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## **Supporting Information**

Novel fluorophore-spacer-receptor to conjugate MWNT and ferrite nanoparticles to design ultra-thin shield to screen electromagnetic radiation

Sourav Biswasab, Sujit Sankar Panjab, Suryasarathi Boseb

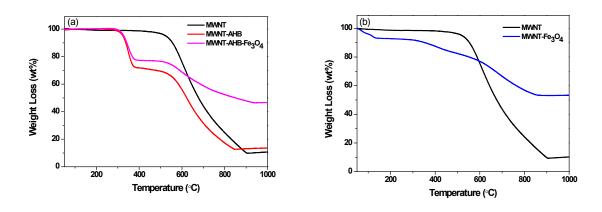


Figure S1: TGA plot of various conjugated nanoparticles in air (a) non-covalent conjugation (b) covalent conjugation.

Here, we have tried to fix the MWNTs concentration as 2 wt% in all the blends. When we prepared MWNT-Fe<sub>3</sub>O<sub>4</sub> by covalent conjugation, we have fixed 50/50 weight ratio. At the end of the conjugation we obtained 44% Fe<sub>3</sub>O<sub>4</sub> and 46% MWNT as seen from the TGA curves (Figure S1). So during mixing the total amount of filler was fixed at 4 wt% with respect to the total blend, consisting of 2 wt% MWNT and 2 wt% Fe<sub>3</sub>O<sub>4</sub>. In case of MWNT-AHB- Fe<sub>3</sub>O<sub>4</sub> the final yield was 38% Fe<sub>3</sub>O<sub>4</sub>, 40% MWNT and 22% AHB as obtained from TGA analysis.

High resolution TEM images of various conjugated nanoparticles

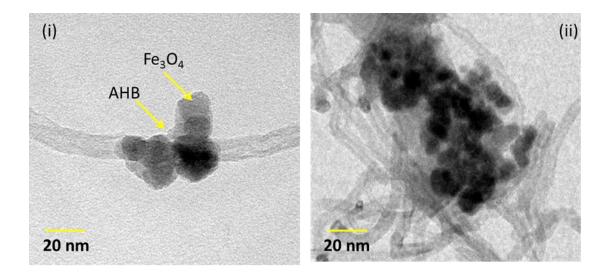
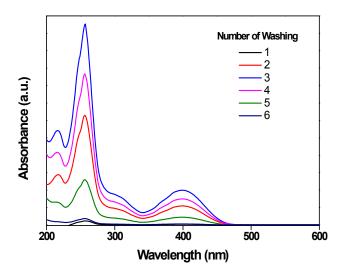


Figure S2: TEM images (i)MWNT-AHB-Fe<sub>3</sub>O<sub>4</sub> (ii) MWNT-Fe<sub>3</sub>O<sub>4</sub>

Monitoring the non-covalent attachment of AHB onto MWNT by UV-vis spectroscopy

The synthesized AHB has extended  $\pi$ -electron cloud associated with the anthracene moiety which can be used to conjugate with the  $\pi$ -electron cloud of MWNTs. The attachment of AHB was further confirmed by UV-vis and fluorescence emission spectroscopy. In general the MWNTs do not show any absorption under UV or fluorescence emission spectroscopy but after non-covalent attachment of AHB, the absorption due to AHB is clearly evident. In general in UV-Vis spectrum, a peak at 255 nm correspond to the  $\pi$ - $\pi$ \* transition and a peak at 398 nm correspond to n- $\pi$ \* transition. The unbound AHB molecules were thoroughly washed and the hybrid nanoparticles were monitored using UV-vis spectroscopy (figure S3). The absorption in the hybrid nanomaterials is from the AHB molecules that are non-covalently attached onto the surface of MWNTs as the unbound AHB has been thoroughly washed.



**Figure S3:** UV-Vis spectra of successive washing steps to remove unbound AHB from non-covalently modified MWNTs

Selective localization of hybrid nanoparticles: assessing by DSC

In general, crystallization and melting temperatures are greatly affected by the presence of various rigid nanoparticles and their distribution inside the matrix. So the preferential localization of various nanoparticles in the PVDF phase was further assessed by DSC experiments; changes in the crystallization and melting temperatures of PVDF (table S1 in the supporting information) clearly indicate the presence of hetero nucleating effect of these nanoparticles in the PVDF phase (figure S4).

