

## Electronic Supplementary Information for “Characterization of the Temperature and Humidity-Dependent Phase Diagram of Amorphous Nanoscale Organic Aerosols”

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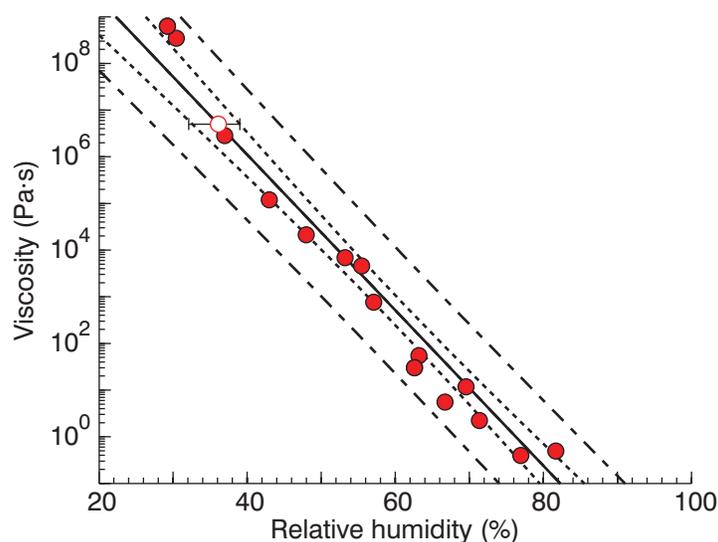
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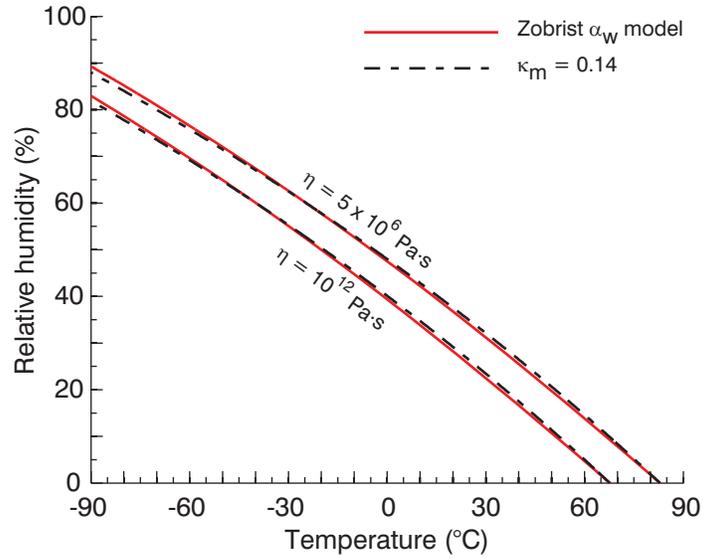
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Abbreviations used in this document: temperature ( $T$ ), viscosity ( $\eta$ ), coalescence characteristic relative humidity ( $RH_c$ ), coalescence characteristic temperature ( $T_c$ ), uncoalesced dimer diameter ( $D_{uc}$ ), coalesced dimer diameter ( $D_c$ ), logistic curve steepness parameter ( $k$ ), glass transition temperature ( $T_g$ ), mass-based hygroscopicity parameter ( $K_m$ )

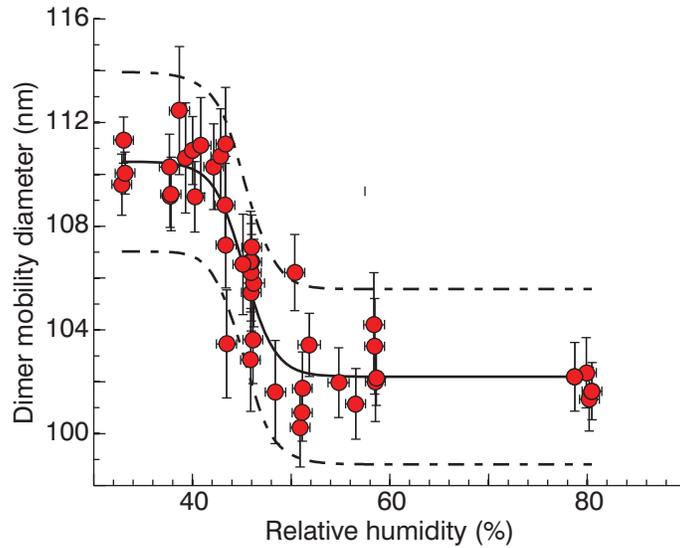
### 1. Additional Figures Referenced in the Manuscript



