Electronic Supplementary Material (ESI) for Lab on a Chip. This journal is © The Royal Society of Chemistry 2016

Supporting Information

Monitoring CO_2 invasion processes at pore scale using Geological Labs on Chip

S. Morais, N. Liu, A. Diouf, D. Bernard, C. Lecoutre, Y. Garrabos, S. Marre*

<u>S1 – Microfabrication procedure and set-up</u>

Microfabrication

Fig. S1 summarized the microfabrication procedure used for developing the GLoCs devices.



Fig. S1.1 Scheme of the GLoCs microfabrication procedure.

In details: The network is etched on a silicon wafer (<100> orientation perpendicular to the surface) purchased from BT Electronics, Inc. The purchased silicon wafer is already coated with a thermal silicon oxide layer of 500 nm on both sides. The photolithography process consists in:

- (i) Spin coating a thin layer (4 µm) of positive photoresist (S1818 from Shipley),
- Exposing the coated wafer with UV light (6 mW/cm², 45 sec) through a soft mask.
 The positive photoresist exposed to UV through the mask is removed from the silicon oxide surface with a developer (MF319 from Shipley).
- (iii) Removing the silicon dioxide with a buffered HF solution (hydrofluoric acid + NH_4F) in water (Sigma Aldrich).
- (iv) Dissolving the remaining photoresist with acetone.

The wet etching of the silicon is done with a solution of Tetramethylammonium hydroxide (TMAH) 25% in water (Sigma Aldrich) at an etching rate of 0.7 μ m/min. A thin silicon oxide layer is deposited onto the etched silicon wafer using a wet oxidation process conducted in an oven at 1000°C during 2 hours under water saturated atmosphere. The injection holes are

drilled with a sandblasting equipment. Eventually, the etched silicon wafer is anodically bonded to a Pyrex wafer.

<u>Set-up</u>

The micro fabricated pore network was then connected to the external inlet/outlet tubing thanks to a homemade compression fitting:



Fig. S1.2 Scheme of the compression fitting used in this study. The scheme was adapted from: "Marre, S., Adamo, A., Basak, S., Aymonier, C. & Jensen, K. F. Design and Packaging of Microreactors for High Pressure and High Temperature Applications. *Ind. Eng. Chem. Res.* **49**, 11310–11320 (2010)."

A general picture of the micromodel / compression fitting assembly is given hereafter:



Fig. S1.3 Picture of the [micromodel + Compression fitting] assembly.

S2 - Wetting contact angle measurements

The contact angle measurement are obtained by an image analyses with ImageJ¹ and the contact angle plug-in of Marco Brugnara.² Two types of images were used for these measurements. First, the interface of water and CO_2 into a straight feeding microchannel (Fig S2-a.). Here, the contact angle corresponds to the angle between the wall of the channel and the tangent to the interface meniscus (Fig S2-b.). Secondly, the shape of the dome on the silica plots are also used for these measurements. The contact lines between the water and the solid are curved (Fig S2-c.), the contact angle is here between the tangent of the circular plot and the tangent the water dome (Fig S2-d.). The obtained values for θ are reported in Table S2.



Fig. S2 Example of observations and further measurements of the contact angle at p = 4.5 MPa T = 28 °C with Micromodel M2. (a, b) inside the feeding microchannel and (c, d) around a circular plot.

p (MPa)	T (°C)	Phase	heta (deg)	
4.5	28	Gas	25.7 ± 3.1	
6	28	Gas	30.7 ± 1.9	
8	28	Liquid	39.2 ± 2.4	
8	50	Supercritical	36.7 ± 2.6	
8	75	Supercritical	35.7 ± 2.1	

Table S2 Contact angle values measured depending on the operating conditions.

¹ Abramoff, M. D.; Magalhaes, P. J.; Ram, S. J. Image Processing with ImageJ. Biophotonics Int. 2004, 11 (7), 36–42. (52)

² M. Brugnara, contact Email: marco.brugnara@ing. unitn.it)

<u>S3 – General properties of the fluids depending on the p and T conditions</u>

Table S3 summarizes the thermophysical properties of water and CO_2 in the studied conditions. Density and viscosity were obtained from the NIST,³ while the interfacial tension values were obtained from the literature (references mentioned in the Table).

