Supporting Information for

Corrosion behavior of 316L and 304 stainless steels exposed to Industrial-Marine-Urban environment: Field Study

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Index

1.	Experimental Methods			
1.1	Measurement of Atmospheric Corrosion Parameters			
1.1.1	Preparation of Wet Candle for Chloride Determination			
1.1.2	Preparation of Sulphation Plate for the Determination of SO ₂ 4			
1.1.3	Gravimetric Weight-Loss Analysis and Determination of Corrosion Rate5			
1.2	Surface Characterization of Exposed Steels			
1.2.1	Raman Spectroscopic Studies			
1.2.2	Scanning Electron Microscopy (SEM) with Energy Dispersive			
	X-ray (EDAX) Analysis6			
1.2.3	Vicker's Micro-Hardness Measurement6			
1.2.4	X-ray Fluorescence Analysis			
2.	Additional Figures			
	Figure S17			
	Figure S27			
	Figure S38			
	Figure S410			
	Figure S5 11			
	Figure S611			
	Figure S712			
	Figure S812			
	Figure S9 13			
	Figure S1013			
	Figure S1114			
	Figure S1214			
	Figure S1315			
	Figure S1416			
	Table S117			
3.	Supporting Information References18			

1. Measurement of Atmospheric Corrosion Parameters

1.1 Preparation of Wet Candle for Chloride Determination

The procedure mentioned in ASTM G 140-02⁻¹ (2002) was adopted for preparation and assembly of wet candle apparatus using Erlen Meyer flask, glass test tube, solid rubber, cotton bandage gauze (Fig. 3). Type IV reagent water was prepared as follows: 200 ml glycerin and 20 drops of octanoic acid were added in 1L of water. The octanoic acid was added to prevent freezing during the winter season. The apparatus was exposed for 30 days and the chloride content was estimated against AgNO₃ by titration.

The following equation was used to calculate the chloride content

where T is titre, mgCl⁻/ml of AgNO₃, *B*- Indicator blank.

The determined chloride content in the atmosphere is reported as mg Cl-/ $m^2/day.$

1.1.2 Preparation of Sulphation Plate for the Determination of SO₂

Wattmann Filter papers (grade 30) were cut and placed at the bottom of polystyrene culture dishes. Paper is bonded to the plate by adding acetone until the filter paper becomes saturated. Acetone is allowed to evaporate. Polystyrene plates were rinsed with distilled water. 900 ml of distilled H₂O, 3.5 g of gum tragacanth was added and blended for 2 h. From this solution, 350 ml was taken and then about 3.5 g pulp of filter paper was added to that mixer solution. Further about 112 g of lead peroxide (PbO₂) was added to the same solution and blend for 2 min. 10 ml of the mixture was pipetted out carefully into the plate and ensured for the uniform spreading through the water layer in plate. 40 the The plates were placed in oven and heated at to

50 °C for 20 h. The plates were removed from oven and allowed to cool. They were sealed with tight fitting covers to preserve until the exposure begins. The sulphation plates were exposed for 30 day intervals time. The plates were recovered and analyzed for the SO₂ content. Barium sulphate (BaSO₄) precipitation by gravimetric analysis was used and the sulfate analysis provided the quantity of sulfate present on each disc (**Fig.** S3). Using the following equation SO₂ capture rate was determined and further from it, SO₂ content in the exposed environment are reported. The above described sulphation plate were prepared by following the ASTM G 91-97² (1997) procedure.

$$\mathbf{R} = (\mathbf{m} - \mathbf{m}_0) \times \mathbf{MWSO}_2 / \mathbf{MWSO}_4 \times \mathbf{A} \times \mathbf{T}$$
(1.2)

where m is the mass of sulphate found in the plate, in mg, m_0 is the mass of sulfate found in blank (unexposed) plate, in mg, $MWSO_2 = 64$, $MWSO_4 = 96$, A =Area of the plate, m² T = exposure time of the plate, days, R= SO₂ capture rate, mg SO₂/m²/day

1.1.3 Gravimetric Weight-Loss Analysis and Determination of Corrosion Rate

The exposed samples were removed from the stand and the initial weights were measured. The corrosion products of SS were removed by immersion in etching solution as specified in ASTM G1-99³ (1999). The etching solution was prepared as follows: 100 ml of HNO₃ was added to 1000 ml of distilled water. The exposed SS specimens were immersed for 20 minutes at 60 °C to remove the corrosion products. The final weight was measured after removing the corrosion products. From the initial and final weights, the corrosion rate in mpy was calculated using the following formula,

Corrosion rate in mpy =
$$k \times w/DAT$$
 (1.3)

where, $k = \text{constant} (3.45 \times 10^6)$, w = mass loss, mg, D = Density of SS, g/cm^3 , A = area, cm^2 , T = Time of exposure in hours.

1.2 Surface Characterization of Exposed Steels1.2.1 Raman Spectroscopic Studies

Raman spectra of rust layers were obtained from the corrosion products of the atmospheric exposed steels using the Almega dispersive instrument with the He-Ne 532 nm wavelength on the rust layers. The compounds in rust layers exist as mixture of iron oxides and oxyhydroxides as intimate mixtures with their own strong structural relationships. Hence, the conversion of one phase to another phase is very feasible either by electrochemical redox reactions, heating in under laser radiation. These treatments can cause the de-hydroxylation or oxidation of the corrosion products (α , β , γ -FeOOH and Fe₂O₃, Fe₃O₄), in particular magnetite is highly sensitive to laser irradiation which is disadvantageous for obtaining good Raman signal. To overcome this we used a set of six density filters to modulate the laser power on the sample from 5.2 mW to 5 μ W. With this precaution, all identified phases presented stable Raman spectra checked at a power of 0.65 μ W. ⁴⁻⁶ The Nikon microscope was used to monitor the analyzing spot at the

magnification of 50 μ m. The sampling stage equipped with the motorized platform joy stick to move to the desired location of the spot.

