

continence Supporting information for:

Performance, combustion and emission characteristics of a direct injection VCR CI engine using *Jatropha curcas* oil microemulsion: A comparative assessment with JCO B100, JCO B20 and Petrodiesel

Himansh Kumar, Lakhya Jyoti Konwar, Mohammad Aslam, Anil Kumar Sarma*

Sardar Swaran Singh National Institute of Bio-Energy

(An autonomous institute of Ministry of New and Renewable Energy, Govt. of India),

Kapurthala-144601 (Punjab), India

1. Experimental

1.1. Biodiesel preparation

JCO B100 was obtained by transesterification of pretreated/esterified JCO with methanol in the presence of 1 wt% NaOH (99.9%, Merck) as catalyst. NaOH was weighed separately of the total amount of oil (1200 g) using standard weighing balance and dissolved in required quantity of anhydrous methanol (mole ratio of oil to methanol was ~1:9) at 50 °C. The reaction mixture was vigorously stirred (500 rpm) and heated to at 60 °C for 30 min in 2 L capacity Jacketed Lab Reactor (Radleys) equipped with mechanical stirring and reflux condenser. After completion of the reaction, excess methanol was removed with a rotary evaporator (Heidolph Hei-VAP). The resulting product was neutralized with by washing with warm deionised water. Finally the product JCOB100 was recovered in a separatory funnel, dried in an oven (105 °C) and anhydrous Na₂SO₄ prior to use. 200 ml of the biodiesel (B100) was taken mixed with 800 ml of petroleum diesel (IOCL, LDO) to prepare the JCO B20 blend.

1.2. Determination of activation energy

Calculation of activation energy was done using Coats and Redfern method. Coats and Redfern method is an integral method used for non-isothermal kinetic analysis. This method eliminates the rate constant and gives activation energy and frequency factor directly. The equations used in calculation are:

$$\ln \left[\frac{1 - (1 - x)^{(1-n)}}{T^2(1-n)} \right] = \ln \left(\frac{AR}{\beta E_a} \right) \left[1 - \frac{2RT}{E_a} \right] - \frac{E_a}{RT} \quad (\text{for } n \neq 1) \quad (1)$$

and

$$\ln \left[\frac{\ln \left[\frac{1-x}{T^2} \right]}{T^2} \right] = \ln \left(\frac{AR}{\beta E_a} \right) \left[1 - \frac{2RT}{E_a} \right] - \frac{E_a}{RT} \quad (\text{for } n=1) \quad (2)$$

where, x is the fractional weight loss. In Eq. (2) except fractional weight loss (x) and TGA temperature T (also refer to Figure S3), other parameters are constant. Thus plotting a graph

between $\ln \left[\frac{\ln \left[\frac{1-x}{T^2} \right]}{T^2} \right]$ and $\frac{1}{T}$ the value of $-\frac{E_a}{R}$ can be obtained, from which activation energy (E_a) can be calculated.

1.3. Equations used in the determination of performance parameters

Brake power is given by:

$$BP (kw) = \frac{2 \times \Pi \times W \times R}{60000}$$

$$BP (kw) = \frac{0.785 \times RPM \times W \times 9.81 \times \text{arm length}}{60000} \quad (3)$$

Where, W = 9.81 kg, R = radius (m), arm length = 0.00185 (m)

Brake thermal efficiency (η_{bte}) can be expressed as follows:

$$\eta_{bte} = \frac{BP \times 3600 \times 100}{\text{fuel flow rate (kg/hr)} \times \text{calorific value (KJ/kg)}} \quad (4)$$

Indicated thermal efficiency (η_{ite}):

$$\eta_{ite} = \frac{\text{indicated power}}{\text{fuel energy}}$$

$$\eta_{ite} = \frac{IP \times 3600 \times 100}{\text{fuel flow rate (kg/hr)} \times \text{calorific value (kJ/kg)}} \quad (5)$$

Mechanical Efficiency:

$$\eta_{mech} = \frac{BP \times 100}{IP} \quad (6)$$

Volumetric efficiency (%) is given by:

$$\% Vol = \frac{\text{air flow rate} \times 100}{\left(\frac{\Pi}{4}\right) \times D^2 \times \left(\frac{N}{n}\right) \times \text{no of cycle} \times A_{den}} \quad (7)$$

Where, air flow rate (kg/hr):

$$\text{Air flow rate (kg/hr)} = C_d \times \frac{\Pi}{4} \times D^2 \times \sqrt{(2gh_{water} \times \frac{W_{den}}{A_{den}})} \times A_{den} \times 3600 \quad (8)$$

Where, C_d = Co-efficient of discharge of orifice, D = Orifice diameter in meter, g = acceleration due to gravity (m/s^2) = 9.81 m/s^2 , h = differential head across orifice (m of water), W_{den} = Water density (kg/m^3) = @1000 kg/m^3 , A_{den} = p/RT = Air density at working condition (kg/m^3).

