

Combined experimental and theoretical approach to study SmC→N_{Cybc} phase transition studies of a four-ring bent-core liquid crystal†

Swapnil Singh^a, Rahul Deb^b, Nirmalangshu Chakraborty^b, Harshita Singh^a, Vineet Gupta^a, Kirti Sinha^a, Poonam Tandon^{*a}, M. M. Omelchenko^d, N.V.S. Rao^b and A.P. Ayala^c

^aDepartment of Physics, University of Lucknow, Lucknow-226007, India

^bChemistry Department, Assam University, Silchar-788011, Assam, India

^cDepartamento de Física, Universidade Federal do Ceará, C.P. 6030, 60.455-900 Fortaleza, CE, Brazil

^dDepartment of Chemistry, Warsaw University, Al. Zwirki i Wigury 101, 02-089 Warsaw, Poland

†Electronic Supplementary Information (ESI)

Synthesis:

[3-(4-pentyloxy-2-hydroxybenzylideneamino)-2-methyl benzoic acid], **3**:

An ethanolic solution of 2-methyl-3-aminobenzoic acid **2** (0.45g, 3 mmol) was added to an ethanolic solution (20 ml) of 4-n-pentyloxy-2-hydroxybenzaldehyde **1** (0.63 g, 3mmol). The mixture was refluxed with a few drops of glacial acetic acid as catalyst for 4 hours to yield the yellow colored Schiff's base. The precipitate was collected by filtration from the hot solution and recrystallized several times from absolute ethanol to give a pure compound **3**. Yield = 0.81g, (80%).

IR ν_{\max} in cm^{-1} : 1618 ($\nu_{\text{CH=N}}$, imine); 1719 ($\nu_{\text{C=O}}$, acid), 3425($\nu_{\text{O-H}}$, H-bonded); ¹H NMR (CDCl₃, 400 MHz): δ = 13.49 (s, 1H, -OH), 9.99 (s, 1H, -COOH), 8.35 (s, 1H, -CH=N-), 7.88 (d, 1H, J = 8.4Hz, ArH), 7.46 (d, 1H, J = 8.4Hz, ArH), 7.33 (t, 1H, J = 8.0 Hz, ArH), 7.29 (d, 1H, J = 7.8 Hz, ArH), 6.98 (d, 1H, J = 8.4 Hz, ArH), 6.43 (s, 1H, ArH), 4.03 (t, 2H, J = 7.8Hz, - O-CH₂-), 2.46 (s, 3H, Ar-CH₃), 1.57 (q, 2H, -O-CH₂-CH₂-), 1.29-1.21 (m, 4H, -O-(CH₂)₂-(CH₂)₂-), 0.88 (t, 3H, J = 7.8Hz, -O-(CH₂)₄-CH₃). Elemental analysis calculated for C₂₀H₂₃NO₄: C = 70.36%; H = 6.79%; N = 4.10% Found C = 70.33%; H = 6.76%; N = 4.07%.

[4-(4-heptyloxy-2-hydroxybenzylideneamino) phenol], **6** :

An ethanolic solution of 4-aminophenol **5** (0.32g, 3 mmol) was added to an ethanolic solution (20 ml) of 4-n-heptyloxysalicylaldehyde **4** (0.70g, 3 mmol). The mixture was refluxed with a few drops of glacial acetic acid as catalyst for 4 hours to yield the yellow colored Schiff's base. The

precipitate was collected by filtration from the hot solution and recrystallized several times from absolute ethanol to give a pure compound **6**. Yield = 0.34g, (77%).

IR ν_{\max} in cm^{-1} : 1627 ($\nu_{\text{CH}=\text{N}}$, imine); 3412 ($\nu_{\text{O-H}}$, H-bonded); ^1H NMR (CDCl_3 , 400 MHz): δ = 13.42 and 13.39 (s, 2H, -OH), 8.39 (s, 1H, -CH=N), 7.43 (d, 1H, $J = 8.4\text{Hz}$, ArH), 7.22 (d, 2H, $J = 8.0\text{Hz}$, ArH), 6.91 (d, 2H, $J = 8.4\text{Hz}$, ArH), 6.65 (d, 1H, $J = 7.8\text{Hz}$, ArH), 6.34 (s, 1H, Ar-H), 4.01 (t, 2H, $J = 7.8\text{Hz}$, -O-CH₂-), 1.63 (q, 2H, -O-CH₂-CH₂-), 1.31-1.22 (m, 8H, -O-(CH₂)₂-(CH₂)₄-), 0.98 (t, 3H, $J = 7.8\text{Hz}$, -O-(CH₂)₆-CH₃). Elemental analysis calculated for C₂₀H₂₅NO₃: C = 73.37%; H = 7.70%; N = 4.28% Found C = 73.33%; H = 7.67%; N = 4.25%.