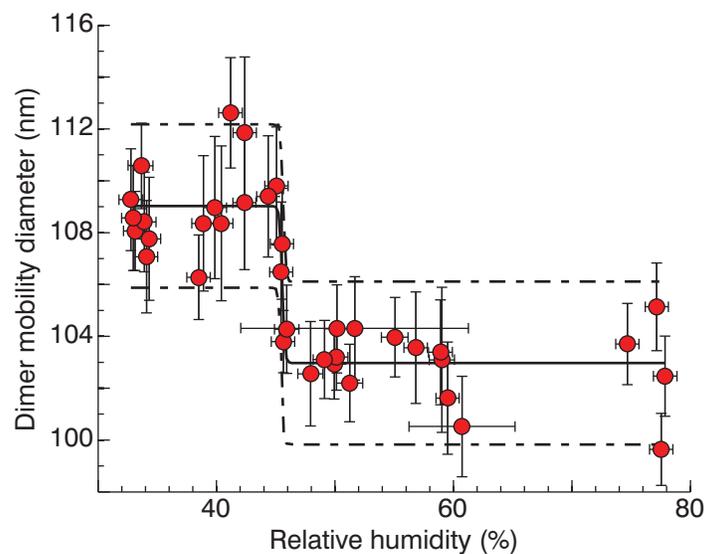
**Figure S1.** Plot depicting how the relative humidity where viscosity equals  $5 \times 10^6$  Pa s (open red circle) was interpolated from data digitized from Power et al.<sup>1</sup> (solid red circles). Solid black line: fitted linear regression line; dotted black lines: 95% confidence interval of the fitted regression line; dashed black lines: 95% observational prediction interval of the fitted regression line.



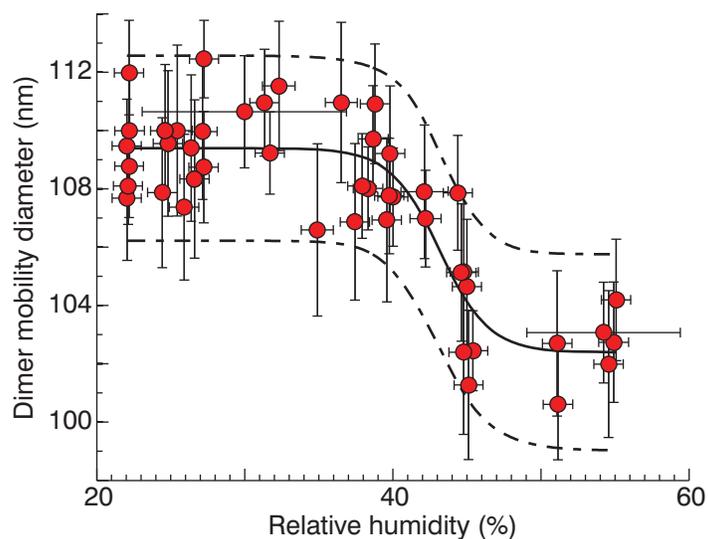
**Figure S2.** Variation in placement of modelled  $5 \times 10^6$  Pa·s and  $10^{12}$  Pa·s isopleths where the relationship between sucrose mass fraction and water activity was modelled using either the approach of Zobrist et al.<sup>2</sup> or a mass-based hygroscopicity parameter approach<sup>3</sup> with a fixed parameter value of 0.14, characteristic of sucrose.



