------------------------------|------|-----------------|------|----|
| DAN/TPU | 0, 0 | 2.6 | 20 | 35 |
| SeRM | 0, 0 | 10 | 23 | 36 |
| Azo-g-PDMS | 0, 0 | 17 | 67.5 | 37 |
| Carbon black/PU | 0, 0 | 18 ^c | 20 | 38 |
| SiC@C-PU | 0, 0 | 18 ^c | 18 | 39 |
| PBDII | 0, 0 | 25.5 | 42 | 40 |
| TRG/TPU | 0, 0 | 1.8 | 0.25 | 41 |
| TiO ₂ /ESO/HNBR | 0, 0 | 13.6 | 30 | 42 |
| 10 phr TiO ₂ -PDA/NBR | 0, 0 | 5.2 | 12.5 | |

^aEstimated from graphical data in cited reference, when there is no tabular was provided; ^bThe axial prestrain; ^cThe longitudinal strain.

As getting a high actuated strain under the condition of prestrain-free is a big object for researchers, we compared the actuated strain of 10 phr TiO₂-PDA/NBR composite with those of other dielectric elastomers reported in the literature under the condition of prestrain-free. It can be easily observed that the actuated strain (5.2%) of 10 phr TiO₂-PDA/NBR composite is relatively high, showing an obvious advantage in practical application.

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