SUPPLEMENTARY MATERIAL

Integrated microfluidic platform for instantaneous flow and localized temperature control[†]

Cifeng Fang,^{‡a} Doojin Lee,^{‡b} Boris Stober,^c Gerald G. Fuller,^d and Amy Q. Shen^{*a,b}

^a Department of Mechanical Engineering, University of Washington, Seattle, WA, 98195

^b Micro/Bio/Nanofluidics Unit, Okinawa Institute of Science and Technology Graduate University, 1919-1 Tancha, Onna-son Okinawa, 904-0495 Japan ^c Department of Mechanical Engineering, The University of British Columbia, 2054-6250 Applied Science Lane, Vancouver, BC, V6T 1Z4, Canada ^d Chemical Engineering, Stanford University, Stanford, CA, 94305-4125

Supplementary Movies

Movie S1 Shows the nematic to isotropic transition of a trapped liquid crystal droplet (110 μ *m* in diameter) during one localized ascending temperature cycle. The droplet was trapped in the stagnation zone at the cross junction. (The microscope illumination is polarized. This clip was captured at 24 fps and plays at 1 x. Scale bar: 50 μ *m*)

Movie S2 Shows the nematic to isotropic to nematic transition of a trapped liquid crystal droplet (110 μ *m* in diameter) during periodic temperature variations. The droplet was trapped in the stagnation zone at the cross junction. (The microscope illumination is polarized. The clips was captured at 24 fps and plays at 1 x. Scale bar: 50 μ *m*)

Movie S3 Shows the nematic state liquid crystal droplets (110 μ *m* in diameter) under polarized illumination condition. (The clip was captured at 1,000 fps and plays at 24 fps. Scale bar: 50 μ *m*)

Supplementary Text: Fabrication procedures of flow and temperature manipulation platforms

Microfabrication

We use standard multilayered soft-lithography (MSL) protocols for fabrication the microfluidic channel and the wet etching process for conductive wire micropatterning. The mask design is also available as a separate file in ESI.

Conductive wire patterning

A glass slide (EMF, CA-134) with a 1000 Å thick gold film on a 50 Å thick chrome adhesion layer was used for conductive wire patterning. The slide was spincoated with a positive photoresist with thickness ~ 1.5 μ m (Microchem, AZ-1512), followed by a soft baking process at 110 °C for 2 min. The microheater and the adjacent temperature sensor were designed by AutoCAD and printed on a transparency with 50,800 dpi resolution (Fineline Imaging, OR). The exposure process was carried out by using a mask aligner (ABM-aligner, ABM-USA Inc.) under wavelength of 365 μ m for 5–6 sec. The photoresist was then developed by using 25 % v/v aqueous photoresist solution (Microchem, AZ-340) for 1 min. The glass slide with the patterned photoresist was baked at 110 °C for 1 hr for better adhesion and curing. A wet etching process was conducted by immersing the glass slide into gold etchant (TFA gold etchant, Transene) for 30–35 sec, followed by immersing the glass slide immediately in chrome etchant (TFE chromium etchant, Transene) for 2–3 sec. The glass slide was rinsed by acetone to remove residual photoresist. The etched glass slide was again rinsed with isopropanol (IPA) and water, and dried by nitrogen gas. The glass slide, together with the electric connection pads covered by Teflon tape, was coated with 100 nm silicon dioxide to prevent any electrolysis.

Double layered microchannel fabrication

The microfluidic channel was fabricated using standard multilayer soft-lithography (MSL). Photomasks were designed using AutoCAD and printed on a transparency with 50,800 dpi resolution using commercial laser photoplotting service (Fineline Imaging, OR). The masters were fabricated by contact photolithography using a negative photoresist (SU-8 2050, Microchem). The photoresist was spincoated onto a plasma-cleaned 100 mm silicon wafer (test grade wafer, SVM). After a soft baking process at 65 °C for 3 min then at 95 °C for 9 min, an exposure process was carried out by using a mask aligner (ABM-USA Inc., ABM-aligner) with a 365 μ m wavelength UV light for 22 sec. After post baking (2 min at 65 °C, 7 min at 95 °C), the master was then developed with a propylene glycol monomethyl ether acetate (PGMEA) (Y020100, Microchem), followed by surface treatment with trichloro (1H, 1H, 2H, 2H-perfluorooctyl) silane (448931, Sigma-Aldrich) vapor under a vacuum condition for easy peeling of PDMS replica from the master.