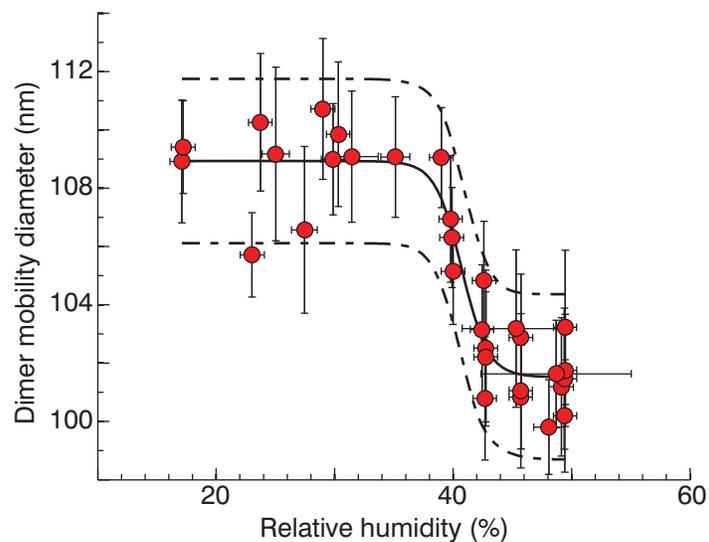
**Figure S3.** Measurements of dimer mobility diameter versus RH for the sucrose-sucrose isothermal humidification experiment performed at  $T = 4$  °C, including fitted logistic curve (solid black curve) and 95% observational prediction interval (dashed black curves). ( $RH_r = 45.2\% \pm 1.0\%$ ,  $D_{uc} = 110.5 \text{ nm} \pm 1.2 \text{ nm}$ ,  $D_c = 102.2 \text{ nm} \pm 0.9 \text{ nm}$ ,  $k = 0.6430$ )



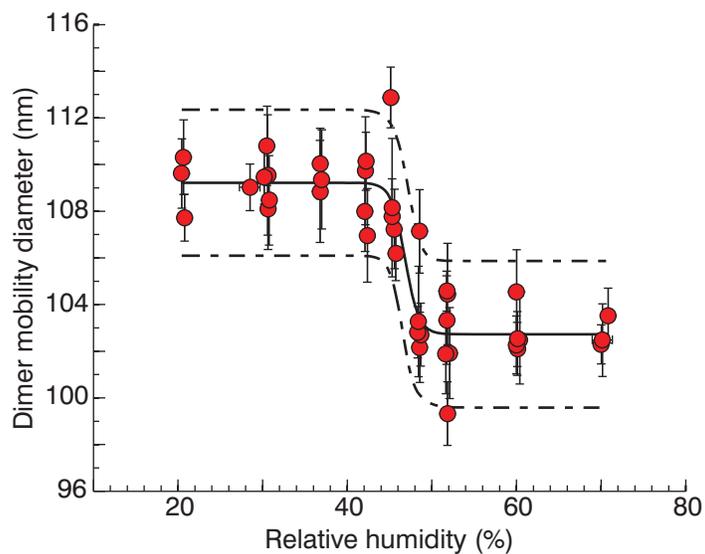
**Figure S4.** Measurements of dimer mobility diameter versus RH for the sucrose-sucrose isothermal humidification experiment performed at  $T = 5\text{ }^{\circ}\text{C}$ , including fitted logistic curve (solid black curve) and 95% observational prediction interval (dashed black curves). ( $RH_r = 45.5\% \pm 0.1\%$ ,  $D_{uc} = 109.0\text{ nm} \pm 0.8\text{ nm}$ ,  $D_c = 103.0\text{ nm} \pm 0.7\text{ nm}$ ,  $k = 9.525$ )