Here, p is atmospheric pressure in kgf/m^2 (1 Standard atm = 1.0332 $\times 10^4$ kgf/m^2), R is Gas constant (29.27 $kgfm/kgK$) and T is atmospheric Temperature at K.

Brake specific energy consumption (BSEC) was evaluated from:

$$BSFC = \frac{\text{fuel flow rate (kg/hr)}}{BP} \quad (9)$$

Table S1**Technical Specifications of the CI engine test rig used in the study**

| | |
|---------------------------|--|
| Experimental test rig. | Variable Compression Ratio Diesel Engine test setup with 4 stroke single cylinder (Computerized) |
| Test rig. code | 234 |
| Make | Kirloskar |
| Type | 1 cylinder, 4 stroke, D.I diesel engine |
| Power | 3.5 KW @ 1500 rpm |
| Bore & stroke | 87.5 mm & 110 mm |
| Capacity | 661 CC |
| Cooling method | Water cooled |
| Compression Ratio range | 12:1 to 18:1 |
| Dynamometer | Water cooled eddy current type dynamometer with loading unit |
| Air box | M S fabricated with orifice meter and manometer |
| Temperature sensor | Type RTD, PT100 and Thermocouple, Type K |
| Crank angle sensor | Range 5000 PSI, with low noise cable |
| Piezo sensor | Range 5000 PSI, with low noise cable |
| Crank angle sensor | Resolution 1 Deg, Speed 5500 RPM with TDC pulse. |
| Rotameter | Engine cooling 40-400 LPH; Calorimeter 25-250 LPH |
| Data acquisition Software | “EnginesoftLV” Engine performance analysis software Version 9.0 |
| Load indicator | Digital, Range 0-50 Kg, Supply 230VAC |
| Load sensor | Load cell, type strain gauge, range 0-50 Kg |
| Fuel flow transmitter | DP transmitter, Range 0-500 mm WC |
| Air flow transmitter | DP transmitter, Range 0-500 mm WC |

Table S2

Technical Specifications of the gas analyzer used in this work

| Measured quality | Measuring range | Resolution | Accuracy |
|---------------------|--|---|---|
| CO: | 0-10 % vol | 0.01 % vol | <0.6 % vol: ± 0.03 % vol ≥ 0.6 % vol: $\pm 5\%$ of ind. Val. |
| CO ₂ : | 0-20 % vol | 0.1 % vol | <10 % vol: ± 0.5 % vol ≥ 10 % vol: $\pm 5\%$ vol |
| HC: | 0-20000 ppm vol | ≤ 2000 :1 ppm vol >2000 :10 ppm vol | <200 ppm vol: ± 10 ppm vol ≥ 200 ppm vol: $\pm 5\%$ of ind. Val. |
| O ₂ : | 0-22 % vol | 0.01 % vol | <2 % vol: ± 0.1 % vol ≥ 2 % vol: $\pm 5\%$ of vol |
| NO: | 0-5000 ppm vol | 1 ppm vol | <500 ppm vol: ± 50 ppm vol ≥ 500 ppm vol: $\pm 10\%$ of ind. Val. |
| Miscellaneous | | | |
| Power consumption: | ≈ 25 W | | |
| Connector CAL. Gas: | 60-140 l/h, max. overpressure 450 hPa | | |
| Connector Gas In: | ≈ 180 l/h, max. overpressure 450 hPa | | |
| Dimension (WxDxH): | 270 | 320 x 85 mm ³ | |

Table S3

List of standard test methods used in the study

| Parameter | Standard Methods |
|---------------------------|---|
| Density (40 °C, g/cc) | ASTM D-1250-08 & DIN 51757 |
| Kinematic Viscosity (cSt) | ASTM D-445 & D-2171 |
| Calorific value (MJ/kg) | IS: 1359 –1959, BS 1016: Part 5:1967, IP 12/63T |
| Acidity index (mgKOH/g) | A.O.C.S. Official Method Ca 5a-40 |
| Flash point (°C) | D93 |
| Pour point (°C) | D2500 |
| Fatty acid composition | EN14103 |

