Electronic Supporting Information

for

Isomerization of Methoxy Radical Revisited: Impact of Water Dimer

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Rate Calculations:

Isomerization of MR can be written in terms of the bimolecular encounters between MR and catalyst, say X (X = WM, WD, FA and SA) to give HM, as:

$$MR+X \xleftarrow[k_1]{k_1} RC \xrightarrow{k_2} PC \longrightarrow HM + X$$

In the above reaction scheme RC is assumed to be in equilibrium with MR and X and subsequently RC undergoes unimolecular isomerization through TS to form PC. Under this assumption, the reaction rate (v) can be expressed as:

$$\nu = \frac{k_1}{k_{-1}} k_2[MR][X] = K_{eq} k_2[MR][X] = k[MR][X]$$

where
$$K_{eq} = \frac{k_1}{k_{1}}$$
 and $k = K_{eq}k_2$

Where, K_{eq} = equilibrium constant of RCs ,

 k_2 = rate constant for the unimolecular reaction of RCs leading to PCs.

 K_{eq} and k_2 have been computed by using TST as shown below:

$$K_{eq} = \frac{Q_{RC}}{Q_{MR} \cdot Q_X} e^{\frac{-(E_{RC} - E_{MR})}{RT}}$$

$$k_2 = \sigma \Gamma \frac{k_B T Q_{TS}}{h Q_{RC}} e^{\frac{-(E_{TS} - E_{RC})}{RT}}$$

Where, Q = The product of electronic, translational, rotational and vibrational canonical partition functions of the respective species referenced to the zero-point energy (ZPE), E = ZPE corrected energies of the respective species,

= reaction path number or reaction degeneracy,

 Γ = tunneling correction for the reaction (it has been taken into account by assuming unsymmetrical Eckart barrier.^y

 k_B = Boltzmann constant

h = Planck constant

T = temperature in Kelvin

R = ideal gas constant.

The inherent assumption behind this approximation is that the time scale to established the equilibrium is significantly different (fast) as compared to the time scale of second step of reaction (unimolecular conversion). This assumption will work well if the catalyst molecules are present at sufficiently large concentration. Calculations of the rate constants were carried out by use of TheRate program package.¹

It is evident from reaction rate (ν) equation that if all other conditions remain same, then k[X](where, k is the rate constant and [X] is the concentration of the catalyst) can be considered as an effective rate constant: $k_{eff} = k[X]$

To further assess the pre-equilibrium approximation, we have also carried out the rate calculations using MESMER software.² MESMER solves a multi grain master equation to obtain

the phenomenological rate constants which is known as Bartis-Widom phenomenological rate coefficients.

 Table S1 Relative energies (kcal mol⁻¹) of all species with respect to the isolated reactants

 calculated using two different levels of theory

Catalyst	Species	MP2/aug-cc-pVTZ	CCSD(T)/aug-cc-pVTZ
	MR	0	0
None	TS	30.0	32.7
	НМ	-14.1	-8.7
	MR-WM	-5.1	-5.2
WM	TS_{WM}	19.7	22.9
	HM-WM	-20.8	-15.4
	MR-WD	-8.1	-8.4
WD	TS _{WD}	5.3	7.8
	HM-WD	-25.8	-20.5
	MR-FA	-8.5	-8.8
FA	TS _{FA}	3.8	4.4
	HM-FA	-24.1	-18.9
	MR-SA	-11.4	-11.8
SA	TS _{SA}	1.3	1.8
	HM-SA	-25.5	-20.3

