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### **Supplementary Information**

# A new insight on the conformation and melt dynamics of hydrogenated polybutadiene as revealed by computer simulation

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#### S.1 End-to-end autocorrelation function and Mean-square internal distances

The end-to-end autocorrelation function ( $\langle \mathbf{u}(t)\mathbf{u}(0) \rangle$ ) and the mean square internal distances for the linear polyethylene (LPE) and hydrogenated polybutadienes (PEB2) models are show in Figure S.1. The  $\langle \mathbf{u}(t)\mathbf{u}(0) \rangle$  is fitted with the Kohlrausch-Williams-Watts (KWW) stretch exponential function (dashed lines in Figure S.1.a) as:

$$G(t) = A e^{-\left(t/\tau_{KWW}\right)^{\beta}}$$

The integration of the KWW curves allows one to get the end-to-end relaxation time  $(\tau_{\text{ACF}})$  as follows:

$$\tau_{ACF} = \int_{0}^{\infty} G(t)dt = A \frac{\tau_{KWW}}{\beta} \Gamma\left(\frac{1}{\beta}\right)$$

, where  $\Gamma$ () designates the gamma function. In general, the fitting using the KWW function is very good.

The parameters of the fitting are shown in Table S.1. The relaxation time ( $\tau_{ACF}$ ) increases both with length chain and with the presence of branches. At the same time, the parameter  $\beta$  decreases for branched systems as compared with the linear system of the same molecular length.

Model	Α	β	τ <sub>κww</sub> (ns)	τ <sub>ACF</sub> (ns)						
LPE36	1.00	0.920	0.129	0.135						
LPE106	0.98	0.710	1.387	1.698						
LPE192	0.98	0.632	5.248	7.256						
LPE377	0.99	0.538	27.502	47.991						
PBE2_36	1.00	0.907	0.131	0.137						
PBE2_106	0.98	0.696	1.390	1.734						
PBE2_192	0.98	0.615	5.392	7.705						
PBE2 377	0.99	0.524	31.929	58.193						

Table S.1: Fitting parameters of the end-to-end autocorrelation function to the KWW stretch exponential function.



**Figure S.1**.a) End-to-end autocorrelation function  $\langle \mathbf{u}(t)\mathbf{u}(0) \rangle$ , where  $\mathbf{u}(t)$  is the unit vector at time t along the chain end-to-end vector. The points are the values calculated from the simulations and the dashed lines show the best fit to the KWW equation. b) Mean-square internal distances for the linear (LPE) and hydrogenated polybutadiene (PBE2) models.

## S.2 Calculated Rouse and reptation relaxation times as well as friction coefficients for LPE and PEB2 simulated systems.

For the two untangled systems, we have directly obtained the Rouse time  $(\tau_R)$  from the crossover point in the  $g_1(t)$  graph as shown in the figure S.2:



**Figure S.2.** Mean-squared monomer displacement, g1(t), for the unentangled PEB2\_36 and PEB2\_106. The obtained relaxation times are collected in Table S.2. As it can be seen in this table, the  $\tau_{ACF}$  is smaller than the corresponding  $\tau_R$  as discussed by other authors (ref. 25 in the main text). Using these  $\tau_R$  values of unentangled systems, it is possible to obtain the friction coefficient by means of the equation:

$$\tau_R = \frac{\zeta N \langle R_0^2 \rangle}{3\pi^2 k_B T} \tag{1}$$

The obtained values are shown in Table S.2. As the coefficient friction is independent of molecular weight above a certain value (see Figure 8 in ref. 29), we have used the value of  $\zeta$  corresponding to LPE\_106 or PEB2\_106 to calculate the  $\tau_R$  for the entangled systems by applying Eq. 1.

Then, the reptation times can be obtained using different approaches: i)  $\tau_d$  is directly obtained from the  $g_1(t)$  graph as  $g_1(\tau_d) = \langle \mathbf{R}_0^2 \rangle$ , ii) from pure reptation model as  $\tau_d^0 = 3\tau_e Z^3 = 3\tau_R Z$  (ref.46 main text) and iii) using the contour length fluctuation (CLF) model as  $\tau_d^{th} = 3\tau_e Z^3 (1-X Z^{-1/2})^2$ , with X=0.6 (ref.46 main text). In all cases, the  $\tau_{ACF}$  is an order of magnitude smaller than the  $\tau_d$ . This could indicate that the single KWW fitting is not adequate to calculate the reptation times. As expected, the  $\tau_d^0$  (pure reptation model) is higher than  $\tau_d^{th}$  (taking into account the CLF corrections). The  $\tau_d$  value obtained directly from the simulations is similar to the  $\tau_d^{th}$  indicating that the simulations capture the CLF mechanism.