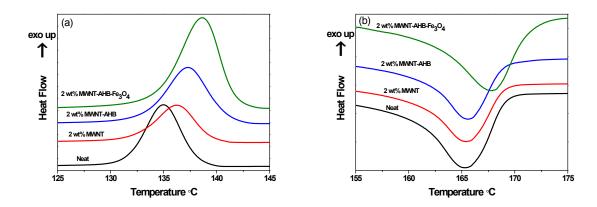
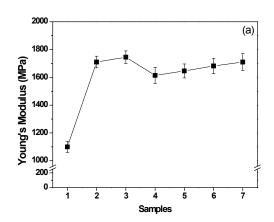
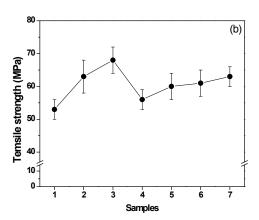


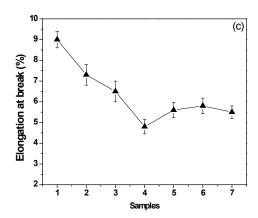
Figure S4: (a) DSC crystallization curve of various blends (b) DSC melting curve of various blends

Mechanical properties: effect of efficient dispersion of nanofillers inside the matrix

Interfacial adhesion between the constituents and the phase morphology are the deciding factors on the overall mechanical properties in case of multicomponent system<sup>1-3</sup>. Thermodynamic and chemical incompatibility between the immiscible polymers often results in poor mechanical properties due to poor stress transfer at the interfacial region. Neat 50/50 PC/PVDF blend exhibit much lower mechanical properties than the constituents, which indicates the incompatibility of the system. After the addition of MWNTs, improvement in tensile properties and Young's modulus was observed whereas; elongation at break is sacrificed due to premature failure at the interface originating from the agglomerating MWNTs [figure S5 (a-c)]. Generally, formation of hierarchical microstructure is the important parameters for deciding the mechanical properties of the polymer blend nanocomposites. The mechanical behaviour of blend nanocomposites is contingent on microstructural parameters such as interfacial interaction, localization and state of dispersion of fillers, percolation threshold and the state of dispersion in the matrix. After incorporation of AHB modified MWNTs, improvement in tensile properties and Young's modulus was more prominent due to the better dispersion of nanofillers in the PVDF matrix. However, mechanical properties deteriorate after addition of Fe<sub>3</sub>O<sub>4</sub> nanoparticles into the system. Though, conjugation of Fe<sub>3</sub>O<sub>4</sub> nanoparticles with MWNTs via non-covalent modification approach showed slight improvement in the properties. Further increase in the concentration of nanoparticles slightly deteriorates the overall properties.







**Figure S5:** Mechanical properties of various blends (a) Young's modulus (b) Ultimate tensile strength and (c) % elongation at break, where (1) neat 50/50 blend, (2) 2 wt% MWNT, (3) 2 wt% MWNT-AHB, (4) 2 wt% MWNT +  $Fe_3O_4$ , (5) 2 wt% MWNT-Fe<sub>3</sub>O<sub>4</sub>, (6) 2 wt% MWNT-AHB-Fe<sub>3</sub>O<sub>4</sub> and (7) 3 wt% MWNT-AHB-Fe<sub>3</sub>O<sub>4</sub> along X-axis.

## *Melt rheology: effect of different filler particles*

Flow characteristics of the blend were studied by melt rheology, which is an important tool to determine the processability of the nanocomposites. Due to the inter-dependence of viscoelastic properties between the two immiscible polymers, the characteristics flow behavior is complex in nature<sup>4-5</sup>. Figure S6 (a-b) shows the viscoelastic properties of different PC/PVDF blends at 260°C. It is observed that complex viscosity of PVDF is much higher than PC, whereas the 50/50 blends showed complex viscosity in between the two extremes<sup>6</sup>. The complex viscosity of MWNTs filled blends is much higher than the neat blend, particularly at lower frequency, where sufficient time is available for the relaxation of polymer chains. This indicated that the rigid network of MWNTs impedes macromolecular motion in a given flow field. In presence of AHB modified MWNTs, viscosity even raises higher, suggesting more exfoliation of MWNTs network resulting in mesh-like structure that restricts the macromolecular motion. So, the state of dispersion can also be comprehended by viscoelastic properties of the blend. Furthermore, addition of Fe<sub>3</sub>O<sub>4</sub> nanoparticles influences the blend complex viscosity by restricting the macromolecular motion to a greater extent. But interestingly, enhancement in complex viscosity is observed greatly only when Fe<sub>3</sub>O<sub>4</sub> nanoparticles were attached onto MWNTs surface via chemical conjugation. Now in the case of non-covalent attachment, further enhancement in complex viscosity is achieved suggesting