Temperatures	WM	WD	FA	SA
298	3.55 × 10 ⁻²⁹	2.82 × 10 ⁻²¹	3.65 × 10 ⁻¹⁶	2.80×10^{-13}
259	3.55 × 10 ⁻²⁹	2.82 × 10 ⁻²¹	6.20 × 10 ⁻¹⁶	1.28 × 10 ⁻¹²
230	9.08 × 10 ⁻³¹	8.46 × 10 ⁻²²	1.40 × 10 ⁻¹⁵	7.13 × 10 ⁻¹²
213	7.08 × 10 ⁻³²	3.39 × 10 ⁻²²	2.89 × 10 ⁻¹⁵	2.74 × 10 ⁻¹¹
216	1.91 × 10 ⁻³²	2.15 × 10 ⁻²²	2.50×10^{-15}	2.11 × 10 ⁻¹¹
219	2.38 × 10 ⁻³²	2.30 × 10 ⁻²²	2.18 × 10 ⁻¹⁵	1.65 × 10 ⁻¹¹
224	2.97 × 10 ⁻³²	2.49 × 10 ⁻²²	1.76 × 10 ⁻¹⁵	1.11 × 10 ⁻¹¹
235	4.37 × 10 ⁻³²	2.85 × 10 ⁻²²	1.17 × 10 ⁻¹⁵	5.06 × 10 ⁻¹²
250	1.07 × 10 ⁻³¹	3.94 × 10 ⁻²²	7.61 × 10 ⁻¹⁶	2.04 × 10 ⁻¹²
280	6.56 × 10 ⁻³⁰	1.64 × 10 ⁻²¹	4.39 × 10 ⁻¹⁶	5.16 × 10 ⁻¹³
290	1.68 × 10 ⁻²⁹	2.22×10^{-21}	3.92 × 10 ⁻¹⁶	3.61 × 10 ⁻¹³
300	4.27 × 10 ⁻²⁹	2.98 × 10 ⁻²¹	3.60 × 10 ⁻¹⁶	2.64×10^{-13}
310	1.06 × 10 ⁻²⁸	3.96 × 10 ⁻²¹	3.38 × 10 ⁻¹⁶	2.00×10^{-13}
320	2.57×10^{-28}	5.20 × 10 ⁻²¹	3.18 × 10 ⁻¹⁶	1.56 × 10 ⁻¹³

Table S2 Rate constants (molecule⁻¹ cm³ s⁻¹) in presence of the four catalysts calculated using results obtained from CCSD(T)/aug-cc-pVTZ//MP2/aug-cc-pVTZ level of theory

Catalyst		280	290	298	300	310	320
	20% H	5.16×10^{16}	9.56 × 10 ¹⁶	1.55×10^{17}	1.72×10^{17}	2.92×10^{17}	4.70×10^{17}
	40% H	1.03×10^{17}	1.91 × 10 ¹⁷	3.09×10^{17}	3.43×10^{17}	5.84×10^{17}	9.40 × 10 ¹⁷
WM ^a	60% H	1.55×10^{17}	2.87×10^{17}	4.64×10^{17}	5.15×10^{17}	8.77×10^{17}	1.41×10^{18}
	80% H	2.07×10^{17}	3.82 × 10 ¹⁷	6.18 × 10 ¹⁷	6.86 × 10 ¹⁷	1.17×10^{18}	1.88 × 10 ¹⁸
	100% H	2.58×10^{17}	4.78×10^{17}	7.73×10^{17}	8.58 × 10 ¹⁷	1.46 × 10 ¹⁸	2.35×10^{18}
WDa	20% H	8.18 × 10 ¹²	2.36×10^{13}	5.44 × 10 ¹³	6.50 × 10 ¹³	1.63 × 10 ¹⁴	3.71 × 10 ¹⁴
	40% H	3.27×10^{13}	9.46 × 10 ¹³	2.18×10^{14}	2.60×10^{14}	6.52×10^{14}	1.48 × 10 ¹⁵
	60% H	7.36×10^{13}	2.13×10^{14}	4.90×10^{14}	5.85×10^{14}	1.46 × 10 ¹⁵	3.33 × 10 ¹⁵
	80% H	1.31×10^{14}	3.78×10^{14}	8.70×10^{14}	1.04×10^{15}	2.60×10^{15}	5.90 × 10 ¹⁵
	100% H	2.04×10^{14}	5.91×10^{14}	1.36 × 10 ¹⁵	1.62×10^{15}	4.06×10^{15}	9.24 × 10 ¹⁵
	High	2.61 × 10 ¹¹	2.52×10^{11}	2.45 × 10 ¹¹	2.43 × 10 ¹¹	2.36×10^{11}	2.28×10^{11}
FA ^b	Average	2.02×10^{10}	1.95×10^{10}	1.90 × 10 ¹⁰	1.89 × 10 ¹⁰	1.83×10^{10}	1.77×10^{10}
	Low	2.61 × 10 ¹¹	2.52×10^{11}	2.45×10^{11}	2.43×10^{11}	2.36 × 10 ¹¹	2.28×10^{11}
SA°		3.94 × 10 ⁸	3.80 × 10 ⁸	3.70 × 10 ⁸	3.68 × 10 ⁸	3.56 × 10 ⁸	3.45 × 10 ⁸