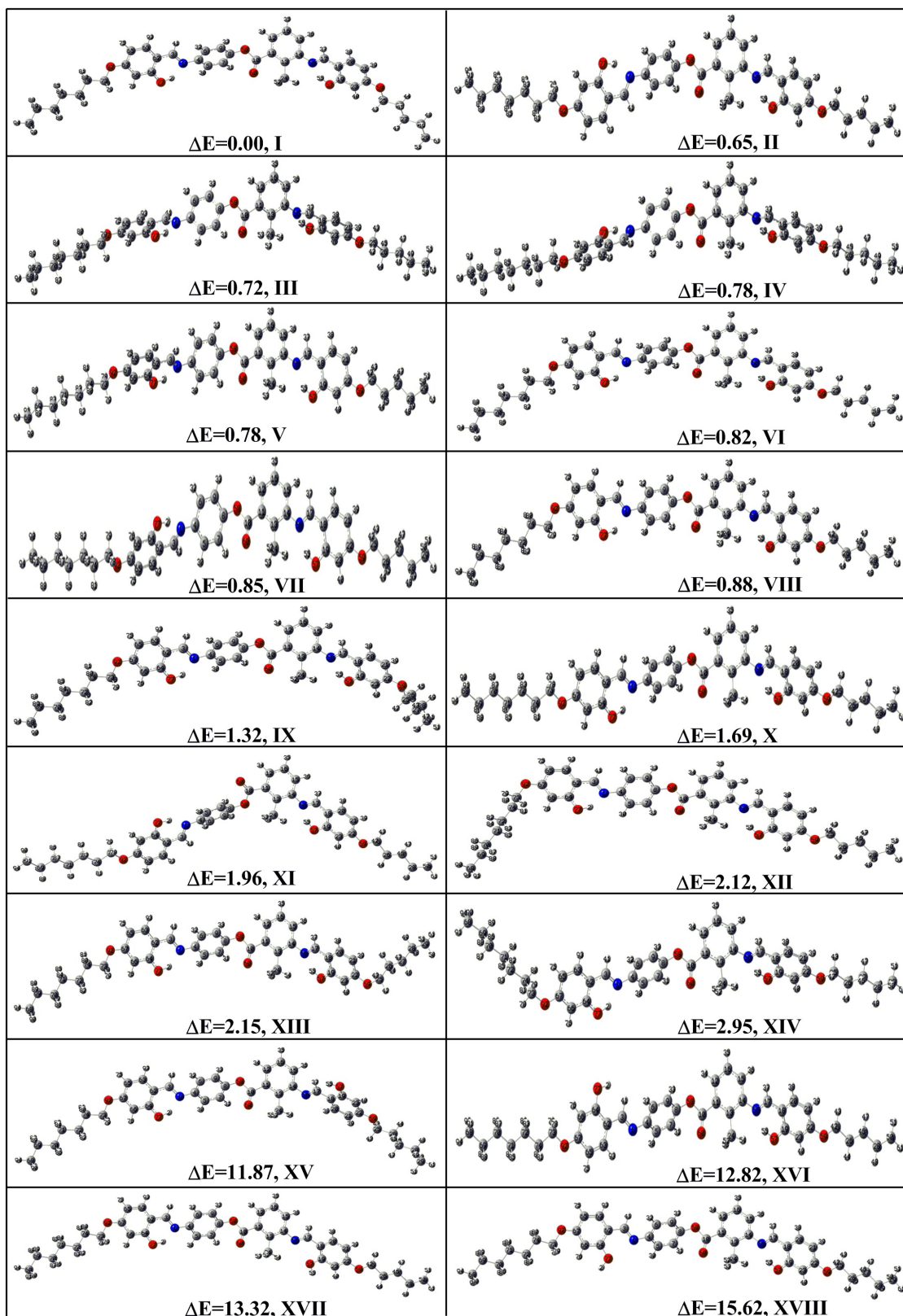


Fig. S1 All possible 18 conformers with their relative energy (kcal/mol)

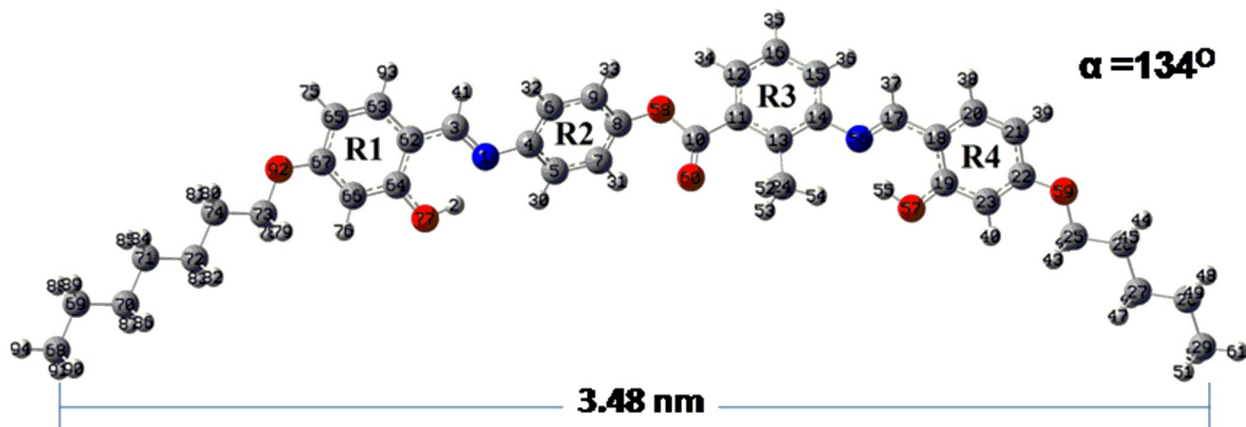


Fig. S2 Optimized structure of the most stable conformer I, with molecular length ~ 3.48 nm and bent angle $\sim 134^\circ$.

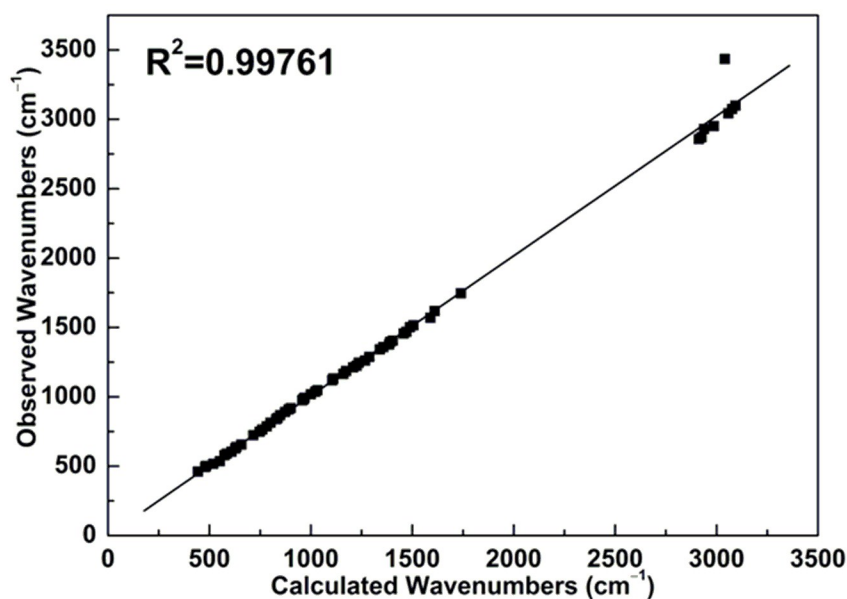


Fig. S3 The correlation graph between the calculated wavenumbers and observed wavenumbers of HAMPB.

Table S1 The optimized structural parameters: Bond length, bond angle and dihedral angle conformer I.

