Supporting Information

A novel multi-stage microbial desalination cell for simultaneous desalination and enhanced organics and nitrogen removal from domestic wastewater

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MATERIALS AND METHODS

Analysis and calculations. The concentration of COD, total nitrogen, and NH₄⁺-N of wastewater were measure using colorimetric method (5B-3C, Lianhua, China). The MDC voltage (U) across the external resistance (R_{ex}) were automatically measured and recorded every 5 min suing a data acquisition system (DAQ2213, ADLINK, China). Current (I) was determined according to Ohm's law: $I = U/R_{ex}$. Power density (P) and internal resistance (R_{in}) were obtained from polarization curve, and the power density were calculated based on the MDC sectional area. The conductivity of the concentrate and wastewater were automatically measured and recorded every 5 min with a conductivity meter (Inlab 731, Mettler Toldeo, USA). The desalination efficiency (DE) in wastewater and salt recovery efficiency (RE) in salt water were calculated based on corresponding conductivity change as follow:

$$DE = \frac{C_{\text{was,inf}} - C_{\text{was,eff}}}{C_{\text{was,inf}}}$$
(1)

$$RE = \frac{C_{\text{con,i}} - C_{\text{con,f}}}{C_{\text{con,i}}}$$
(2)

where $C_{\text{was,inf}}$ and $C_{\text{was,eff}}$ (mS/cm) are the conductivity of wastewater influent and effluent (or effluent of each chambers) respectively, $C_{\text{con,i}}$ and $C_{\text{con,f}}$ (mS/cm) are the initial and final conductivities of the concentrate, respectively.

Coulombic efficiency (I_i) were utilized to evaluate the percentage of coulombs contained in wastewater to produce electricity:

$$\eta = \frac{8\int Idt}{F \cdot \Delta \text{COD} \cdot Q \cdot t}$$
(3)

where F is Faraday's constant (96485 C/mol), \triangle COD is the COD change (g/L) of wastewater, Q is the flow rate of wastewater, t is operation time.

Current efficiency (*CE*) was utilized to evaluate the percentage of current being used to remove salt from wastewater (CE_{was}) or to recover salt in concentrate (CE_{con}):

$$CE_{\text{was}} = \frac{F(C_{\text{was,inf}} - C_{\text{was,eff}}) \cdot Q \cdot t}{M \cdot \int I dt}$$
(4)

$$CE_{\rm con} = \frac{F(C_{\rm con,f} - C_{\rm con,i}) \cdot V_{\rm con,f}}{M \cdot \int I dt}$$
(5)

where M is the molecular weight of salt, which was regarded to be all existed in the form of NaCl (M: 58.5 g/mol) in this study.



Figure S1 Fabrication of the M-MDC. (A) activated carbon granules in the electrode chambers; (B) over all view of the M-MDC; (C) Titanium meshes in the electrode chambers; (D) AEM in the concentrate chamber. ACG: activated carbon granular;

CEM: cation exchange membrane; AEM: anion exchange membrane; Con:

concentrate; Ww: wastewater.



Figure S2 Schematic of the M-MDC operated with AACC mode. Ww: wastewater; Con: concentrate (or cocnetrate chamber); ACG: activated carbon granular; Mixed IER: mixed ion exchange resins; CEM: cation exchange membrane; AEM; anion exchange membrane; AH: areation head; An: anode; Ca: cathode.



Figure S3 The effluent quality of MDC during one concentrate replacement cycle at each HRT. (A) HRT of 4 h; (B) HRT of 8 h; (C) HRT of 12 h; (D) HRT of 16 h. Inf: influent.



Figure S4 Coulombic efficiency and current efficiency calculated based on the removed salt from wastewater and the recovered salt in concentrate.



Figure S5 Removal efficiency of TN and NH_4^+ -N in each chamber of M-MDC at HRT of 16 h.



Figure S6 pH of wastewater in each chamber of the M-MDC during operation in ACAC mode.



Figure S7 Effluent quality of each chamber in M-MDC when operated in AACC mode. (HRT of 64 h, adding 1.4 g/L glucose).



Figure S8 pH of wastewater in each chamber of the M-MDC during operation in AACC mode.