Table S3 Concentration of the four catalysts (in molecules cm⁻³) within 280 K to 320 K temperature range at 0 km altitude. (% H stands for relative humidity)

^{*a*} Reference 3 (concentration of WM and WD has directly been taken from this reference where the authors computed WD concentration from WM concentration and calculated equilibrium constant for WM to WD transformation) ^{*b*} Reference 4 ^{*c*} Reference 5

Table S4 Effective rate constants (s⁻¹) in presence of the four catalysts within 280 K to 320 K temperature range at 0 km altitude calculated by TheRate. (% H stands for relative humidity)

Catalyst	Conc.	280	290	298	300	310	320
WM	20% H	3.38 × 10 ⁻¹³	1.61 × 10 ⁻¹²	5.50 × 10 ⁻¹²	7.34 × 10 ⁻¹²	3.10 × 10 ⁻¹¹	1.21 × 10 ⁻¹⁰
	40% H	6.76 × 10 ⁻¹³	3.22 × 10 ⁻¹²	1.10 × 10 ⁻¹¹	1.46 × 10 ⁻¹¹	6.19 × 10 ⁻¹¹	2.41 × 10 ⁻¹⁰
	60% H	1.02 × 10 ⁻¹²	4.83 × 10 ⁻¹²	1.65 × 10 ⁻¹¹	2.20 × 10 ⁻¹¹	9.30 × 10 ⁻¹¹	3.62 × 10 ⁻¹⁰
	80% H	1.36 × 10 ⁻¹²	6.43 × 10 ⁻¹²	2.19 × 10 ⁻¹¹	2.93 × 10 ⁻¹¹	1.24 × 10 ⁻¹⁰	4.83 × 10 ⁻¹⁰
	100% H	1.69 × 10 ⁻¹²	8.05 × 10 ⁻¹²	2.74 × 10 ⁻¹¹	3.66 × 10 ⁻¹¹	1.55 × 10 ⁻¹⁰	6.04 × 10 ⁻¹⁰
	20% H	1.34 × 10 ⁻⁸	5.25 × 10 ⁻⁸	1.53 × 10 ⁻⁷	1.94 × 10 ⁻⁷	6.46 × 10 ⁻⁷	1.93 × 10 ⁻⁶
	40% H	5.37 × 10 ⁻⁸	2.10 × 10 ⁻⁷	6.14 × 10 ⁻⁷	7.76 × 10 ⁻⁷	2.58 × 10 ⁻⁶	7.70 × 10 ⁻⁶
WD	60% H	1.21 × 10 ⁻⁷	4.74 × 10 ⁻⁷	1.38 × 10 ⁻⁶	1.75 × 10 ⁻⁶	5.78 × 10 ⁻⁶	1.73 × 10 ⁻⁵
	80% H	2.15 × 10 ⁻⁷	8.41 × 10 ⁻⁷	2.45 × 10 ⁻⁶	3.10 × 10 ⁻⁶	1.03 × 10 ⁻⁵	3.07 × 10 ⁻⁵
	100% H	3.35 × 10-7	1.31 × 10 ⁻⁶	3.83 × 10 ⁻⁶	4.83 × 10 ⁻⁶	1.61 × 10 ⁻⁵	4.81 × 10 ⁻⁵
	High	1.14 × 10 ⁻⁴	9.87 × 10 ⁻⁵	8.95 × 10 ⁻⁵	8.75 × 10 ⁻⁵	7.95 × 10 ⁻⁵	7.26 × 10 ⁻⁵
FA	Average	8.87 × 10 ⁻⁶	7.65 × 10 ⁻⁶	6.94 × 10 ⁻⁶	6.79 × 10 ⁻⁶	6.17 × 10 ⁻⁶	5.63 × 10 ⁻⁶
	Low	1.14 × 10 ⁻⁷	9.87 × 10 ⁻⁸	8.95 × 10 ⁻⁸	8.75 × 10 ⁻⁸	7.95 × 10 ⁻⁸	7.26 × 10 ⁻⁸

SA	2.03 × 10 ⁻⁴	1.37 × 10 ⁻⁴	1.04 × 10 ⁻⁴	9.69 × 10 ⁻⁵	7.10 × 10 ⁻⁵	5.37 × 10 ⁻⁵

Table S5 Effective rate constants (s⁻¹) in presence of the four catalysts within 280 K to 320 K temperature range at 0 km altitude calculated by MESMER. (% H stands for relative humidity)

