## Supporting materials

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## Ductile-to-brittle transition and materials' resistance to amorphization by irradiation damage

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\* The shear and bulk moduli are calculated within Voigt approximation. MD represents molecular dynamics. Expt reveals that this data is from experimental findings on single crystal. Calc suggest that this data is from calculations based on DFT. EMTO is the abbreviation of exact muffin-tin orbitals (EMTO) method.

		C	C	C	G	D		C/P	Cauchy Drassura/D	Nota
fcc-Zr	a 4 52	$C_{11}$	$C_{12}$	53 53	U	D	V	G/D	Caucity Pressure/B	FPI APW <sup>1</sup>
fcc-Zr	4.52	115	- 78	48	33	90	0 3373	0 3649	0 3270	This work
fcc-Al	4 04	114 3	61.92	31.62	29	79	0.3355	0.3694	0.3270	Expt <sup>2</sup>
fcc-Al	4.038	105.3	65.1	31	26	79	0.3506	0.3319	0.4343	This work
fcc-Au	4.079	192.3	163.1	42	28	173	0.4244	0.1592	0.7007	$Expt(300K)^3$
fcc-Au	4.173	141	133	30	24	185	0.4376	0.1301	0.7545	This work
fcc-Cu	-	171.0	123.9	75.6	48	140	0.3458	0.3438	0.3444	Expt <sup>4</sup>
fcc-Cu	3.635	178	145	69	39	156	0.3847	0.2499	0.4876	This work
fcc-Ir	3.877	582.1	230.3	252	218	348	0.2404	0.6279	-0.0627	This work
fcc-Ir	3.829	596	252	270	225	367	0.2450	0.6146	-0.0491	Calc <sup>5</sup>
fcc-Ir	-	580	242	256	225	367	0.2450	0.6146	-0.0491	Expt <sup>6</sup>
fcc-Ag	-	124	93.4	46.1	30	104	0.3693	0.2863	0.4566	Expt <sup>6</sup>
fcc-Ag	-	115.8	89	40.7	26	98	0.3776	0.2665	0.4932	Calc <sup>6</sup>
fcc-Pd	-	227.1	176	71.73	47	193	0.3864	0.2458	0.5402	Expt <sup>6</sup>
fcc-Pd	-	198.1	149.7	55.2	40	166	0.3893	0.2391	0.5698	This work
fcc-Pt	-	346.7	250.7	76.5	63	283	0.3956	0.2244	0.6162	Expt <sup>6</sup>
fcc-Pt	-	289.9	224.9	45.9	40	247	0.4231	0.1620	0.7261	This work
fcc-Ni	-	243.6	149.4	119.6	82	181	0.3024	0.4553	0.1648	Expt <sup>6</sup>
fcc-Ni	-	268.2	159.7	130.2	92	196	0.2976	0.4679	0.1505	This work
bcc-Mo	3.150	496	159	107	125	265	0.2958	0.4729	0.1974	This work
bcc-Mo	-	464.7	161.5	109	124	263	0.2955	0.4736	0.2003	Expt/
bcc-Nb	3.322	238	143	14	24	174	0.4346	0.1368	0.7350	This work
bcc-Nb	-	246.6	133.2	28.1	3/	1/1	0.3981	0.2185	0.6146	Expt'
bcc-Fe	2.870	239.55	150.75	120.75	80	1/0	0.2838	0.5051	0.0881	Expt <sup>o</sup>
bcc-la	3.30	200.32	158.10	8/.30	162	194	0.3349	0.3/11	0.3645	Expt <sup>o</sup>
bcc-w	3.10	5166	204.95	103.13	103	314 205	0.2784	0.5200	0.1333	Expl <sup>*</sup>
bee V	-	222.4	199.7	140.7	50	303 157	0.2674	0.4955	0.1730	Evet <sup>8</sup>
bee Cr	5.05	204 1	88 5	45.95	121.2	100 /	0.3302	0.5160	0.4073	OK <sup>9</sup>
bcc-Cr	-	474 Q	54 5	97 <i>4</i>	121.2	178	0.2374	0.0307	-0.2410	This work