Parameters	Parameters	Parameters	Parameters	Parameters	Parameters		
Bond length	A(10,11,12)	118.7987	A(74,72,82)	109.4257	D(42,25,26,27)	-60.2293	
R(1,3)	1.2957	A(10,11,13)	120.3002	A(74,72,83)	109.5453	D(42,25,26,44)	61.9923
R(1,4)	1.4057	A(12,11,13)	120.8983	A(82,72,83)	106.0692	D(42,25,26,45)	177.5997
R(2,77)	1.0005	A(11,12,16)	120.5105	A(74,73,78)	110.8859	D(43,25,26,27)	59.849
R(3,41)	1.0983	A(11,12,34)	119.1731	A(74,73,79)	110.8648	D(43,25,26,44)	-177.929
R(3,62)	1.4427	A(16,12,34)	120.3116	A(74,73,92)	107.908	D(43,25,26,45)	-62.322
R(4,5)	1.4049	A(11,13,14)	117.5815	A(78,73,79)	107.8948	D(59,25,26,27)	179.7917
R(4,6)	1.4056	A(11,13,24)	122.9885	A(78,73,92)	109.6791	D(59,25,26,44)	-57.9867
R(5,7)	1.3907	A(14,13,24)	119.418	A(79,73,92)	109.603	D(59,25,26,45)	57.6207
R(5,30)	1.0857	A(13,14,15)	120.5962	A(72,74,73)	112.2265	D(26,25,59,22)	-179.497
R(6,9)	1.3924	A(13,14,56)	119.0718	A(72,74,80)	110.1163	D(42,25,59,22)	59.6868

R(6,32)	1.0859	A(15,14,56)	120.2719	A(72,74,81)	110.1869	D(43,25,59,22)	-58.6801
R(7,8)	1.396	A(14,15,16)	120.8329	A(73,74,80)	108.6813	D(25,26,27,28)	179.998
R(7,31)	1.0829	A(14,15,36)	118.9844	A(73,74,81)	108.7651	D(25,26,27,46)	58.027
R(8,9)	1.3933	A(16,15,36)	120.1498	A(80,74,81)	106.6931	D(25,26,27,47)	-58.0323
R(8,58)	1.3936	A(12,16,15)	119.5579	A(2,77,64)	107.1477	D(44,26,27,28)	58.5996
R(9,33)	1.0856	A(12,16,35)	120.2741	A(67,92,73)	119.0884	D(44,26,27,46)	-63.3713
R(10,11)	1.4922	A(15,16,35)	120.164	<u>Dihedral angle</u>		D(44,26,27,47)	-179.431
R(10,58)	1.3775	A(18,17,37)	116.5214	D(4,1,3,41)	3.8941	D(45,26,27,28)	-58.6779
R(10,60)	1.2105	A(18,17,56)	122.7559	D(4,1,3,62)	-176.91	D(45,26,27,46)	179.3511
R(11,12)	1.4063	A(37,17,56)	120.7169	D(3,1,4,5)	-148.241	D(45,26,27,47)	63.2918
R(11,13)	1.4163	A(17,18,19)	121.5674	D(3,1,4,6)	33.9494	D(26,27,28,29)	179.9027
R(12,16)	1.3883	A(17,18,20)	120.3587	D(1,3,62,63)	-179.34	D(26,27,28,48)	-57.8575
R(12,34)	1.0824	A(19,18,20)	118.0727	D(1,3,62,64)	0.736	D(26,27,28,49)	57.6718
R(13,14)	1.4176	A(18,19,23)	120.3339	D(41,3,62,63)	-0.1095	D(46,27,28,29)	-57.8624
R(13,24)	1.5108	A(18,19,57)	121.765	D(41,3,62,64)	179.9662	D(46,27,28,48)	64.3774
R(14,15)	1.4037	A(23,19,57)	117.901	D(1,4,5,7)	-179.83	D(46,27,28,49)	179.9066
R(14,56)	1.4094	A(18,20,21)	121.9182	D(1,4,5,30)	1.0835	D(47,27,28,29)	57.7156
R(15,16)	1.391	A(18,20,38)	118.5005	D(6,4,5,7)	-1.9112	D(47,27,28,48)	179.9554
R(15,36)	1.0863	A(21,20,38)	119.5814	D(6,4,5,30)	179.0022	D(47,27,28,49)	-64.5153
R(16,35)	1.0862	A(20,21,22)	119.2234	D(1,4,6,9)	179.0727	D(27,28,29,50)	60.0343
R(17,18)	1.4425	A(20,21,39)	122.0424	D(1,4,6,32)	1.3172	D(27,28,29,51)	-59.8096
R(17,37)	1.0988	A(22,21,39)	118.7341	D(5,4,6,9)	1.2788	D(27,28,29,61)	-179.888