Catalyst	Conc.	280	290	298	300	310	320
WM	20% H	3.77 × 10 ⁻¹³	1.74 × 10 ⁻¹²	5.81 × 10 ⁻¹²	7.71 × 10 ⁻¹²	3.19 × 10 ⁻¹¹	1.22 × 10 ⁻¹⁰
	40% H	7.52 × 10 ⁻¹³	3.47 × 10 ⁻¹²	1.16 × 10 ⁻¹¹	1.54 × 10 ⁻¹¹	6.34 × 10 ⁻¹¹	2.45×10^{-10}
	60% H	1.13 × 10 ⁻¹²	5.21 × 10 ⁻¹²	1.74 × 10 ⁻¹¹	2.31 × 10 ⁻¹¹	9.59 × 10 ⁻¹¹	3.67 × 10 ⁻¹⁰
	80% H	1.51 × 10 ⁻¹²	6.94 × 10 ⁻¹²	2.32 × 10 ⁻¹¹	3.08 × 10 ⁻¹¹	1.28 × 10 ⁻¹⁰	4.89 × 10 ⁻¹⁰
	100% H	1.88 × 10 ⁻¹²	8.68 × 10 ⁻¹²	2.9 × 10 ⁻¹¹	3.85 × 10 ⁻¹¹	1.6 × 10 ⁻¹⁰	6.11 × 10 ⁻¹⁰
	20% H	1.31 × 10 ⁻⁸	5.05 × 10 ⁻⁸	1.46 × 10 ⁻⁷	1.85 × 10 ⁻⁷	6.09 × 10 ⁻⁷	1.80 × 10 ⁻⁶
	40% H	5.22 × 10 ⁻⁸	2.02×10^{-7}	5.86 × 10 ⁻⁷	7.39 × 10 ⁻⁷	2.44 × 10 ⁻⁶	7.20 × 10 ⁻⁶
WD	60% H	1.18 × 10 ⁻⁷	4.56 × 10 ⁻⁷	1.32 × 10 ⁻⁶	1.66 × 10 ⁻⁶	5.45 × 10 ⁻⁶	1.62 × 10 ⁻⁵
	80% H	2.09 × 10 ⁻⁷	8.09 × 10 ⁻⁷	2.34 × 10 ⁻⁶	2.95 × 10 ⁻⁶	9.71 × 10 ⁻⁶	2.87 × 10 ⁻⁵
	100% H	3.26 × 10 ⁻⁷	1.26 × 10 ⁻⁶	3.65 × 10 ⁻⁶	4.6 × 10 ⁻⁶	1.51 × 10 ⁻⁵	4.49 × 10 ⁻⁵
	High	7.93 × 10 ⁻⁵	7.44 × 10 ⁻⁵	7.1 × 10 ⁻⁵	7.12 × 10 ⁻⁵	6.71 × 10 ⁻⁵	6.44 × 10 ⁻⁵
FA	Average	6.14 × 10 ⁻⁶	5.76 × 10 ⁻⁶	5.5 × 10 ⁻⁶	5.46 × 10 ⁻⁶	5.20 × 10 ⁻⁶	5.00 × 10 ⁻⁶
	Low	7.93 × 10 ⁻⁸	7.44 × 10 ⁻⁸	7.1 × 10 ⁻⁸	7.12 × 10 ⁻⁸	6.71 × 10 ⁻⁸	6.44 × 10 ⁻⁸

SA	2.95 × 10 ⁻⁵	2.66 × 10 ⁻⁵	2.45 × 10 ⁻⁵	2.4 × 10 ⁻⁵	2.16 × 10 ⁻⁵	1.95 × 10 ⁻⁵
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Table S6 Optimized geometries in Cartesian coordinates and normal mode frequencies of all species calculated at MP2/aug-cc-pVTZ level of theory

