## Supplementary materials

## High Performance Perovskite Solar Cells by a Vapor Based

## Method with Optimized $\mathrm{PbI}_{2}$ Precursor Films

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## Testing platform for solar cell long term stability measurement

A PMMA sealed box is used to maintain the humidity at a constant value when the solar cell is heated. The heater module (TC-48-20, TE technology, INC., Traverse city, USA) was used to main the heating temperature at a constant value. Temperature control accuracy of this testing platform is $\pm 1^{\circ} \mathrm{C}$. Humidity control accuracy of this testing platform is $\pm 3 \%$ (relative humidity).


Figure S1. Testing platform for perovskite solar cell long term stability measurement


Figure S2. Actual temperature curve in the quartz recorded by a wireless thermometer when the furnace heating up program was set as: 30 min to heat up from the room temperature to $70{ }^{\circ} \mathrm{C}$, maintaining for 30 min , taking 20 min to heat up to $110{ }^{\circ} \mathrm{C}$, maintaining for three hours, then end the program. Finally, the quartz tube cooled down to the room temperature.

Table S1. Statistics of ten HPCVD solar cells before and after heat-treated at $80^{\circ} \mathrm{C}$ for 50 $h$ and 96 h .

| No. | $J_{S C}\left(\mathrm{~mA} \mathrm{~cm}^{-2}\right)$ | $V_{O C}(\mathrm{~V})$ | FF | PCE (\%) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Before treatment |  |  |  |  |  |  |  |
| Avg. | $\mathbf{1 6 . 5 5}$ | $\mathbf{0 . 9 6}$ | $\mathbf{0 . 5 4}$ | $\mathbf{8 . 9}$ |  |  |  |
| 1 | 18.80 | 0.97 | 0.63 | 11.8 |  |  |  |
| 2 | 16.60 | 0.95 | 0.50 | 8.1 |  |  |  |
| 3 | 15.70 | 0.95 | 0.51 | 7.8 |  |  |  |
| 4 | 16.70 | 0.97 | 0.47 | 7.8 |  |  |  |
| 5 | 17.10 | 0.98 | 0.49 | 8.5 |  |  |  |
| 6 | 17.60 | 0.96 | 0.58 | 10.1 |  |  |  |
| 7 | 16.30 | 1.01 | 0.59 | 10.0 |  |  |  |
| 8 | 19.00 | 0.89 | 0.56 | 9.8 |  |  |  |
| 9 | 12.30 | 0.98 | 0.54 | 6.7 |  |  |  |
| 10 | 15.40 | 0.91 | 0.54 | 7.8 |  |  |  |
| Avter heated at $80{ }^{\circ} \mathrm{C}$ for |  |  |  |  |  | 50 h |  |
| 1 | $\mathbf{1 6 . 0 6}$ | $\mathbf{0 . 9 4}$ | $\mathbf{0 . 5 1}$ | $\mathbf{7 . 9}$ |  |  |  |
| 2 | 18.90 | 0.95 | 0.52 | 9.6 |  |  |  |
| 3 | 16.60 | 0.95 | 0.50 | 8.1 |  |  |  |
| 4 | 14.40 | 0.92 | 0.33 | 4.5 |  |  |  |
| 5 | 16.00 | 0.96 | 0.47 | 7.4 |  |  |  |
| 6 | 15.50 | 0.95 | 0.53 | 8.0 |  |  |  |
| 7 | 17.60 | 0.96 | 0.57 | 9.9 |  |  |  |
| 8 | 16.30 | 0.97 | 0.60 | 9.8 |  |  |  |
| 9 | 19.30 | 0.89 | 0.51 | 9.0 |  |  |  |
| 10 | 10.60 | 0.90 | 0.49 | 4.8 |  |  |  |
| 15.40 | 0.91 | 0.54 | 7.8 |  |  |  |  |


| After heated at $80{ }^{\circ} \mathrm{C}$ for 96 h |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Avg. | $\mathbf{1 4 . 5 3}$ | $\mathbf{0 . 9 2}$ | $\mathbf{0 . 4 8}$ | $\mathbf{6 . 9}$ |
| 1 | 14.00 | 0.90 | 0.49 | 6.4 |
| 2 | 15.20 | 0.91 | 0.45 | 6.4 |
| 3 | 10.90 | 0.88 | 0.31 | 3.1 |
| 4 | 15.60 | 0.98 | 0.47 | 7.4 |
| 5 | 14.10 | 0.96 | 0.49 | 6.8 |
| 6 | 17.10 | 0.97 | 0.58 | 9.9 |
| 7 | 16.10 | 1.00 | 0.61 | 10.1 |
| 8 | 17.20 | 0.82 | 0.53 | 7.7 |
| 9 | 11.70 | 0.92 | 0.44 | 4.9 |
| 10 | 13.40 | 0.89 | 0.47 | 5.8 |