R(17,56)	1.2951	A(21,22,23)	120.6009	D(5,4,6,32)	-176.477	D(48,28,29,50)	-62.0065
R(18,19)	1.4234	A(21,22,59)	115.18	D(4,5,7,8)	1.3395	D(48,28,29,51)	178.1496
R(18,20)	1.4127	A(23,22,59)	124.2192	D(4,5,7,31)	-179.588	D(48,28,29,61)	58.0712
R(19,23)	1.4016	A(19,23,22)	119.8508	D(30,5,7,8)	-179.589	D(49,28,29,50)	-177.952
R(19,57)	1.3413	A(19,23,40)	117.7039	D(30,5,7,31)	-0.516	D(49,28,29,51)	62.2037
R(20,21)	1.3781	A(22,23,40)	122.4453	D(4,6,9,8)	-0.1032	D(49,28,29,61)	-57.8747
R(20,38)	1.0878	A(13,24,52)	111.3208	D(4,6,9,33)	-179.409	D(3,62,63,65)	-179.631
R(21,22)	1.4131	A(13,24,53)	111.1658	D(32,6,9,8)	177.6646	D(3,62,63,93)	0.1917
R(21,39)	1.0843	A(13,24,54)	110.5128	D(32,6,9,33)	-1.6411	D(64,62,63,65)	0.296
R(22,23)	1.3954	A(52,24,53)	105.7955	D(5,7,8,9)	-0.1178	D(64,62,63,93)	-179.881
R(22,59)	1.3555	A(52,24,54)	108.8513	D(5,7,8,58)	-176.474	D(3,62,64,66)	179.6232
R(23,40)	1.0826	A(53,24,54)	109.0502	D(31,7,8,9)	-179.193	D(3,62,64,77)	-0.4383
R(24,52)	1.0939	A(26,25,42)	110.9949	D(31,7,8,58)	4.451	D(63,62,64,66)	-0.3029
R(24,53)	1.094	A(26,25,43)	111.0133	D(7,8,9,6)	-0.4931	D(63,62,64,77)	179.6357
R(24,54)	1.0901	A(26,25,59)	107.5711	D(7,8,9,33)	178.8254	D(62,63,65,67)	-0.0755
R(25,26)	1.5221	A(42,25,43)	107.9579	D(58,8,9,6)	176.0821	D(62,63,65,75)	179.8363
R(25,42)	1.0991	A(42,25,59)	109.6688	D(58,8,9,33)	-4.5995	D(93,63,65,67)	-179.896
R(25,43)	1.0991	A(43,25,59)	109.6302	D(7,8,58,10)	-52.2171	D(93,63,65,75)	0.0156
R(25,59)	1.4312	A(25,26,27)	112.6463	D(9,8,58,10)	131.2827	D(62,64,66,67)	0.0942
R(26,27)	1.5341	A(25,26,44)	108.6262	D(58,10,11,12)	-9.1651	D(62,64,66,76)	-179.956
R(26,44)	1.0976	A(25,26,45)	108.5745	D(58,10,11,13)	171.4328	D(77,64,66,67)	-179.847
R(26,45)	1.0976	A(27,26,44)	110.08	D(60,10,11,12)	170.994	D(77,64,66,76)	0.1029
R(27,28)	1.5343	A(27,26,45)	110.0689	D(60,10,11,13)	-8.4081	D(62,64,77,2)	-0.2258
R(27,46)	1.1001	A(44,26,45)	106.6481	D(11,10,58,8)	178.8477	D(66,64,77,2)	179.7142
R(27,47)	1.1	A(26,27,28)	112.9603	D(60,10,58,8)	-1.3041	D(63,65,67,66)	-0.1453
R(28,29)	1.5318	A(26,27,46)	109.6282	D(10,11,12,16)	-178.935	D(63,65,67,92)	179.872
R(28,48)	1.099	A(26,27,47)	109.5744	D(10,11,12,34)	0.2638	D(75,65,67,66)	179.94
R(28,49)	1.099	A(28,27,46)	109.1579	D(13,11,12,16)	0.4633	D(75,65,67,92)	-0.0427
R(29,50)	1.097	A(28,27,47)	109.1871	D(13,11,12,34)	179.6622	D(64,66,67,65)	0.1343
R(29,51)	1.0969	A(46,27,47)	106.1003	D(10,11,13,14)	-179.851	D(64,66,67,92)	-179.885
R(29,61)	1.0958	A(27,28,29)	113.1535	D(10,11,13,24)	-1.1234	D(76,66,67,65)	-179.813
R(55,57)	0.9993	A(27,28,48)	109.1679	D(12,11,13,14)	0.7592	D(76,66,67,92)	0.1683
R(62,63)	1.4126	A(27,28,49)	109.1422	D(12,11,13,24)	179.4872	D(65,67,92,73)	-179.169
R(62,64)	1.4237	A(29,28,48)	109.524	D(11,12,16,15)	-0.7536	D(66,67,92,73)	0.8487