Two SU-8 masters of fluidic layer (70 μ m deep) and control layer (70 μ m deep) were fabricated. The fluid layer with a thin PDMS valve membrane was obtained by spincoating the fluidic SU-8 master with PDMS (Sylgard 184, Dow Corning) at 15:1 ratio of the base resin and the crosslinker. The control layer was fabricated by casting PDMS at 5:1 ratio of base resin and crosslinker onto the corresponding SU-8 master. Both PDMS layers were partially cured by baking at 65 °C for 25 min. The thick PDMS replica (control layer) was then peeled off from the master, aligned, and was hermetically sealed onto the thin PDMS layer (fluidic layer). The bonded PDMS double-layer was placed on a hot plate at 65 °C for 4 hr to form an integrated monolithic device. Verified by the microscopy image, the double-layered microchannel has a 17.5 μ m thin PDMS valve membrane, 70 μ m control layer, and 70 μ m fluid layer.

A step-by-step fabrication protocol for the device fabrication is provided as below.

Master making process: using SU-8 2050

- Turn on hot plates, UV power, and spinner
- Clean silicon wafer(s), rinse with
 - Acetone-IPA-Water-IPA
 - Dry with N₂
- Place wafer on hot plate at first setting, for few minutes to remove excess solvent
- Remove wafer and let cool, then pour SU-8 2050 negative photoresist (~2mL/inch substrate diameter).
- To prevent edge effects, rotate wafer with tweezers to ensure a uniform distribution of photoresist
- Place the wafer on the spin coater and follow the recipe below:

Control layer: 70 um (SU-8 2050)

	RPM	RPM/S	DWELL (s)
0	1	100	1
1	500	100	5
2	2000	300	30
3	0	200	0

Fluidic layer: 70 um (SU-8-2050)

	RPM	RPM/S	DWELL (s)
0	1	100	1
1	500	100	5
2	2000	300	30
3	0	200	0

• Start UV Lamp and **soft bake** the wafer on the hot plate and cover with glass dish for:

	65°C (min)	95°C (min)
70um	3	9

- Let wafer rest on bench for ~ 10 min in open petri dish
- Apply mask and expose to UV for 22 s at 9.5mW/cm²
- Delay 5-10 min after exposure before developing.
- Post bake wafer on hotplate and cover with glass dish for:

	65°C (min)	95°C (min)
70um	2	7

- Use developer PGMEA for 6-7 mins until clean, remove hazing by rinsing with developer then IPA, repeat if necessary.
- Let wafer cool then rinse with IPA and gently dry with N_2
- Silanize wafer with trichlorosilane for 10–20 min in a vacuum desiccator.

PDMS process:

- Pour and mix PDMS 15:1 and 5:1 of base : crosslinker.
- Place both cups in desiccator and hold vacuum for at least \sim 10-15 min. Remove bubbles by shaking against soft tubing.
- Pour small amount of 5:1 PDMS on top control layer master (first time around 80g in total, the rest 24g).
- Pour 15:1 PDMS on top of fluidic layer master.
- Then vacuum desiccate both again for 5 min.
- Then spin coat 15:1 PDMS/fluidic layer master for:

	RPM	RPM/S	DWELL (s)
0	1	100	1
1	500	200	5
2	900	300	30
3	0	100	0

• Then spin coat 5:1 PDMS/control layer master for:

	RPM	RPM/S	DWELL (s)
0	1	100	1
1	500	100	5
2	500	0	30
3	0	100	0

- Pour remaining 5:1 PDMS onto control layer.
- Then place both masters/PDMS into 65 °C oven for 25-30 min.
- Remove both masters/PDMS and let cool.
- Once cooled down remove control layer PDMS slab with scalpel and punch valve ports.
- Position the control layer PDMS slab to line up with the fluidic layer master/PDMS.
- Remove air bubbles by compression of flat tool.
- Place fluidic layer master/PDMS/Control layer PDMS slab into 65 °C oven for 1 hour overnight.

Microheater & sensor patterning

Gold coated slides: EMF CA134 (Cr 50 Å, Au 1000 Å, sized at 1" x 3" x .040")

- Clean slide (s), rinse with
 - Acetone IPA Water IPA
- Dry with N₂
- + 110 $^\circ\text{C}$ dry solvent
- Place and double tape slide on spin coater and follow recipe: (AZ 1512)

	RMP	ACC	DWELL (s)
0	1	1	1
1	500	100	5
2	3000	400	30
3	0	500	1

- Soft bake 110 °C for 2 mins before UV exposure.
- Make sure by microscope that the sharp face of the transparency should be faced to gold slide directly, exposure 5-6s.
- 4:1 ratio of water : AZ 340 for 1 mins, after develop, put slides into water and rinse.
- Post bake 110 °C for 1 hour.

- Wet etching:
 - Gold etching: 30-35s
 - Chrome etching: 1-2s
 - Water rinsing
- Put patterned slides into acetone for 2 hours
- Rinse slide(s) with
 - IPA Water IPA
 - Dry with N₂

Deposit silicon oxide layer to slides:

- Clean patterned slide (s), rinse with
 - Acetone IPA Water IPA
 - Dry with N₂
- Cover the connection pads with Teflon types.
- Mount slides to sample holder and place to deposition chamber.
- Deposit silicon oxide layer.
- Peel off the Teflon tapes.