Species		Cartesian	coordinat	ce (Å)	Vibratio	nal freque	ncies (cm ⁻¹)
MR	С Н Н О	0.581872 0.865280 0.999450 0.999079 -0.794380	0.000089 -0.004096 0.903630 -0.900437 0.000046	-0.010498 1.050892 -0.458822 -0.465240 -0.007980	807.7226 1415.008 3006.008	968.7007 1432.323 3090.193	1127.056 1539.404 3131.184
HM	С Н Н О Н	0.684714 1.113909 1.229154 -0.670357 -1.088491	0.027438 0.987547 -0.882854 -0.125781 0.736930	-0.066480 0.173444 0.109015 0.021718 -0.057321	433.6348 1212.753 3194.145	621.2987 1367.984 3343.541	1067.206 1509.170 3854.749
ST	С Н Н О Н	-0.628082 -1.151053 -1.151052 0.742190 0.133075	0.000001 0.934246 -0.934234 0.000004 -0.000051	0.006767 -0.171669 -0.171728 -0.084151 0.976004	-2108.122 1149.538 2602.608	844.6455 1191.385 3112.367	1031.746 1502.643 3229.723
MR-WM	С Н Н О Н Н О	-1.304759 -0.603971 -2.305564 -1.365238 -0.824776 1.119029 2.646450 1.867007	-0.496026 -1.187156 -0.564287 -0.771375 0.798388 0.407694 0.355046 -0.206359	-0.011360 -0.482799 -0.438409 1.050999 -0.008100 0.017476 -0.003530 -0.001346	69.9095 179.4596 935.9952 1411.271 1642.0936 3149.0056	6.5984 350.26 1025.52 1435.192 3004.88 3727.8958	113.9642 437.0240 1123.5392 1535.8440 3097.0467 3 3915.5858
ММ-МН	С Н О Н Н Н	1.594154 2.647667 1.164833 0.817172 -2.475492 -0.114948 -2.324381 -1.874998	0.453076 0.262332 1.393885 -0.661979 -0.249859 -0.389470 0.137155 0.177916	-0.049929 0.057840 0.260395 -0.001150 0.639227 0.012611 -0.828992 0.020961	64.1035 185.1505 584.6835 1233.4945 1629.4883 3666.6407	80.9239 236.92 774.30 1436.24 3183.95 3813.7576	154.5240 288.9752 1116.4078 1508.4694 3330.1810 3935.3650