R(63,65)	1.3785	A(29,28,49)	109.5316	D(11,12,16,35)	178.5149	D(90,68,69,70)	59.8946
R(63,93)	1.0879	A(48,28,49)	106.0755	D(34,12,16,15)	-179.943	D(90,68,69,88)	-178.012
R(64,66)	1.4019	A(28,29,50)	111.2316	D(34,12,16,35)	-0.6749	D(90,68,69,89)	-62.189
R(64,77)	1.3404	A(28,29,51)	111.2087	D(11,13,14,15)	-1.7053	D(91,68,69,70)	-59.8459
R(65,67)	1.4128	A(28,29,61)	111.3283	D(11,13,14,56)	-178.895	D(91,68,69,88)	62.2472
R(65,75)	1.0843	A(50,29,51)	107.5437	D(24,13,14,15)	179.5196	D(91,68,69,89)	178.0705
R(66,67)	1.3952	A(50,29,61)	107.6648	D(24,13,14,56)	2.3297	D(94,68,69,70)	-179.971
R(66,76)	1.0825	A(51,29,61)	107.6776	D(11,13,24,52)	-54.4497	D(94,68,69,88)	-57.8774
R(67,92)	1.3566	A(14,56,17)	120.7205	D(11,13,24,53)	63.2258	D(94,68,69,89)	57.9459
R(68,69)	1.5321	A(19,57,55)	107.1757	D(11,13,24,54)	-175.538	D(68,69,70,71)	-179.856
R(68,90)	1.097	A(8,58,10)	120.3318	D(14,13,24,52)	124.256	D(68,69,70,86)	-57.6274
R(68,91)	1.097	A(22,59,25)	119.3422	D(14,13,24,53)	-118.069	D(68,69,70,87)	57.8335
R(68,94)	1.0959	A(3,62,63)	120.4144	D(14,13,24,54)	3.1675	D(88,69,70,71)	57.9202
R(69,70)	1.5342	A(3,62,64)	121.5641	D(13,14,15,16)	1.4636	D(88,69,70,86)	-179.852
R(69,88)	1.0993	A(63,62,64)	118.0215	D(13,14,15,36)	-176.451	D(88,69,70,87)	-64.3908
R(69,89)	1.0993	A(62,63,65)	121.9797	D(56,14,15,16)	178.6197	D(89,69,70,71)	-57.6056
R(70,71)	1.5338	A(62,63,93)	118.4697	D(56,14,15,36)	0.7054	D(89,69,70,86)	64.6224
R(70,86)	1.1003	A(65,63,93)	119.5504	D(13,14,56,17)	-140.034	D(89,69,70,87)	-179.917
R(70,87)	1.1002	A(62,64,66)	120.3035	D(15,14,56,17)	42.767	D(69,70,71,72)	179.8946
R(71,72)	1.5344	A(62,64,77)	121.8173	D(14,15,16,12)	-0.2035	D(69,70,71,84)	57.7852
R(71,84)	1.0999	A(66,64,77)	117.8791	D(14,15,16,35)	-179.473	D(69,70,71,85)	-57.9275
R(71,85)	1.0999	A(63,65,67)	119.2052	D(36,15,16,12)	177.6866	D(86,70,71,72)	57.7064
R(72,74)	1.5342	A(63,65,75)	122.0298	D(36,15,16,35)	-1.5826	D(86,70,71,84)	-64.4029
R(72,82)	1.1	A(67,65,75)	118.765	D(37,17,18,19)	179.6268	D(86,70,71,85)	179.8844
R(72,83)	1.0999	A(64,66,67)	119.9191	D(37,17,18,20)	0.0391	D(87,70,71,72)	-57.8639
R(73,74)	1.5222	A(64,66,76)	117.6323	D(56,17,18,19)	0.502	D(87,70,71,84)	-179.973
R(73,78)	1.0992	A(67,66,76)	122.4486	D(56,17,18,20)	-179.086	D(87,70,71,85)	64.314
R(73,79)	1.0992	A(65,67,66)	120.5702	D(18,17,56,14)	-176.485	D(70,71,72,74)	-179.58
R(73,92)	1.4307	A(65,67,92)	115.2697	D(37,17,56,14)	4.426	D(70,71,72,82)	-57.4398
R(74,80)	1.0976	A(66,67,92)	124.1601	D(17,18,19,23)	-179.703	D(70,71,72,83)	58.1079
R(74,81)	1.0976	A(69,68,90)	111.1857	D(17,18,19,57)	0.1872	D(84,71,72,74)	-57.3998
<u>Bond angle</u>		A(69,68,91)	111.1789	D(20,18,19,23)	-0.1062	D(84,71,72,82)	64.7399
A(3,1,4)	121.3903	A(69,68,94)	111.429	D(20,18,19,57)	179.784	D(84,71,72,83)	-179.713
A(1,3,41)	120.997	A(90,68,91)	107.502	D(17,18,20,21)	179.7418	D(85,71,72,74)	58.1935
A(1,3,62)	122.5596	A(90,68,94)	107.6808	D(17,18,20,38)	-0.2495	D(85,71,72,82)	-179.667
A(41,3,62)	116.4388	A(91,68,94)	107.6763	D(19,18,20,21)	0.14	D(85,71,72,83)	-64.1191
A(1,4,5)	117.8654	A(68,69,70)	113.1892	D(19,18,20,38)	-179.851	D(71,72,74,73)	179.786
A(1,4,6)	123.481	A(68,69,88)	109.4605	D(18,19,23,22)	0.0737	D(71,72,74,80)	58.5769
A(5,4,6)	118.6184	A(68,69,89)	109.4959	D(18,19,23,40)	-179.98	D(71,72,74,81)	-58.8485
A(4,5,7)	121.2136	A(70,69,88)	109.2255	D(57,19,23,22)	-179.821	D(82,72,74,73)	57.7919
A(4,5,30)	118.5753	A(70,69,89)	109.1981	D(57,19,23,40)	0.1259	D(82,72,74,80)	-63.4173
A(7,5,30)	120.2048	A(88,69,89)	106.0202	D(18,19,57,55)	0.7166	D(82,72,74,81)	179.1573
A(4,6,9)	120.448	A(69,70,71)	113.5667	D(23,19,57,55)	-179.391	D(83,72,74,73)	-58.0985
A(4,6,32)	120.0311	A(69,70,86)	109.2031	D(18,20,21,22)	-0.1372	D(83,72,74,80)	-179.308
A(9,6,32)	119.4832	A(69,70,87)	109.2101	D(18,20,21,39)	179.9954	D(83,72,74,81)	63.267
A(5,7,8)	119.127	A(71,70,86)	109.2752	D(38,20,21,22)	179.8541	D(78,73,74,72)	60.4484
A(5,7,31)	120.5431	A(71,70,87)	109.3356	D(38,20,21,39)	-0.0133	D(78,73,74,80)	-177.522
A(8,7,31)	120.3234	A(86,70,87)	105.9707	D(20,21,22,23)	0.1001	D(78,73,74,81)	-61.729
A(7,8,9)	120.709	A(70,71,72)	113.3283	D(20,21,22,59)	-179.894	D(79,73,74,72)	-59.3801
A(7,8,58)	122.7122	A(70,71,84)	109.3518	D(39,21,22,23)	179.972	D(79,73,74,80)	62.6498
A(9,8,58)	116.4852	A(70,71,85)	109.3615	D(39,21,22,59)	-0.0224	D(79,73,74,81)	178.4425
A(6,9,8)	119.8601	A(72,71,84)	109.2255	D(21,22,23,19)	-0.0695	D(92,73,74,72)	-179.413
A(6,9,33)	120.9805	A(72,71,85)	109.2733	D(21,22,23,40)	179.9866	D(92,73,74,80)	-57.3832
A(8,9,33)	119.1558	A(84,71,85)	106.0419	D(59,22,23,19)	179.9243	D(92,73,74,81)	58.4096
A(11,10,58)	111.0144	A(71,72,74)	113.1945	D(59,22,23,40)	-0.0195	D(74,73,92,67)	179.176
A(11,10,60)	126.4819	A(71,72,82)	109.1653	D(21,22,59,25)	179.5372	D(78,73,92,67)	-59.9287