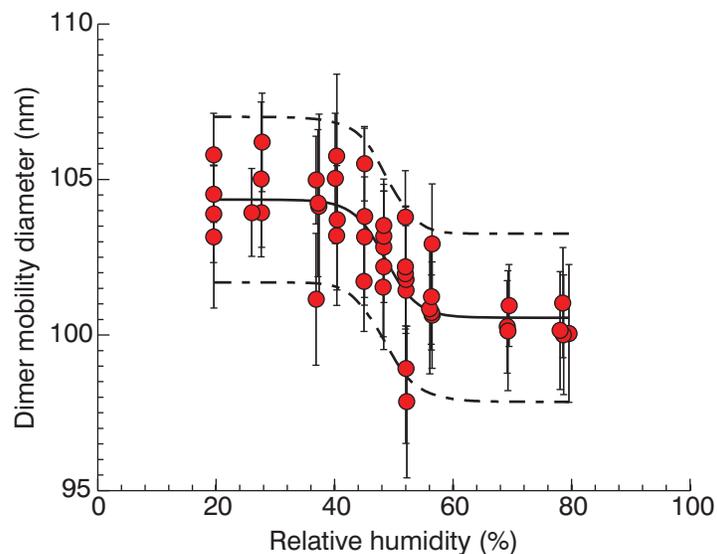
**Figure S5.** Measurements of dimer mobility diameter versus RH for the sucrose-sucrose isothermal humidification experiment performed at  $T = 12\text{ }^{\circ}\text{C}$ , including fitted logistic curve (solid black curve) and 95% observational prediction interval (dashed black curves). ( $RH_r = 43.2\% \pm 1.5\%$ ,  $D_{uc} = 109.4\text{ nm} \pm 0.7\text{ nm}$ ,  $D_c = 102.4 \pm 1.3\text{ nm}$ ,  $k = 0.5982$ )



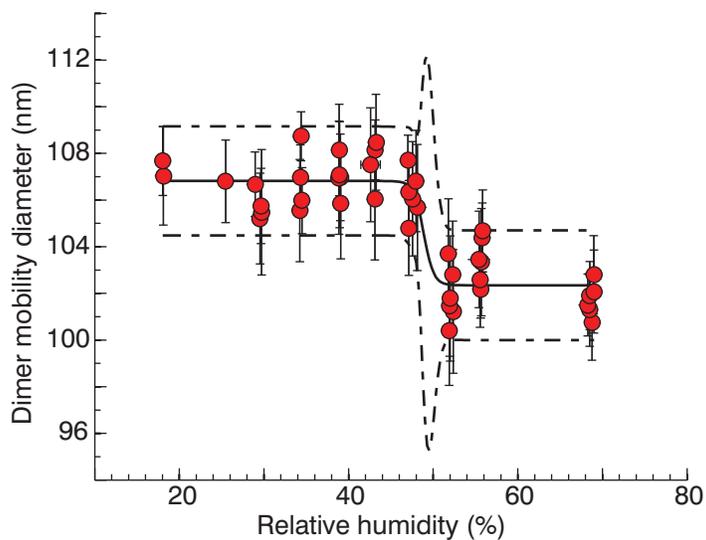
**Figure S6.** Measurements of dimer mobility diameter versus RH for the sucrose-sucrose isothermal humidification experiment performed at  $T = 15\text{ °C}$ , including fitted logistic curve (solid black curve) and 95% observational prediction interval (dashed black curves). ( $RH_r = 40.7\% \pm 1.0\%$ ,  $D_{uc} = 108.9\text{ nm} \pm 0.8\text{ nm}$ ,  $D_c = 101.5\text{ nm} \pm 0.9\text{ nm}$ ,  $k = 0.8967$ )