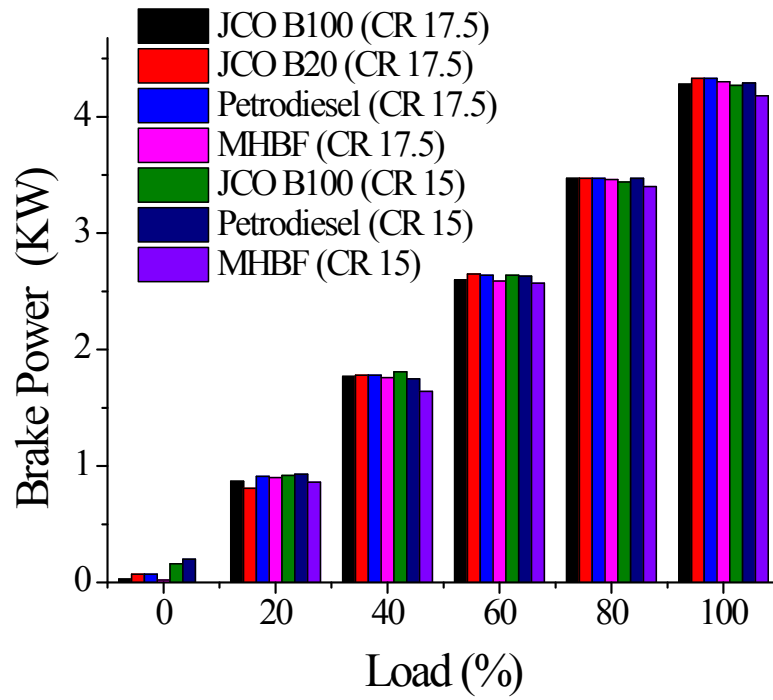


Figure S1. Brake power as a function of engine load for the test fuels (the engine was operating at constant speed of 1500 rpm)

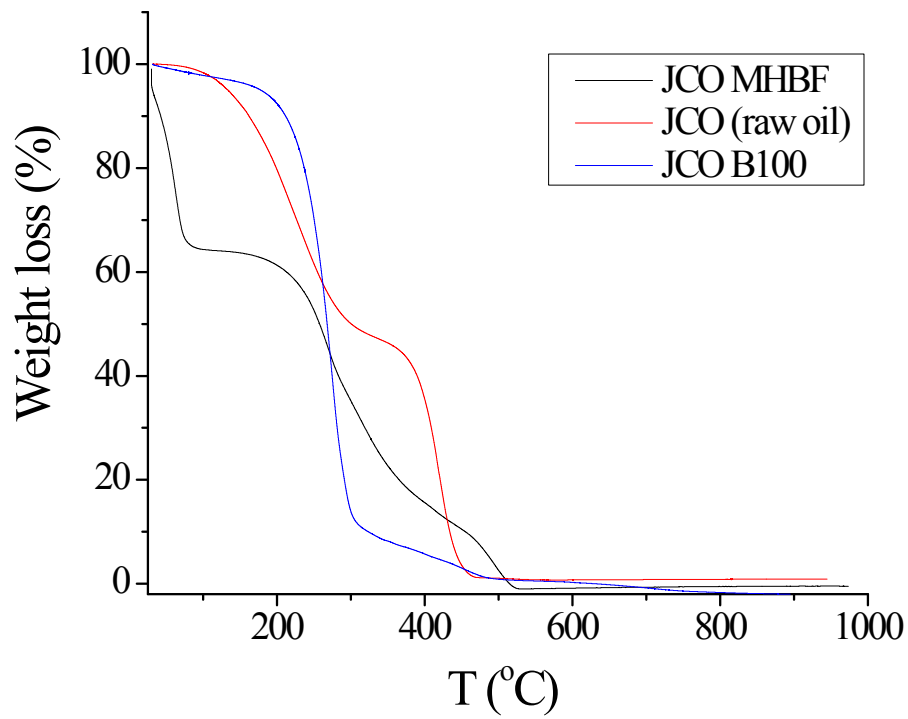


Figure S2. TGA patterns of JCO MHBf, JCO oil and JCO B100 in air.