A(58,10,60)	122.5034	A(71,72,83)	109.1921	D(23,22,59,25)	-0.457	D(79,73,92,67)	58.3513
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Note: Bond length in angstrom, bond angle and dihedral angles are in degree.

Table S2 Observed and calculated vibrational wavenumbers (in cm^{-1}) of conformers I.

Wavenumber (unscaled)	Scaled	FTIR	CONTRIBUTIONS
3250.64	3125.16		R3[v(C12H)](97)
3246.30	3120.99		R4[v(C23H40)](92) R1[v(C66H)](7)
3246.29	3120.98		R1[v(C66H)](92) R4[v(C23H40)](7)
3245.51	3120.24		R2[v(CH)](99)
3228.18	3103.57		R4[v(C21H)](96)
3227.19	3102.62		R1[v(C65H)](96)
3217.73	3093.52	3098	R2[v(CH)](99)
3209.37	3085.49		R2[v(CH)](95)
3209.19	3085.32		R3[v(CH)](93) R2[v(C5H)](4)
3200.53	3076.99	3074	R2[v(CH)](98)
3193.23	3069.97		R3[v(CH)](99)
3183.01	3060.15		R4[v(CH)](98)
3181.08	3058.29	3042	R1[v(CH)](99)
3173.69	3051.18		$\nu_a[(\text{C}24\text{H}_3)](99)$
3163.24	3041.14	3435	$\nu(\text{O}57\text{H})(98)$
3140.20	3018.99		$\nu(\text{O}77\text{H})(98)$
3129.66	3008.85		$\nu_a[(\text{C}24\text{H}_3)](100)$
3114.10	2993.90		$\nu_a[(\text{C}29\text{H}_3)](100)$
3111.99	2991.87		$\nu_a[(\text{C}68\text{H}_3)](99)$
3108.36	2988.38		$\nu_a[(\text{C}29\text{H}_3)](96)$
3106.87	2986.95	2951	$\nu_a[(\text{C}68\text{H}_3)](98)$
3096.49	2976.97		$\nu_a[(\text{C}74\text{H}_2)](76)$ $\nu_a[(\text{C}73\text{H}_2)](10)$ $\nu_a[(\text{C}72\text{H}_2)](10)$
3095.32	2975.85		$\nu_a[(\text{C}26\text{H}_2)](75)$ $\nu_a[(\text{C}25\text{H}_2)](12)$ $\nu_a[(\text{C}27\text{H}_2)](8)$
3078.07	2959.26		$\nu_s[(\text{C}24\text{H}_3)](100)$
3072.64	2954.03		$\nu_a[(\text{C}71\text{H}_2)](32)$ $\nu_a[(\text{C}70\text{H}_2)](29)$ $\nu_a[(\text{C}69\text{H}_2)](18)$ $\nu_a[(\text{C}72\text{H}_2)](8)$
3065.35	2947.03		$\nu_a[(\text{C}28\text{H}_2)](61)$ $\nu_a[(\text{C}27\text{H}_2)](20)$ $\nu_a[(\text{C}25\text{H}_2)](8)$ $\nu_a[(\text{C}29\text{H}_2)](8)$
3058.16	2940.11		$\nu[(\text{C}3\text{H})](98)$
3057.22	2939.21		$\nu_a[(\text{C}73\text{H}_2)](33)$ $\nu_a[(\text{C}69\text{H}_2)](32)$ $\nu_a[(\text{C}72\text{H}_2)](16)$ $\nu_a[(\text{C}71\text{H}_2)](11)$
3056.90	2938.91	2930	$\nu_a[(\text{C}25\text{H}_2)](79)$ $\nu_a[(\text{C}26\text{H}_2)](17)$
3055.30	2937.36		$\nu_a[(\text{C}73\text{H}_2)](54)$ $\nu_a[(\text{C}74\text{H}_2)](17)$ $\nu_a[(\text{C}69\text{H}_2)](14)$ $\nu_a[(\text{C}72\text{H}_2)](8)$
3054.95	2937.03		$\nu[(\text{C}17\text{H})](98)$
3049.22	2931.52		$\nu_s[(\text{C}74\text{H}_2)](93)$
3048.78	2931.10		$\nu_s[(\text{C}26\text{H}_2)](92)$
3043.31	2925.84	2870	$\nu_s[(\text{C}29\text{H}_2)](97)$
3042.17	2924.74		$\nu_s[(\text{C}68\text{H}_3)](97)$
3041.67	2924.26		$\nu_a[(\text{C}27\text{H}_2)](69)$ $\nu_a[(\text{C}28\text{H}_2)](27)$
3041.39	2923.99		$\nu_a[(\text{C}72\text{H}_2)](48)$ $\nu_a[(\text{C}69\text{H}_2)](18)$ $\nu_a[(\text{C}70\text{H}_2)](17)$ $\nu_a[(\text{C}71\text{H}_2)](13)$
3034.76	2917.62		$\nu_a[(\text{C}70\text{H}_2)](48)$ $\nu_a[(\text{C}71\text{H}_2)](33)$ $\nu_a[(\text{C}69\text{H}_2)](9)$ $\nu_a[(\text{C}72\text{H}_2)](9)$
3030.07	2913.11	2857	$\nu_s[(\text{C}28\text{H}_2)](87)$ $\nu_a[(\text{C}27\text{H}_2)](6)$
3029.51	2912.57		$\nu_s[(\text{C}69\text{H}_2)](57)$ $\nu_s[(\text{C}71\text{H}_2)](20)$ $\nu_a[(\text{C}70\text{H}_2)](13)$
3022.44	2905.78		$\nu_s[(\text{C}72\text{H}_2)](40)$ $\nu_s[(\text{C}69\text{H}_2)](28)$ $\nu_s[(\text{C}73\text{H}_2)](14)$ $\nu_s[(\text{C}71\text{H}_2)](10)$