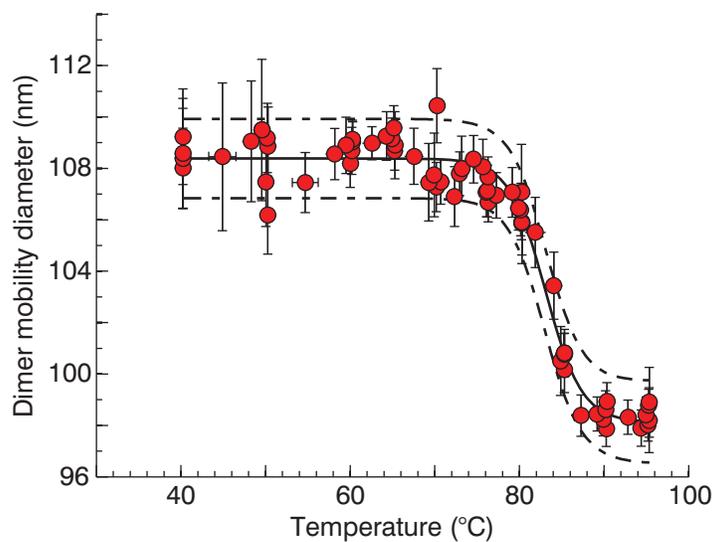
**Figure S7.** Measurements of dimer mobility diameter versus RH for the sucrose-sucrose cooling cycle experiment performed new for this work, including fitted logistic curve (solid black curve) and 95% observational prediction interval (dashed black curves). ( $RH_r = 46.8\% \pm 1.2\%$ ,  $T_r = 0.1\text{ °C} \pm 1.2\text{ °C}$ ,  $D_{uc} = 109.2\text{ nm} \pm 0.8\text{ nm}$ ,  $D_c = 102.7 \pm 0.8\text{ nm}$ ,  $k = 1.222$ )



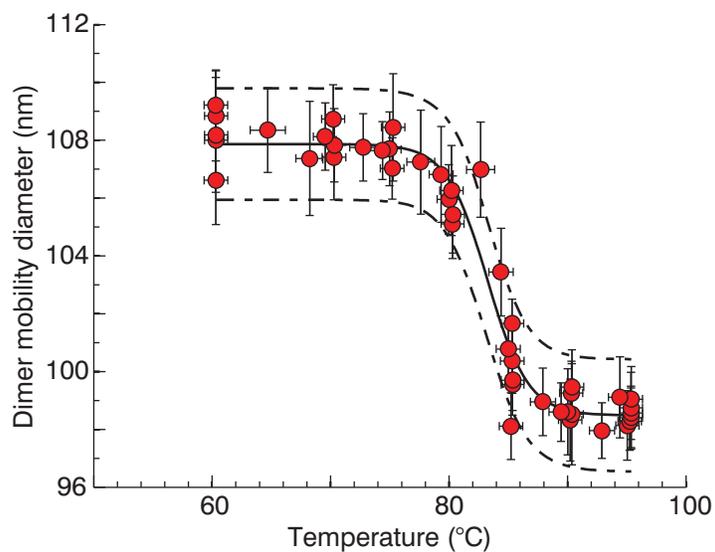
**Figure S8.** Measurements of dimer mobility diameter versus RH for the first sucrose-SDS cooling cycle experiment referenced in Table 1 of the manuscript, including fitted logistic curve (solid black curve) and 95% observational prediction interval (dashed black curves). ( $RH_r = 48.6\% \pm 3.1\%$ ,  $T_r = -1.3\text{ }^\circ\text{C} \pm 1.1\text{ }^\circ\text{C}$ ,  $D_{uc} = 104.4\text{ nm} \pm 0.7\text{ nm}$ ,  $D_c = 100.6\text{ nm} \pm 0.9\text{ nm}$ ,  $k = 0.3698$ )



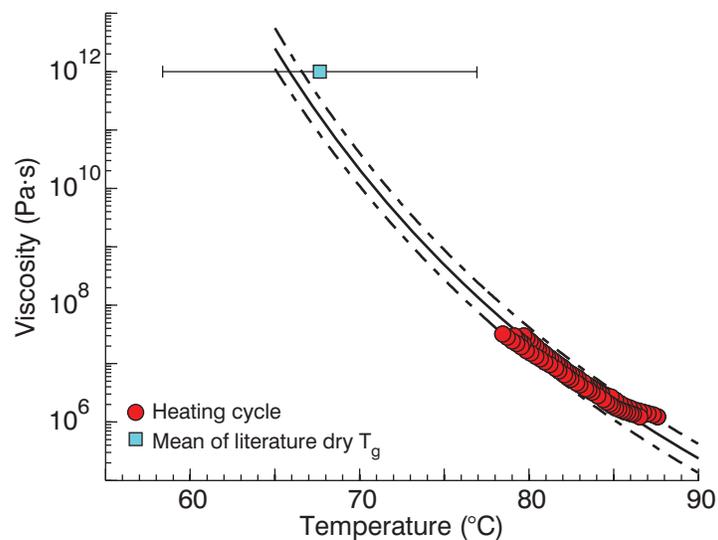
**Figure S9.** Measurements of dimer mobility diameter versus RH for the second sucrose-SDS cooling cycle experiment referenced in Table 1 of the manuscript, including fitted logistic curve (solid black curve) and 95% observational prediction interval (dashed black curves). ( $RH_r = 48.9\% \pm 3.5\%$ ,  $T_r = -3.4\text{ }^\circ\text{C}$ ,  $D_{uc} = 106.8\text{ nm} \pm 0.5\text{ nm}$ ,  $D_c = 102.3\text{ nm} \pm 0.6\text{ nm}$ ,  $k = 1.697$ )