that the exfoliated network of MWNT is retained with lesser/fewer agglomeration. Further increasing concentration of nanoparticles resulted increasing complex viscosity.

Furthermore, to assess the mechanical response of the blends, dynamic storage modulus was studied and plotted in respect to angular frequency (figure S6 b). Generally the storage modulus increases with the addition of nanoparticles. Generally exfoliated nanoparticles restrict the macromolecular motion resulting in pseudo-solid nature leading to enhanced storage modulus. Further improvement is observed after incorporation of higher amount of filler in the blend.

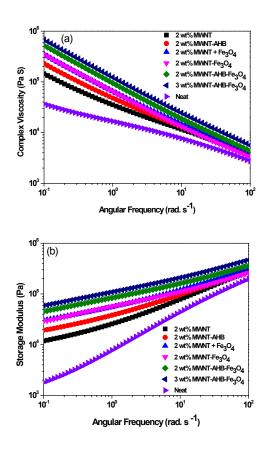


Figure S6: Melt rheology (a) complex viscosity and (b) storage modulus of various blends

**Table S1:** DSC crystallization and melting temperature of various blends

Compositions	Crystallization	Melting	
	Temperature (T <sub>c</sub> )	Temperature (T <sub>m</sub> )	
	(°C)	(°C)	

50/50 PC/PVDF	135	165
PC/PVDF with 2 wt% MWNT	136	166
50/50 PC/PVDF with 2 wt% MWNT-AHB	137	166
50/50 PC/PVDF with 2 wt% MWNT + Fe <sub>3</sub> O <sub>4</sub>	139	168

**Table S2:** Comparison of shielding efficiency with consisting literatures

Sr.	Matrix	Nanoparticles	Thicknes	$SE_T$	RL	Frequency	Referenc
No			s (mm)	(dB)	(dB)	(GHz)	e
1	PVP	MWNT/Fe <sub>3</sub> O <sub>4</sub> (40 wt%)	-	-	-35.8	8.56	7
2	Polyaniline	Polyaniline coated MWNT/γ Fe <sub>2</sub> O <sub>3</sub>	2	-34.1	-	2.5	8
3	PMMA	MWNT and Fe (catalyst)	-	-27	-	2-12	9
4	Epoxy	MWNT (5wt%) /Fe <sub>3</sub> O <sub>4</sub> (15wt%)	-	-40	-	13-40	10
5	Epoxy	MWNT/ Fe <sub>3</sub> O <sub>4</sub> (10 wt%)	1	-	-31.7	13.2	11
6	Epoxy	MWNT/ Fe <sub>3</sub> O <sub>4</sub> (60 wt%)	5.5	-	-37	2.68	12
7	Epoxy	MWNT/ α Fe (20 wt%)	1.2	-	-25	2-18	13
8	Epoxy	MWNT/ Fe <sub>3</sub> O <sub>4</sub>	3.4	-	-41.6	5.5	14
9	PVDF/ABS	IL-MWNT (1 wt%) / Fe <sub>3</sub> O <sub>4</sub> (2 vol%)	5	-22	-	8-18	15
10	PC/SAN	MWNT-grafted- Fe <sub>3</sub> O <sub>4</sub> (3 wt%)	5	-32.5	-	8-18	16
11	PC/PVDF	MWNT-AHB- Fe <sub>3</sub> O <sub>4</sub> (3 wt%)	5	-45	-	8-18	This work
12	PC/PVDF (LBL)	MWNT (3 wt%)+ MWNT-AHB- Fe <sub>3</sub> O <sub>4</sub> (3 wt%)	0.9	-60	-	12-18	This work

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