3020.93	2904.32		$\nu_s[(\text{C}25\text{H}_2)](67)$ $\nu_s[(\text{C}27\text{H}_2)](25)$
3018.21	2901.71		$\nu_s[(\text{C}73\text{H}_2)](58)$ $\nu_s[(\text{C}71\text{H}_2)](29)$ $\nu_s[(\text{C}69\text{H}_2)](9)$
3015.39	2899.00		$\nu_s[(\text{C}27\text{H}_2)](65)$ $\nu_s[(\text{C}25\text{H}_2)](30)$
3013.98	2897.64		$\nu_s[(\text{C}71\text{H}_2)](39)$ $\nu_s[(\text{C}72\text{H}_2)](26)$ $\nu_s[(\text{C}73\text{H}_2)](19)$ $\nu_s[(\text{C}70\text{H}_2)](14)$
3012.23	2895.96		$\nu_s[(\text{C}70\text{H}_2)](66)$ $\nu_s[(\text{C}72\text{H}_2)](23)$
1809.44	1739.60	1746	$\nu(\text{C}=\text{O})(77)$ $\rho(\text{C}10\text{O}58)(7)$ $\rho(\text{C}10\text{C})(6)$
1691.33	1626.04		R1[v(CC)(19)+ $\delta_{\text{in}}(\text{O}77\text{H})(8)$ + $\delta_a(5)$] R4[v(CC)(17)+ $\delta_{\text{in}}(\text{O}57\text{H})(6)$ + $\delta_a(4)$]
1691.04	1625.76		R4[v(CC)(20)+ $\delta_{\text{in}}(\text{O}57\text{H})(7)$ + $\delta_a(4)$] R1[v(CC)(17)+ $\delta_{\text{in}}(\text{O}77\text{H})(7)$ + $\delta_a(4)$] $\nu(\text{C}17\text{N})(4)$
1679.97	1615.12		$\nu(\text{C}3\text{N})(32)$ R2[v(CC)](19) $\rho(\text{C}3\text{H})(11)$ R1[v(C3C)(7)+ $\delta_{\text{in}}(\text{C}62\text{C}3)(4)$]
1674.97	1610.32	1618	$\nu(\text{C}17\text{N})(40)$ $\delta(\text{C}17\text{H})(13)$ R4[v(C17C)(9)+ $\delta_{\text{in}}(\text{C}18\text{C}17)(6)$ + $\nu(\text{C}18\text{C}20)(5)$]
1653.06	1589.25	1570	R2[v(CC)(37)+ $\delta_{\text{in}}(\text{CH})(7)$] $\nu(\text{C}3\text{N})(10)$ R1[v(CC)](8) $\rho(\text{C}3\text{H})(4)$ R2[$\delta^{\prime}_a(3)$]
1638.18	1574.95		R3[v(CC)(66)+ $\delta_{\text{in}}(\text{CH})(15)$ + $\delta^{\prime}_a(10)$]
1630.34	1567.41		R3[v(CC)(18)+ $\delta_a(4)$ + $\delta_{\text{in}}(\text{C}15\text{H})(3)$] R4[v(CC)(12)+ $\delta_{\text{in}}(\text{O}57\text{H})(7)$] R2[v(CC)](12)
1630.08	1567.16		R2[v(CC)(50)+ $\delta_{\text{in}}(\text{CH})(7)$ + $\delta^{\prime}_a(4)$ + $\delta_a(3)$] R3[v(C15C16)](4)
1622.80	1560.16		R1[v(CC)(33)+ $\delta_{\text{in}}(\text{O}77\text{H})(24)$ + $\delta^{\prime}_a(4)$ + $\delta_{\text{in}}(\text{C}64\text{O})(4)$ + $\delta_{\text{in}}(\text{C}67\text{O})(3)$] $\nu(\text{C}3\text{N})(10)$
1618.26	1555.80		R3[v(CC)(23)+ $\nu(\text{C}17\text{N})(8)$ + $\delta_a(4)$ + $\delta_{\text{in}}(\text{C}16\text{H})(4)$] R4[$\delta_{\text{in}}(\text{O}57\text{H})(14)$ + $\nu(\text{CC})(13)$]
1567.16	1506.67		R1[v(CC)(27)+ $\delta_{\text{in}}(\text{CH})(22)$ + $\nu(\text{C}67\text{O})(6)$ + $\delta_{\text{in}}(\text{O}77\text{H})(5)$] $\delta_{\text{sci}}(\text{C}73\text{H}_2)(14)$
1566.03	1505.58	1516	R4[v(CC)(27)+ $\delta_{\text{in}}(\text{CH})(25)$ + $\nu(\text{C}22\text{O})(6)$ + $\delta_{\text{in}}(\text{O}57\text{H})(6)$] $\delta_{\text{sci}}(\text{C}25\text{H}_2)(18)$
1549.89	1490.06		$\delta_{\text{sci}}(\text{C}73\text{H}_2)(29)$ R2[$\delta_{\text{in}}(\text{CH})(21)$ + $\nu(\text{CC})(14)$ + $\nu(\text{C}4\text{N})(3)$] $\delta_{\text{sci}}(\text{C}74\text{H}_2)(9)$ $\delta_{\text{sci}}(\text{C}72\text{H}_2)(6)$
1548.43	1488.66	1501	$\delta_{\text{sci}}(\text{C}25\text{H}_2)(37)$ $\delta_{\text{sci}}(\text{C}26\text{H}_2)(16)$ $\delta_{\text{sci}}(\text{C}27\text{H}_2)(12)$ $\delta_{\text{sci}}(\text{C}28\text{H}_2)(6)$ R4[v(C21C22)(4)+ $\delta_{\text{in}}(\text{C}21\text{H})(3)$]