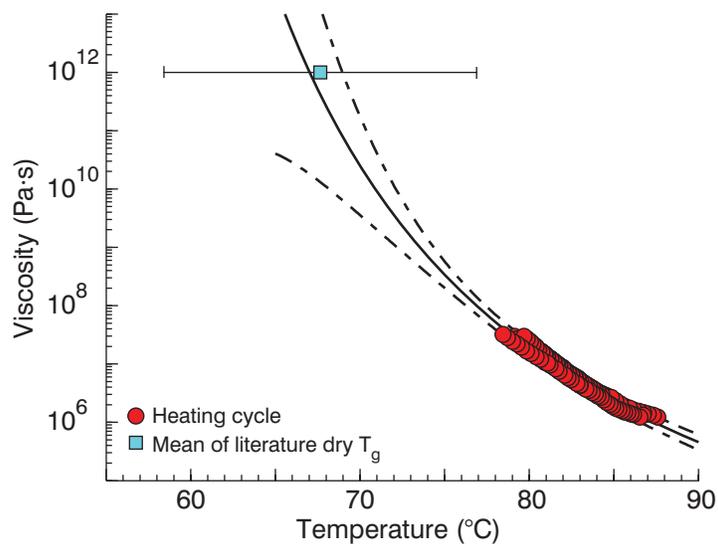
**Figure S10.** Measurements of dimer mobility diameter versus RH for the first sucrose-sucrose heating cycle experiment referenced in Table 1 of the manuscript, including fitted logistic curve (solid black curve) and 95% observational prediction interval (dashed black curves). ( $T_r = 83.1 \text{ }^\circ\text{C} \pm 0.6 \text{ }^\circ\text{C}$ ,  $RH_r = 0.8\% \pm 0.1\%$ ,  $D_{uc} = 108.4 \text{ nm} \pm 0.3 \text{ nm}$ ,  $D_c = 98.1 \text{ nm} \pm 0.5 \text{ nm}$ ,  $k = 0.4646$ )



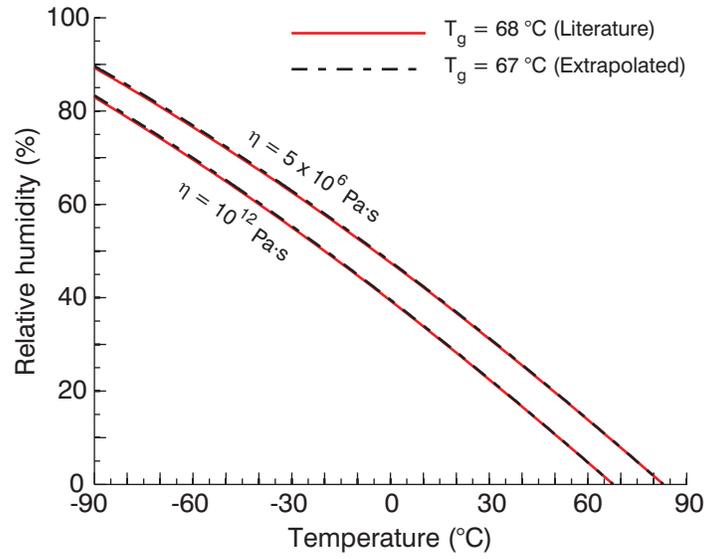
**Figure S11.** Measurements of dimer mobility diameter versus RH for the second sucrose-sucrose heating cycle experiment referenced in Table 1 of the manuscript, including fitted logistic curve (solid black curve) and 95% observational prediction interval (dashed black curves). ( $T_r = 83.2 \text{ }^\circ\text{C} \pm 0.7 \text{ }^\circ\text{C}$ ,  $RH_r = 0.8\% \pm 0.1\%$ ,  $D_c = 107.9 \text{ nm} \pm 0.5 \text{ nm}$ ,  $D_{uc} = 98.5 \text{ nm} \pm 0.5 \text{ nm}$ ,  $k = 0.5814$ ).