Sample	<i>M</i> kg∙mol <sup>-1</sup>	$\langle \mathbf{R}_{\theta}^2 \rangle$ (nm <sup>2</sup> )	Ζ	$ au_R$ (ns)	$ au_d^{ heta}$ (ns)	$ au_d$ (ns)	$ au_d^{th}$ (ns)	$ au_{ACF}^{b}$ (ns)	ζ (10 <sup>10</sup> dyn s cm <sup>-1</sup> )
PEB2_36	0.536	5.40	-	0.196ª	-	-		0.137	$2.10\pm0.19^{\text{c}}$
PEB2_106	1.547	19.07	-	4.7 <sup>a</sup>	-	-		1.73	$4.82\pm0.45^{\text{c}}$
PEB2_192	2.811	35.86	2.6	15.9 <sup>d</sup>	110e	62.9 <sup>e</sup>	43.7e	7.7	-
PEB2_377	5.493	73.11	5	63.7 <sup>d</sup>	788 <sup>e</sup>	630 <sup>e</sup>	421.6 <sup>e</sup>	58.2	-
LPE_36	0.507	5.73	-	0.168ª	-	-		0.135	$1.69\pm0.19^{\rm c}$
LPE_106	1.489	19.78	-	3.2ª	-	-		1.70	$3.17\pm0.39^{\text{c}}$
LPE_192	2.695	37.14	3.4	9.8 <sup>d</sup>	94.3 <sup>e</sup>	53.6 <sup>e</sup>	42.9 <sup>e</sup>	7.3	-
LPE_377	5.290	75.66	6.6	39.2 <sup>d</sup>	690 <sup>e</sup>	502 <sup>e</sup>	405.3e	48.0	-

Table S.2: Calculated relaxation times and friction coefficients for all simulated systems.

<sup>a</sup> Rouse time obtained directly from the crossover point in the  $g_1(t)$  vs t graph (see Figure 3 in the main text) <sup>b</sup> Longest relaxation time from KWW equation (see S.1)

<sup>c</sup> The  $\tau_{\rm R}$  values of unentangled systems have used to calculate the coefficient friction ( $\xi$ ) by applying  $\tau_R = \zeta N \langle R_0^2 \rangle / 3\pi^2 k_B T$  (ref.46 main text)

<sup>d</sup> Using the  $\zeta$  corresponding to LPE\_106 or PEB2\_106, one can calculate the  $\tau_R$  for the entangled systems by applying the above equation.

<sup>e</sup> The reptation times are obtained as: i)  $\tau_d$  is directly obtained from the  $g_1(t)$  graph as  $g_1(\tau_d) = \langle R_0^2 \rangle$ , ii) from pure reptation model as  $\tau_d^0 = 3\tau_e Z^3 = 3\tau_R Z$  (*ref.46 main text*) and iii) using the contour length fluctuation (CLF) model as  $\tau_d^{th} = 3\tau_e Z^3 (1-X Z^{-1/2})^2$ , with X=0.6 (*ref.46 main text*).

S.3 Characteristic ratio (C<sub>n</sub>) for the linear polyethylene (LPE) and hydrogenated polybutadiene (PEB2) as a function of the molecular length.



**Figure S.3**. Characteristic ratio ( $C_n$ ) for the linear polyethylene (LPE) and hydrogenated polybutadiene (PEB2) as a function of the molecular length (n). For a nice explanation of characteristic ratio as an indicator of the chain stiffness see, for example, Bicerano J., Computational and Theoretical Polymer Science, 8, 9-13, 1998.



### S.4 Mean-squared monomer displacement for the simulated and PEB2 models.

**Figure S.4.** Mean-squared monomer displacement,  $g_1(t)$ , for the simulated LPE (solid lines) and PEB2 (dashed lines) samples at 509 K. The ethyl branches seem to produce a slow-down of the segmental dynamics in all cases.

### S.5 Intermolecular radial pair distribution functions, g<sub>inter</sub>(r).



**Figure S.5.** Intermolecular radial pair distribution function of the simulated LPE (black solid lines) and PEB2 (red dashed lines) samples at 509 K.