C -1.006422 0.515997 0.008835 H 0.363026 0.769681 0.015035 -1381.2761 188.7210 373. H -1.340918 1.026908 0.923637 402.1024 553.3765 617. H -1.273163 1.033722 -0.925034 821.99 1138.1143 1197 O -0.828801 -0.748636 0.010748 1211.1802 1375.31 1519 H 0.860446 -0.683665 -0.087404 1597.7765 1713.9734 2960 H 1.997319 0.057738 0.739278 3041.2434 3088.2784 3817 O 1.509028 0.086090 -0.100563 -0.100563 -0.100563 -0.100563 -0.100563	6247 1818 .4839 .3544 .7275
H 0.363026 0.769681 0.015035 -1381.2761 188.7210 373. H -1.340918 1.026908 0.923637 402.1024 553.3765 617. H -1.273163 1.033722 -0.925034 821.99 1138.1143 1197 O -0.828801 -0.748636 0.010748 1211.1802 1375.31 1519 H 0.860446 -0.683665 -0.087404 1597.7765 1713.9734 2960 H 1.987319 0.057738 0.739278 3041.2434 3088.2784 3817 O 1.509028 0.086090 -0.100563 -0.100563 -0.100563 -0.100563 -0.100563	6247 1818 .4839 .3544 .7275
H -1.340918 1.026908 0.923637 402.1024 553.3765 617. H -1.273163 1.033722 -0.925034 821.99 1138.1143 1197 O -0.828801 -0.748636 0.010748 1211.1802 1375.31 1519 H 0.860446 -0.683665 -0.087404 1597.7765 1713.9734 2960 H 1.987319 0.057738 0.739278 3041.2434 3088.2784 3817 O 1.509028 0.086090 -0.100563 -0.100563 -0.100563 -0.100563 -0.100563	1818 .4839 .3544 .7275
H -1.273163 1.033722 -0.925034 821.99 1138.1143 1197 M -0.828801 -0.748636 0.010748 1211.1802 1375.31 1519 H 0.860446 -0.683665 -0.087404 1597.7765 1713.9734 2960 H 1.987319 0.057738 0.739278 3041.2434 3088.2784 3817 O 1.509028 0.086090 -0.100563	.4839 .3544 .7275
VO H 0 -0.828801 -0.748636 0.010748 1211.1802 1375.31 1519 H 0.860446 -0.683665 -0.087404 1597.7765 1713.9734 2960 H 1.987319 0.057738 0.739278 3041.2434 3088.2784 3817 O 1.509028 0.086090 -0.100563 -0.100563 -0.100563 -0.100563 -0.100563	.3544
H 0.860446 -0.683665 -0.087404 1597.7765 1713.9734 2960 H 1.987319 0.057738 0.739278 3041.2434 3088.2784 3817 O 1.509028 0.086090 -0.100563	.7275
H 1.987319 0.057738 0.739278 3041.2434 3088.2784 3817 O 1.509028 0.086090 -0.100563	0 5 7 2
0 1.509028 0.086090 -0.100563	.05/3
C = 1.624684 - 0.646780 - 0.278440	
H = 0.804341 - 1.286595 - 0.080653 49.1017 65.67 66.66	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	4
H = 2.584594 - 1.132864 = 0.108322 = 199.9369 = 211.02 = 357.2	0
- $ -$	0 7
$\begin{bmatrix} 1 \\ -1 \\ -1 \\ -1 \\ -1 \\ -1 \\ -1 \\ -1 \\$, 97
H = 0.163054 1 336766 = 0.008796 1394 6224 1455 05 1529	90
H = 1.597196 = 0.355781 = 0.013842 = 1646.36 = 1665.91 = 2986	20 20
H = 2 365144 = 1 677582 = 0 120264 = 3081 95 = 3148 86 = 3617	99
$ \begin{bmatrix} 1 & 2.303144 & 1.077302 & 0.120204 & 3001.93 & 3140.00 & 3017. \\ 0 & -1 & 098996 & 1 & 445287 & 0 & 235062 & 3659 & 85 & 3900 & 18 & 3909 \\ \end{bmatrix} $	37
$\begin{bmatrix} 0 & 1.030330 & 1.443207 & 0.233002 & 3003300 & 3300.10 & 3303. \\ 0 & -1 & 523891 & -1 & 313881 & -0 & 166712 \end{bmatrix}$	57
$\begin{bmatrix} C & 1.577080 & -0.508740 & 0.410519 \\ H & 0.420104 & 1.412002 & 0.124840 & 78.42 & 105.78 & 142.10 \\ \end{bmatrix}$	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	70
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	/ 3 1 /
	14
$\begin{bmatrix} 0 & 1.3/19/7 & 0.433125 & -0.539185 & 398.46 & 550.56 & 699.11 \\ \end{bmatrix}$	/U F10
$\begin{bmatrix} 1 \\ -1 \\ -1 \\ -1 \\ -1 \\ -1 \\ -1 \\ -1 \\$	513
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	094
H = 1.443934 0.524452 0.106303 1632.48 1651.60 3159.2	826
H = 1.763657 = 1.978221 = 0.348706 = 3306.63 = 3489.52 = 3602.5	402
	4/0
0 - 1.381023 - 1.296227 - 0.211171	
C -1.552565 0.225967 0.177216	
Н -0.474998 1.003292 -0.016289 -1075.77 71.22 186.	2543
H -1.632392 0.400059 1.263376 314.6233 318.9303 349.	1730
H -2.319457 0.738103 -0.418138 387.4418 470.8772 539.	1420
0 -1.092684 -0.893167 -0.241631 582.0361 599.9233 907.	2542
m 1.889932 -1.540721 -0.454687 1072.7153 1136.1818 1198	.7408
н 0.464068 -1.171925 0.082117 1241.9055 1352.1661 1508	.8484
H 1.244853 0.563144 -0.089663 1586.5513 1647.0529 1694	.1074
Н 1.060237 2.003150 0.551133 2876.3894 2947.9467 3052	.1656
0 1.444328 -0.984749 0.191039 3101.5656 3831.9969 3884	.0190
0 0.783749 1.459054 -0.197052	