P (MPa)	т (°С)	Phase	H₂O viscosity μH₂O (μPa∙s)	H ₂ O density ρH ₂ O (kg m ⁻³)	CO₂ viscosity μCO₂ (μPa∙s)	CO2 density pCO2 (kg m ⁻³)	Viscosity ratio log M (M=μCO ₂ / μH ₂ O)	Interfacial tension γ (mN∙m⁻¹)
4.5	28	Gas	831.9	998.2	16.3	107.7	-1.17	43.2 ⁴
6	28	Gas	831.7	998.9	18.1	178.0	-1.66	36.04
8	28	Liquid	831.5	999.7	60.7	736.5	-1.14	30.3 ⁴
8	50	Supercritical	548.3	991.5	20.5	219.2	-1.43	37.5 ⁵
8	75	Supercritical	379.8	978.3	20.0	166.5	-1.28	38.6 ⁶

Table S3 Thermophysical properties of water and CO_2 in the studied conditions.

³ http://webbook.nist.gov/chemistry/fluid/

⁴ Georgiadis, A., Maitland, G., Trusler, J. P. M. & Bismarck, A. Interfacial Tension Measurements of the (H₂O + CO₂) System at Elevated Pressures and Temperatures [†]. *J. Chem. Eng. Data* **55**, 4168–4175 (2010).

⁵ Chun, B.-S. & Wilkinson, G. T. Interfacial tension in high-pressure carbon dioxide mixtures. *Ind. Eng. Chem. Res.* **34**, 4371–4377 (1995).

⁶ Bachu, S., Bennion, D. B., Clark, K., Nw, R. & Tn, A. Interfacial Tension between CO 2 , Freshwater , and Brine in the Range of Pressure from (2 to 27) MPa , Temperature from (20 to 125) ° C , and Water Salinity from (0 to 334 000) mg · L - 1. 765–775 (2009).

<u>S4 – Dimensionless numbers for the considered experimental conditions</u>

Table S4 summarizes the calculated dimensionless numbers (*Log Ca, Log M* and *Re*) for the different experiments performed in the frame of this study. *Ca* was calculated using Eq. 2.

Table S4 Dimensionless numbers (*Log Ca, Log M* and *Re* for the considered experimental conditions.

Micromodel		М1			M2				
p.T conditions	Q _{pump} (µl min⁻¹)	Log Ca	Log M	u _{co2} (m s ⁻¹)	Re	Log Ca	Log M	u _{co2} (m s ⁻¹)	Re
4.5 MPa 28 °C	100	-3.93	-1,71	0.28	41.1	-3.85	-1,66	0.33	38.5
6 MPa 28°C	100	-4.02	-1,66	0.17	37.9	-3.94	-1,71	0.21	35.5
8 MPa 28°C	100	-3.99	-1,14	0.04	11.5	-3.92	-1,14	0.05	10.8
8 MPa 50°C	100	-4.02	-1,43	0.14	34.1	-3.94	-1,43	0.17	31.9
8 MPa 75°C	100	-3.92	-1,28	0.19	35.0	-3.84	-1,28	0.22	32.7
8 MPa 50°C	200	-3.72	-1,43	0.29	68.2	-3.64	-1,43	0.34	63.9

<u>S5 – Location of our experiments in the Lenormand's stability diagram⁷</u>

Based on the calculation of *Log Ca* and *Log M* for each of the investigated conditions, we have defined the area of our experiments in the Lenormand's invasion stability diagram in which plots *Log Ca* as a function of *Log M* and determines the flow regime (viscous fingering, capillary fingering, stable and unstable displacement regime (colourless area in Fig. S5). The area in which our experiments were performed is located in the red square, *i.e.* in the unstable displacement regime.



Fig. S5 Location of our experimental investigated conditions in the Lenormand phase diagram (red square), in the unstable displacement regime.

⁷ R. Lenormand, Journal of Physics: Condensed Matter, 1990, **2**, SA79

<u>S6 – Drying mechanism as a function of the temperature</u>

Figure S6 shows the influence of temperature over the drying kinetics, demonstrating a faster drying process at higher temperature (75°C compared to 50°C both at 8 MPa). Typical pictures of the porous medium are shown as a function of the injection time from t = 5s to t = 75s).



Fig. S6 Drying process for different times during the invasion experiment (with micromodel M1) at two different temperatures (50 and 75°C).

<u>S7 – Solubility of CO₂ in water as a function of temperature and pressure</u>



Fig. S7 Solubility data of water in CO₂ at different pressures and temperatures (adapted from Spycher, N., Pruess, K. & Ennis-King, J. CO2-H2O mixtures in the geological sequestration of CO2. I. Assessment and calculation of mutual solubilities from 12 to 100°C and up to 600 bar. *Geochim. Cosmochim. Acta* **67**, 3015–3031 (2003)).