1.2.2 Scanning Electron Microscopy (SEM) with Energy Dispersive X-ray (EDAX) Analysis

The microstructure and elemental distributions in the rust layers were analyzed using a Quanta 200 FEG SEM equipped with energy dispersive X-ray analysis (SEM-EDAX) facilities. The microstructure and elemental distributions in the rust were analyzed before grinding using Quanta 200 FEG scanning electron microscope (SEM). The 2D line profiles of SEM images were obtained using the scanning probe image processor WSxM 5.0 develop 7.0 software.

1.2.3 Vicker's Micro-Hardness Measurement

The Vicker's micro-hardness of bare and exposed stainless steels were measured using micro-hardness testing system (Fischer scope H100C). The hardness profile of the surface was measured with constant load at 200 mN (10 points / specimen). The loading and unloading time was taken as 10 seconds to investigate the mechanical behaviour of the stainless steels after exposing to the IMU environment during field study.

1.2.4 X-ray Fluorescence Analysis

The elemental chemical composition of the stainless steels and the corrosive agents viz., Cl and S were analyzed semi quantitatively using Shimadzu XRF-1800 fluorescence analyzer.

2. Additional Figures



Fig. S1 Photographs of various steels in the exposure rack at the exposure site Chennai

bul Srinagara
Islamabad
Islamabad
Amritsar 2 TIDET
Indus Dalbi Mt. Everest Brahmapur
kistan Nepal LAYAS
New Delhi Kannar
Lind Agra Garries II
ANCER CHOLA HARDEN PATRA
Anmadabad Bhopal Kolkata Dhako Thim
Surat Nagpur Myan
Mumbai Coddyari Maria Maria Manualash
Bombay) Thyderabad Cart Ganary Rang
Goa Sakrishna Kuisa Datnam Bengal
abian 400 mi
Sea Bangalor Chennai 400 km
ccadive ((Madras) Andaman)
ulf of Cochine Indian Indian
Lanka Ocean Nicobar

Fig. S2 Topography of the location of atmospheric corrosion exposure site of Chennai

Exposure Site



Fig. S3 Photographs of the sulphation plate and wet candle for measuring the Chloride and SO₂ present in the atmospheric environment







Fig. S4 Average monthly values of (a) Temperature, (b) relative humidity (RH),(c) rain fall, (d) Wind speed in industrial-marine-urban environment



Fig. S5 Macroscopic images of surface appearance of the 316L and 304 SS specimens exposed for 3 years at industrial-marine-urban environment



Fig. S6 AFM images of 316L SS after atmospheric exposure in IMU environment for different durations Chennai



Fig. S7 AFM images of 304 SS after atmospheric exposure in IMU environment as a function of exposure durations Chennai



Fig. S8 2D line analysis SEM images of 316L SS after atmospheric exposure in IMU environment for different durations Chennai



Fig. S9 2D line analyses of SEM images of 304 SS after atmospheric exposure in IMU environment for different durations Chennai



Fig. S10 Hardness of atmospheric corroded 316L and 304 SS for different durations



Fig. S11 EDAX spectra of 316L and 304 SS after 3 years of IMU atmospheric corrosion exposure



Fig. S12 Equivalent circuits for fitting the EIS data, (a) for bare SS, (b) for atmospheric corrosion exposed in IMU environment



Fig. S13 Polarization resistance (EIS) behaviour of atmospheric corrosion exposed samples for 3 years in IMU environment Chennai



Fig. S14 Comparison of polarization resistance of 316L and 304 SS atmospheric corrosion exposed in IMU environment for 3 years Chennai

Period of exposure (Months)	Raman signatures 316L SS (cm ⁻¹)	Raman signatures 304 SS (cm ⁻¹)
3 April-June 2012 (Summer season)	250 Lepidocrocite300 Goethite400 Goethite610 Iron oxide	220 Iron oxide300 Goethite400 Goethite500 Iron oxide610 Iron oxide
6 July-Sept (Rainy season) 2012	220 Iron oxide300 Goethite400 Goethite500 Iron oxide600 Iron oxide	180 Maghemite240 Lepidocrocite300 Goethite400 Goethite500 Iron oxide
9 Oct-Dec (winter season) 2012	200 Iron oxide 290 Iron oxide 390 Goethite 590 Iron oxide	220 Iron oxide300 Goethite400 Goethite500 Iron oxide600 Iron oxide
12 Jan-March 2013	220 Iron oxide280 Iron oxide390 Goethite500 Iron oxide600 Iron oxide	190 Iron oxide220 Iron oxide300 Goethite400 Goethite490 Iron oxide600 Iron oxide
24 April – March 2013-14	270 Maghemite300 Goethite390 Goethite500 Iron oxide600 Hematite780 Iron oxide	220 Iron oxide300 Goethite400 Goethite490 Iron oxide600 Iron oxide
36 April- March 2014-15	210 Iron oxide300 Goethite400 Goethite500 Iron oxide600 Iron oxide	670 Akaganeite220 Iron oxide300 Goethite400 Goethite500 Iron oxide600 Iron oxide

Table S1Summary of characteristic signature of Raman spectrafrom the
atmospheric exposed stainless steels

3. Supporting Information References

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- 2. ASTM G 91-97 1997, Standard practice for monitoring atmospheric SO₂ using the sulfation plate technique', vol. 11.01, pp. 1-5.
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