	С	-2.052698	0.524993	0.076215			
	Н	-1.306125	1.259131	-0.228755	40.3170	86.4580	125.6243
	Н	-2.151417	0.606489	1.168719	155.2585	180.6970	209.6524
	Н	-3.031596	0.694212	-0.370856	672.2190	807.7323	937.8172
A آتا	0	-1.604893	-0.764896	-0.134572	1042.9286	1079.5520	1142.664
R-I	С	1.722305	0.115209	0.020609	1202.5510	1375.1448	1410.067
Σ	0	1.153459	-1.089016	0.059260	1430.1417	1441.4301	1525.887
	Н	0.176890	-0.969956	-0.010754	1771.4689	2998.9995	3100.006
	0	1.137058	1.171977	-0.078662	3109.3138	3161.6177	3426.185
	Н	2.809616	0.024391	0.092494			
	C	-1 800717	0 523674	0 354276			
	н	0.157259	1.114783	-0.120741	92.1393	132.5318	158.0052
	н	-1 429815	0 444542	1 369361	177 8394	210 0715	335 1436
	н	-2 664446	1 132478	0 144673	671 4281	745 0239	801 0968
A	0	-1.676894	-0.553924	-0.455107	830.7942	1075.8084	1116.497
	C	1.608167	-0.096982	0.008791	1198.0583	1248.4473	1359.648
MZ	0	0.945221	-1.088904	0.243429	1420.7062	1439.6606	1509.519
	Н	-0.863789	-1.024344	-0.190475	1756.5087	3132.0642	3152.884
	0	1.138913	1.127501	-0.204314	3308.5377	3430.4857	3603.395
	Н	2.698165	-0.105002	-0.053284			
		1 606000	0 460592	0 226401			
		-0.558027	0.409505	-0.056682	_1581 09/1	111 5960	228 2081
	н Н	-1 532307	0.575994	1 312175	261 0540	389 4417	415 6065
	н	-2 495433	1 074226	-0 184142	544 6929	760 9463	1013 599
-		-1 456043	-0 683456	-0 308575	1067 4046	1162 5465	1198 660
S ^{E2}	C	1 495744	0 080996	0 008453	1242 5259	1294 9177	1317 449
	0	0.958896	-1.091916	0.150798	1406.1732	1476.9912	1541.168
	Н	-0.077257	-1.042473	0.019649	1595.5030	1743.4637	2359.819
	0	0.899805	1.154806	-0.162035	2975.1113	3133.1158	3138.370
	H	2.585598	0.062917	0.058366			
	C	-2 915023	0 196359	0 011898			
	н	-2.522735	1.068147	-0.830346	21.7927	47.5046	105.8865
	Н	-2.494425	0.965032	0.913268	108.4937	137.4555	224.7016
	н	-4.002036	0.510538	0.064505	267.1392	376.4545	424.1798
	0	-2.415190	-0.790996	0.023246	507.4708	536.6131	546.5106
A	0	0.131338	-0.989986	-0.786004	767.1543	827.4224	903.2702
	Н	-0.813612	-0.942525	-0.472221	911.0901	1035.7410	1151.8127
MH	0	0.076530	1.252092	0.228191	1162.49	1212.7792	1324.3341
	S	0.951852	0.149227	-0.071781	1391.2265	1437.2317	1456.8997
	0	1.283218	-0.502939	1.357044	1528.8446	3002.8137	3100.7217
	Н	2.054365	-1.079815	1.241329	3168.1656	3229.8462	3767.1996
	0	2.178972	0.295933	-0.802405			
	_	–					