bcc-Li	3 4 3 9	15.1	13.4	12.7	79	13.9	0.2150	0.7699	0.0493	This work*
bcc-Li	3.471	-	-	11.7	1.7	14.1		0.0000	0.0175	Calc <sup>10</sup>
bcc-Na	4.193	8.7	7.4	6.8	4.33	7.87		0.5502	0.0829	This work*
bcc-Na	4.200	-	-	6.3		7.67		0.0002	01002)	Calc <sup>10</sup>
bcc-K	4.166	4.5	4.0	2.9	1.8	4.2		0.4286	0.2706	This work*
bcc-K	-	-	-	2.9		3.77				Calc <sup>10</sup>
bcc-Rb	-	-	-	2.2		3.17				Calc <sup>10</sup>
bcc-Rb	-	3.1	2.7	2.1	1.33	2.8		0.4750	0.2200	This work*
bcc-Cs	-	-	-	1.61	2.32					Calc <sup>10</sup>
Diamond-C	3.567	1079	124	578	535	442	0.069	1.2105	-1.0263	Expt <sup>11</sup>
Diamond-C	3.557	-	-	534						LCAO <sup>12</sup>
Diamond-C	3.572	1051.4	125.9	560	519	434	0.073	1.195	-1.000	This work
Diamond-Si	5.4309	-	-	-						Expt <sup>13</sup>
Diamond-Si	5.4345	-	-	-						PBE-HSE
Diamond-Si	5.468	153.3	56.8	75	63	89	0.2150	0.7038	-0.1996	This work
SiC	4.3596	390	142	256	191	225	0.1683	0.8518	-0.5074	Expt <sup>14</sup>
SIC	4.315	420	126	287	219	224	0.1308	0.9/95	-0.7188	
SIC	4.20	383	126.6	240.2	187	212	0.1597	0.8803	-0.5355	This work
AIN	4.58	328	159	133	116	202	0.2590	0.5742	0.029/	
GaN	4.54	264	153	68	63	190	0.3514	0.3299	0.4474	Calc <sup>10</sup>
ININ S: M	5.03	1/2	119	3/ 2/10	32 250	15/	0.3902	0.2308	0.0000	Calc <sup>17</sup>
SI3IN4	-	305 1	191.2	541.0 224 5	238 176	202 242	0.1098	0.8409	-0.4911	Cale <sup>17</sup>
$Ge_3N_4$	-	393.1 292.4	105.4	234.3 52.9	1/0	242 169	0.2072	0.7277	-0.2830	Calc <sup>18</sup>
	-	202.4	106.4	35.0	206	205	0.3262	0.3001	0.3301	Calc <sup>19</sup>
TIN	-	625	100.4	162	200	293	0.2107	0.0985	-0.2030	Exet <sup>19</sup>
TiCrN	-	640.35	123.0	160.22	107	200	0.2342	0.5679	0.1214	Cale <sup>19</sup>
TiZrN	-	503.80	85.07	147.15	183	299	0.2310	0.0558	-0.1214	Calc <sup>19</sup>
TINHN	-	595.09	102.85	146.58	180	255 266	0.2093	0.7200	-0.2430	Calc <sup>19</sup>
TiVN	-	574 78	102.03	150.19	182	200 274	0.2230	0.6676	-0.1044	Calc <sup>19</sup>
TiWN	-	574.01	154 7	134 12	161	294	0.2270	0.5451	0.0700	Calc <sup>19</sup>
TiMoN	-	573 33	191 23	145 00	167	29 <del>4</del> 310	0.2094	0.5084	0.1450	Calc <sup>19</sup>
TiAIN	_	503.87	143.05	174.01	177	263	0.2261	0.6703	-0 1173	Calc <sup>19</sup>
$Zr_2Al$	_	146.45	74.27	75.67	56	98	0.2599	0.5717	-0.0142	Calc <sup>20</sup>
PdZr(Pm-3m)	-	152.9	141.3	34.1	17	145	0.4431	0.1183	0.7385	Calc <sup>21</sup>
MgAl <sub>2</sub> O <sub>4</sub>	-	266.2	148.0	148.6	103	187	0.2684	0.5479	-0.0032	Calc <sup>17</sup>
MgAl <sub>2</sub> O <sub>4</sub>	-	282.9	154.8	155.4	109	198	0.2671	0.5514	-0.0030	Expt <sup>17</sup>
Mg <sub>2</sub> SiO <sub>4</sub>	-	333.7	111.0	140.0	128	185	0.2196	0.6896	-0.1566	Calc <sup>17</sup>
$Mg_2SiO_4$	-	327.0	126.0	112.0	107	193	0.2656	0.5557	0.0725	Expt <sup>17</sup>