**Figure S12.** Fitted VFT curve as derived for sucrose when fixing the A parameter to a value of -5. The curve fit utilized both viscosity data derived from heating cycle experiments and mean literature  $T_g$ . Error bars associated with the glass transition point correspond to one standard deviation of the literature values utilized. Black dashed curves correspond to the 95% observational prediction interval of the fitted VFT equation.



**Figure S13.** Fitted VFT curve as derived for sucrose utilizing only data from heating cycle experiments and not considering mean literature  $T_g$ . Error bars associated with the glass transition point correspond to one standard deviation of the literature values utilized. Black dashed curves correspond to the 95% observational prediction interval of the fitted VFT equation.



**Figure S14.** Variation in placement of modelled  $5 \times 10^6 \text{ Pa}\cdot\text{s}$  and  $10^{12} \text{ Pa}\cdot\text{s}$  isopleths where dry sucrose glass transition temperature was determined either using an average literature value or via extrapolation of our own dry sucrose viscosity measurements.

## 2. Additional Table Referenced in the Manuscript

**Table S1.** Viscosity measurements for amorphous sucrose at various temperatures as derived from the three heating cycle experiments performed for this work. Experiment numbering corresponds to order of mention in Table 1 of the main manuscript.

Experiment #1 ( $T_r = 83.1\text{ }^\circ\text{C}$ )		Experiment #2 ( $T_r = 83.2\text{ }^\circ\text{C}$ )		Experiment #3 ( $T_r = 82.8\text{ }^\circ\text{C}$ )	
$T\text{ (}^\circ\text{C)}$	$\eta\text{ (Pa}\cdot\text{s)}$	$T\text{ (}^\circ\text{C)}$	$\eta\text{ (Pa}\cdot\text{s)}$	$T\text{ (}^\circ\text{C)}$	$\eta\text{ (Pa}\cdot\text{s)}$
78.46	$3.22 \times 10^7$	79.69	$2.96 \times 10^7$	79.13	$2.96 \times 10^7$
78.73	$2.82 \times 10^7$	79.87	$2.66 \times 10^7$	79.30	$2.66 \times 10^7$
79.01	$2.47 \times 10^7$	80.05	$2.41 \times 10^7$	79.48	$2.42 \times 10^7$
79.29	$2.18 \times 10^7$	80.22	$2.18 \times 10^7$	79.66	$2.19 \times 10^7$
79.56	$1.92 \times 10^7$	80.4	$1.97 \times 10^7$	79.83	$1.99 \times 10^7$
79.84	$1.69 \times 10^7$	80.58	$1.77 \times 10^7$	80.01	$1.80 \times 10^7$
80.12	$1.52 \times 10^7$	80.75	$1.62 \times 10^7$	80.18	$1.64 \times 10^7$
80.39	$1.35 \times 10^7$	80.93	$1.48 \times 10^7$	80.36	$1.51 \times 10^7$
80.67	$1.20 \times 10^7$	81.10	$1.35 \times 10^7$	80.54	$1.38 \times 10^7$
80.95	$1.07 \times 10^7$	81.28	$1.23 \times 10^7$	80.71	$1.26 \times 10^7$