	C 2.510875 0.680962 0.050198	
	н 0 795983 0 576275 1 022455	39 5454 92 0279 133 9790
	μ 2 00/3/5 1 188305 -0 763026	157 3001 103 4630 273 6302
	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	220 0106 202 2027 424 2770
	H 3.315531 1.172627 0.572400	339.8196 382.382/ 424.2//8
-	0 2.654199 -0.660886 -0.028989	503.4366 536.7415 547.1142
-S ¹	0 -0.008152 -0.880376 -0.871317	657.9004 732.0890 831.6837
μ	н 1.898349 -1.011354 -0.529868	851.1883 901.8792 1106.0538
	0 -0.139467 0.345177 1.273393	1161.4534 1207.9206 1254.4039
	s -0.907671 -0.146997 -0.013395	1271.2194 1407.9641 1454.8035
	0 -1.175219 1.21807 -0.807261	1508.6361 3147.9997 3237.1761
	н -1.951734 1.643462 -0.409544	3304.7289 3686.2906 3759.2855
	0 -2.156985 -0.684880 0.436762	
	C -2.450647 0.565668 -0.020888	
	н -1.457484 0.758118 -0.733978	-1703.5797 35.0188 114.6252
	н -2.050967 1.184776 0.796835	211.4644 219.0340 337.9861
	н -3.358948 0.928019 -0.493884	378.8078 409.2606 452.8162
	0 -2.324418 -0.723092 0.097017	479.6697 548.1197 562.8545
	0 -0.008582 -1.075531 0.623297	675.8058 818.4387 900.9640
So So	н -1.135673 -0.952674 0.453688	1002.4573 1074.7410 1151.5177
H	0 0.036471 0.650509 -1.128048	1196 6273 1220 2323 1253 6144
	S = 0.844939 = 0.052198 = 0.120732	1324 6264 1365 2764 1403 8972
	$\begin{array}{c} 0 \\ 0 \\ 0 \\ 110185 \\ -0 \\ 610565 \\ -0 \\ 504571 \\ 0 \\ 120752 \\ 0 \\ 120752 \\ 0 \\ 120752 \\ 0 \\ 120752 \\ 0 \\ 120752 \\ 0 \\ 120752 \\ 0 \\ 120752 \\ 0 \\ 120752 \\ 0 \\ 100752 \\ 100752 \\ 0 \\ 100752$	1510 71 1602 4501 1743 6568
		2002 2429 2196 2520 2765 2460
	0 1.104439 1.098098 0.975020	2993.2428 3186.3530 3765.2460
	H 1.8431/1 0.80/569 1.532654	
	0 0.000000 0.000000 0.118189	
MM	н 0.000000 0.758025 -0.472754	1627.7612 3824.7050 3950.6090
	н 0.000000 -0.758025 -0.472754	
	0 -1.385097 0.000601 0.110496	
	н -1.746597 -0.763119 -0.349950	127.0098 147.1099 154.9316
	н -1.747854 0.758911 -0.357831	184.1613 360.4078 630.2965
MD	0 1.512857 -0.000695 -0.121976	1629.3162 1650.2617 3718.7825
	н 0.559405 0.000611 0.048517	3813.9011 3915.1798 3935.2566
	н 1.912972 0.004353 0.751104	
	C = 0.000000 = 0.422392 = 0.000000	
	$H = 0.376774 \ 1.447695 \ 0.000000$	625 952 674 778 1058 557
A	$\begin{array}{c} 0 \\ 0 \\ 1 \\ 163418 \\ 0 \\ 108154 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ $	
E.	0 -1 034994 -0 439528 0 000000	1794 039 3125 306 3741 349
	u = 0.650614 = 1.221055 = 0.000000	1/94.039 5123.300 3741.349
	H -0.850814 -1.551055 0.000000	
	H 1.683905 -0.014800 1.107699	
	0 0.659484 1.084346 -0.827065	242.8958 328.1320 367.2603
	0 1.034771 -0.687872 0.848480	431.4837 485.9993 531.5543
SA	s 0.000058 0.000064 -0.159243	542.2237 821.4432 873.6608
	0 -1.035291 0.687175 0.848517	1155.1241 1170.0433 1219.2879
	н -1.684504 0.013827 1.106801	1469.2375 3760.6034 3764.8107
	0 -0.659005 -1.083655 -0.828259	

Species	MP2/aug-cc-pVTZ	CCSD(T)/aug-cc-pVTZ
MR	-114.84396077	-114.885062
TS	-114.79613291	-114.8328949
HM	-114.86634476	-114.8988607
MR-WM	-191.18101248	-191.2357163
TS _{WM}	-191.14159052	-191.1909453
HM-WM	-191.20605728	-191.2519222
MR-WD	-267.52313693	-267.5914694
TS _{WD}	-267.50181805	-267.5656003
HM-WD	-267.55128696	-267.6106135
MR-FA	-304.34423196	-304.4168392
TS _{FA}	-304.32465040	-304.395769
HM-FA	-304.36904354	-304.4328489
MR-SA	-814.28172138	-814.3693943
TS	-814.26141531	-814.3478167
HM-SA	-814.30415433	-814.3829675

Table S7 Absolute energies (in Hartree) of all species involved in isomerization of MR calculated at the two different levels of theory

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b) S. H. Robertson, D. R. Glowacki, C. H. Liang, C Morley, R. Shannon, M. Blitz, P. W. Seakins, M. J. Pilling, *MESMER (Master Equation Solver for Multi-Energy Well Reactions)*, 2008-2013; an object oriented C++ program implementing master equation methods for gas phase reactions with arbitrary multiple wells. http://sourceforge.net/projects/mesmer

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