Bonding:

- Remove fluidic layer master/PDMS/Control layer PDMS slab from oven and let cool.
- Use scalpel to cut along the control PDMS edge to remove both layers.
- Chop excess PDMS edges with razor blade, separate each device, and hole punch inlet ports in the fluidic layer.
- Clean PDMS with tape and clean patterned slide(s) with deionized (DI) H₂O. Then rinse with IPA.
- Dry patterned slide(s) with N2 and place on metal plate sample holder next to PDMS slab that sits side up
- Place into the chamber of plasma cleaner (Harrick Plasma, PDC-32G), set the RF level to MED and after reaching between 500 mTorr -1Torr run for 90 s allowing a small amount of air into the chamber every 30 s.
- When time is up, remove and immediately bond to the patterned slide by placing one edge at desired location and dropping the slab to force air out, then put the bonded device on the hot plate (65 $^{\circ}$ C) baking for 1 hour –overnight.



Fig. 1 Snapshots of the microfluidic device (scale bar = 5 mm) for (a) Temperature sensor calibration. The temperature sensor is connected to one channel of the digital multimeter while J-type thermocouple is connected to the other channel of the digital multimeter. (b) Double-layered microfluidic device with inlet and outlet tubings sitting onto an inverted microscope. Wires from the microheater and temperature sensor are connected to the temperature controller and the multimeter, respectively.

Supplementary Text and Figures: Temperature sensor calibration procedure

The underlying mechanism of temperature measurement in the temperature sensor rests upon the temperature dependency of the electrical conductivity of the wire. Thus, it is important to calibrate the temperature sensor to obtain a reliable and precise temperature. A PDMS slab with a reservoir, holding calibration fluid, was placed on the glass slide etched with the microheater and temperature sensor. A J-type thermocouple (Omega, SA1-J) was placed into the reservoir as the temperature reference. The temperature sensor was connected to one channel of the digital multimeter for 4-wire resistance measurement, while the thermocouple was connected to the other channel for the temperature reading (**Fig. 1a**). The reservoir was then filled with hot water, the calibration fluid, while measuring both the temperature and sensor resistance simultaneously. A series of resistance data which corresponds to the temperature ranging from room temperature to 60 °C was collected to obtain a linear curve fit that was used as a general calibration curve between the sensor resistance and real temperature. This calibration curve was implemented into the temperature control algorithm in the LabVIEW code. Once the calibration is finished, the PDMS slab was removed from the glass slide, and the double-layered microfluidic channel was bonded with the glass slide. Inlet and outlet tubings were then connected to the device (**Fig. 1b**) for further experiments.

Supplementary Text and Diagram: Controlling the temperature profile mimicking a PCR cycle

We evaluated the temperature control ability in our platform at relatively high temperatures in a wide temperature range to simulate a single PCR cycle. A typical PCR cycle consists of the denaturation step (maintaining temperature in the range of 94–98 °C for 1–9 minutes), annealing step (maintaining temperature in the range of 50–68 °C for 20–60 seconds), and elongation step (maintaining temperature in the range of 70–74 °C for 3–15 minutes). We used mineral oil as the solvent and applied the standard PCR temperature profile (with characteristic temperature steps and time intervals) at the cross junction in the microdevice, subsequently measured the actual temperature output, see Fig. 2.



Fig. 2 Temperature control diagram mimicking a single PCR cycle: the in-situ temperature at the cross junction of the microdevice is first heated to the DNA denaturation temperature ($95^{\circ}C$) and held for 120 s; then cooled to the annealing temperature ($68^{\circ}C$) for around 120 s, and finally reaching the elongation temperature ($72^{\circ}C$) for 200 s.

Supplementary Text and Figures: LabVIEW program

Hardware components

All the hardware components were controlled with a custom made LabVIEW program in real time. The hardware is not limited to specific build up. Components from other venders will also work after proper modification of hardware Input/Output (I/O) setup in LabVIEW.

Real time image processing

The LabVIEW built-in Vision Assistant Express module was used for image processing, involving the feature enhancement and particle analysis. The real time image processing for droplet segmentation is challenging, as the conductive micropattern is in the background

image and the illumination condition of droplet change dynamically. To achieve optimized results, we incorporate the following functions: Gaussian smoothing, thresholding, removal of small objects, image close, convex hull, particle filter, convolution-highlight details, and particle analysis. See two examples shown in **Fig. 3**, from raw images to processed images.



Fig. 3 Image processing sequence: The image is first therosholded to show only the outline of droplet and wire pattern. By removing small objects, only the feature of droplet is left. By closing proper image, convex hull fill and particle filtering, a mask of droplet is obtained. Through convolution, followed by particle analysis, the approximation of centroid and area of the droplet can by obtained, which is used for the droplet position feedback control.