81.23	$9.61 \times 10^6$	81.46	$1.12 \times 10^7$	80.89	$1.15 \times 10^7$
81.50	$8.66 \times 10^6$	81.63	$1.02 \times 10^7$	81.07	$1.05 \times 10^7$
81.78	$7.69 \times 10^6$	81.81	$9.43 \times 10^6$	81.24	$9.72 \times 10^6$
82.06	$6.92 \times 10^6$	81.99	$8.68 \times 10^6$	81.42	$8.98 \times 10^6$
82.33	$6.23 \times 10^6$	82.16	$7.89 \times 10^6$	81.59	$8.22 \times 10^6$
82.61	$5.60 \times 10^6$	82.34	$7.22 \times 10^6$	81.77	$7.50 \times 10^6$
82.89	$5.05 \times 10^6$	82.51	$6.67 \times 10^6$	81.95	$6.94 \times 10^6$
83.16	$4.55 \times 10^6$	82.69	$6.12 \times 10^6$	82.12	$6.41 \times 10^6$
83.44	$4.12 \times 10^6$	82.87	$5.62 \times 10^6$	82.30	$5.88 \times 10^6$
83.72	$3.77 \times 10^6$	83.04	$5.18 \times 10^6$	82.48	$5.43 \times 10^6$
83.99	$3.45 \times 10^6$	83.22	$4.76 \times 10^6$	82.65	$5.01 \times 10^6$
84.27	$3.13 \times 10^6$	83.39	$4.39 \times 10^6$	82.83	$4.63 \times 10^6$
84.55	$2.87 \times 10^6$	83.57	$4.07 \times 10^6$	83.01	$4.28 \times 10^6$
84.83	$2.65 \times 10^6$	83.75	$3.78 \times 10^6$	83.18	$3.98 \times 10^6$
85.10	$2.34 \times 10^6$	83.92	$3.54 \times 10^6$	83.36	$3.72 \times 10^6$
85.38	$2.09 \times 10^6$	84.10	$3.27 \times 10^6$	83.53	$3.48 \times 10^6$
85.66	$1.90 \times 10^6$	84.28	$3.04 \times 10^6$	83.71	$3.23 \times 10^6$
85.93	$1.74 \times 10^6$	84.45	$2.83 \times 10^6$	83.89	$3.00 \times 10^6$
86.21	$1.62 \times 10^6$	84.63	$2.66 \times 10^6$	84.06	$2.81 \times 10^6$
86.49	$1.52 \times 10^6$	84.80	$2.42 \times 10^6$	84.24	$2.65 \times 10^6$
86.76	$1.45 \times 10^6$	84.98	$2.21 \times 10^6$	84.42	$2.41 \times 10^6$
87.04	$1.38 \times 10^6$	85.16	$2.03 \times 10^6$	84.59	$2.20 \times 10^6$
87.32	$1.33 \times 10^6$	85.33	$1.88 \times 10^6$	84.77	$2.03 \times 10^6$
87.59	$1.22 \times 10^6$	85.51	$1.76 \times 10^6$	84.94	$1.88 \times 10^6$
		85.69	$1.65 \times 10^6$	85.12	$1.76 \times 10^6$
		85.86	$1.57 \times 10^6$	85.30	$1.66 \times 10^6$
		86.04	$1.50 \times 10^6$	85.47	$1.58 \times 10^6$
		86.21	$1.44 \times 10^6$	85.65	$1.51 \times 10^6$
		86.39	$1.39 \times 10^6$	85.83	$1.45 \times 10^6$
		86.57	$1.35 \times 10^6$	86.00	$1.40 \times 10^6$
		86.74	$1.31 \times 10^6$	86.18	$1.36 \times 10^6$
				86.35	$1.32 \times 10^6$
				86.53	$1.22 \times 10^6$

### 3. References

- 1 R. M. Power, S. H. Simpson, J. P. Reid and A. J. Hudson, *Chem. Sci.*, 2013, **4**, 2597–2604.
- 2 B. Zobrist, C. Marcolli, D. A. Pedernera and T. Koop, *Atmos. Chem. Phys.*, 2008, **8**, 5221–5244.
- 3 E. Mikhailov, S. Vlasenko, D. Rose and U. Pöschl, *Atmos. Chem. Phys.*, 2013, **13**, 717–740.