104.64	100.60	$\delta_{\text{sci}}(\text{C71C})(7)$ R1[τ_a](6) $\delta_{\text{sci}}(\text{C70C})(6)$ $\delta_{\text{in}}(\text{O92C})(4)$ $\tau(\text{C100})(4)$ R2[τ'_a](4) $\tau(\text{C73C74})(4)$ $\delta_{\text{sci}}(\text{C72C})(3)$ $\tau(\text{C69C70})(3)$
100.22	96.35	$\tau(\text{C22O})(10)$ R3[τ'_a](9) $\tau(\text{C25O})(8)$ $\tau(\text{C27C28})(5)$ $\tau(\text{C24C})(5)$ R1[τ_a](5) R4[$\delta_{\text{oop}}(\text{C18C17})$](4) $\tau(\text{C26C27})(4)$
88.65	85.22	$\tau(\text{C22O})(9)$ R2[$\tau(\text{C8O})$](8) $\tau(\text{C26C27})(6)$ $\tau(\text{C25O})(5)$ $\delta_{\text{in}}(\text{N56C})(5)$ $\delta_{\text{in}}(\text{N1C})(4)$ $\tau(\text{C27C28})(4)$ $\delta_{\text{in}}(\text{O58C})(3)$ R1[$\tau(\text{C3C})$](3)
76.26	73.32	R2[$\tau(\text{C8O})$](14) $\delta_{\text{sci}}(\text{C72C})(7)$ $\delta_{\text{sci}}(\text{C71C})(6)$ $\delta(\text{C3H})(5)$ R1[$\delta_{\text{in}}(\text{C62C3})$](5) $\delta_{\text{sci}}(\text{C70C})(4)$
75.19	72.29	$\tau(\text{C26C27})(11)$ R4[$\tau_a(9)+\tau(\text{C19O})(8)+\tau(\text{C17C})(4)$] $\tau(\text{C22O})(5)$ R2[$\tau(\text{C8O})$](3) $\tau(\text{C73O})(3)$
63.00	60.57	$\tau(\text{C73O})(13)$ $\tau(\text{C67O})(12)$ R2[$\tau(\text{C8O})$](9) $\tau(\text{C3N})(6)$ $\tau(\text{C10C})(5)$ $\tau(\text{C71C72})(4)$ R1[$\delta_{\text{oop}}(\text{C62C3})$](4) $\tau(\text{C70C71})(4)$ $\tau(\text{C26C27})(3)$
58.84	56.57	$\delta_{\text{sci}}(\text{C26H}_2)(6)$ R2[$\tau(\text{C8O})$](6) $\tau(\text{C25C26})(6)$ $\delta_{\text{sci}}(\text{C25C})(5)$ $\tau(\text{C67O})(5)$ $\tau(\text{C10C})(4)$ $\delta_{\text{in}}(\text{N56C})(4)$ $\tau(\text{C73O})(4)$ $\tau(\text{C27C28})(4)$ $\delta(\text{O59C})(4)$
54.02	51.93	R1[$\tau(\text{C3C})$](3) $\tau(\text{N1C4})(3)$
51.22	49.24	$\tau(\text{C25C26})(16)$ $\tau(\text{C26C27})(13)$ $\tau(\text{C25O})(10)$ $\tau(\text{C27C28})(9)$ $\tau(\text{C24C})(5)$ $\tau(\text{C10C})(5)$ R2[$\tau(\text{C8O})$](4)
44.92	43.18	$\tau(\text{C73C74})(15)$ $\tau(\text{N1C4})(14)$ $\tau(\text{C72C74})(14)$ $\tau(\text{C71C72})(11)$ $\tau(\text{C67O})(8)$ $\tau(\text{C70C71})(6)$ R2[$\tau(\text{C8O})$](5) $\tau(\text{C69C70})(4)$
44.34	42.63	$\tau(\text{N1C4})(18)$ R2[$\tau(\text{C8O})$](15) $\delta_{\text{in}}(\text{O58C})(6)$ $\tau(\text{C17N})(5)$ $\tau(\text{C25O})(5)$ R4[$\tau(\text{C17C})(5)+\delta_{\text{oop}}(\text{C18C17})(5)$] R1[$\tau(\text{C3C})$](4) R2[$\delta_{\text{in}}(\text{C8O})$](4)
39.60	38.07	$\tau(\text{C10C})(3)$
36.39	34.99	R2[$\tau(\text{C8O})$](29) $\tau(\text{C10C})(12)$ $\delta_{\text{in}}(\text{O58C})(4)$ $\delta_{\text{in}}(\text{N1C})(4)$ $\tau(\text{N1C4})(4)$ R4[$\tau(\text{C17C})$](3)
28.32	27.23	$\tau(\text{C100})(13)$ $\tau(\text{N1C4})(9)$ $\tau(\text{C72C74})(6)$ R1[$\delta_{\text{oop}}(\text{C62C3})(5)+\tau_a(4)$] $\tau(\text{C14N})(4)$ $\tau(\text{C17N})(4)$ $\tau(\text{C70C71})(4)$ R4[$\delta_{\text{oop}}(\text{C18C17})$](3)
26.67	25.64	$\tau(\text{C3N})(3)$
21.01	20.20	R2[$\tau(\text{C8O})$](22) $\tau(\text{C10C})(15)$ $\tau(\text{C24C})(8)$ $\tau(\text{N1C4})(7)$ R1[$\tau(\text{C3C})$](3) $\delta_{\text{sci}}(\text{C74C})(3)$
17.10	16.44	$\tau(\text{C14N})(14)$ $\tau(\text{C25O})(7)$ $\tau(\text{C3N})(7)$ $\tau(\text{C22O})(6)$ $\tau(\text{C17N})(6)$ R1[$\delta_{\text{oop}}(\text{C62C3})$](5) $\tau(\text{C72C74})(5)$ $\tau(\text{C73O})(4)$ $\delta_{\text{in}}(\text{O58C})(3)$
14.80	14.23	R4[$\delta_{\text{oop}}(\text{C18C17})$](3)
10.71	10.30	R2[$\tau(\text{C8O})$](26) $\tau(\text{C10C})(24)$ $\tau(\text{C24C})(11)$ R2[$\delta_{\text{in}}(\text{C8O})$](5) $\delta_{\text{in}}(\text{O58C})(4)$ $\tau(\text{C14N})(3)$
7.07	6.80	R2[$\tau(\text{C8O})$](30) $\delta_{\text{in}}(\text{O58C})(7)$ $\tau(\text{C25O})(4)$ $\delta_{\text{sci}}(\text{C74C})(4)$ $\delta_{\text{sci}}(\text{C73C})(4)$ $\delta_{\text{in}}(\text{N56C})(4)$ $\tau(\text{C22O})(4)$ $\delta_{\text{in}}(\text{O92C})(3)$
6.50	6.25	$\tau(\text{C10C})(34)$ $\tau(\text{C24C})(16)$ $\tau(\text{C100})(6)$ $\tau(\text{C67O})(5)$ $\tau(\text{C73O})(4)$ $\tau(\text{C22O})(3)$ $\tau(\text{C14N})(3)$
		$\tau(\text{C10C})(13)$ R2[$\tau(\text{C8O})$](10) $\tau(\text{C73O})(9)$ $\tau(\text{C25O})(7)$ $\tau(\text{C22O})(7)$ $\tau(\text{C24C})(6)$ $\tau(\text{C67O})(6)$ $\tau(\text{C14N})(3)$
		$\tau(\text{C10C})(26)$ $\tau(\text{C100})(12)$ $\tau(\text{C73O})(9)$ $\tau(\text{C72C74})(7)$ $\tau(\text{C14N})(6)$ $\tau(\text{C17N})(3)$ $\tau(\text{C73C74})(3)$
		$\tau(\text{C10C})(25)$ R2[$\tau(\text{C8O})$](18) $\delta_{\text{in}}(\text{O58C})(12)$ R2[$\delta_{\text{in}}(\text{C8O})$](9)
		$\tau(\text{C10C})(21)$ $\tau(\text{C73O})(13)$ $\tau(\text{C24C})(12)$ $\tau(\text{C67O})(5)$ $\tau(\text{C25O})(5)$ $\tau(\text{C100})(5)$ $\tau(\text{C3N})(4)$ $\tau(\text{C14N})(3)$ R1[$\delta_{\text{oop}}(\text{C62C3})$](3)

Proposed assignment and potential energy distribution (PED) for vibrational normal modes.

Types of vibrations: v, stretching; δ , deformation(bending); oop, out-of-plane bending; ρ , rocking; τ , torsion; Y, twisting; ω , wagging.

^a Potential energy distribution (contribution ≥ 3)