TABLE I: The calculated lattice parameters (in Å) and elastic properties (in GPa) of typical fcc and bcc metals, as well as experimental results.

	а	C <sub>11</sub>	C <sub>12</sub>	C <sub>44</sub>	G	В	ν	G/B	Cauchy Pressure/B	Note
NaCl	-	51.6	12.2	13.6	16	25	0.2421	0.6229	-0.0553	Expt <sup>22</sup>
NaCl	-	49.11	12.25	12.84	15	25	0.2483	0.6050	-0.0240	Expt <sup>4</sup>
NaCl	5.653	48.97	11.87	12.31	15	24	0.2504	0.5988	-0.0181	This work
NaCl	-	57.33	11.23	13.31	16.6	26.6	0.2415	0.6246	-0.0782	$4.2K^{23}$
NaCl	-	56.48	11.42	13.30	16.4	26.4	0.2424	0.6221	-0.0711	80K <sup>23</sup>
NaCl	-	50.45	12.99	12.95	15.0	25.5	0.2537	0.5895	0.0016	$240K^{23}$
NaCl	-	49.85	13.05	12.85	14.8	25.3	0.2548	0.5862	0.0079	$260K^{23}$
NaCl	-	49.27	13.08	12.75	14.7	25.1	0.2557	0.5836	0.0131	$280K^{23}$
NaCl	-	48.70	13.11	12.66	14.5	25.0	0.2566	0.5811	0.0180	$300K^{23}$
NaCl	-	49.5	13.2	12.79	14.7	25.3	0.2564	0.5818	0.0162	$300K^{24}$
NaCl	-	47.6	13.3	12.62	14.3	24.7	0.2580	0.5770	0.0275	350K <sup>24</sup>
NaCl	-	44.1	13.5	12.26	13.4	23.7	0.2622	0.5653	0.0523	$450K^{24}$
NaCl	-	40.5	13.5	11.90	12.5	22.5	0.2654	0.5563	0.0711	550K <sup>24</sup>
NaCl	-	37.0	13.1	11.52	11.7	21.1	0.2659	0.5549	0.0750	$650K^{24}$
NaCl	-	33.7	12.9	11.10	10.8	19.8	0.2693	0.5453	0.0908	$750K^{24}$
NaF	-	108.5	22.9	28.99	34.5	51.4	0.2298	0.6591	-0.1184	$4.2K^{*23}$
NaF	-	107.1	23.12	28.97	34.2	51.1	0.2302	0.6579	-0.1145	80K* <sup>23</sup>
NaF	-	98.62	24.28	28.19	31.7	49.1	0.2356	0.6419	-0.0797	260K* <sup>23</sup>
NaF	-	98.07	24.36	28.13	31.3	48.9	0.2360	0.6406	-0.0770	$270K^{23}$
NaF	-	97.49	24.44	28.07	31.45	48.79	0.2365	0.6393	-0.0744	280K* <sup>23</sup>
NaF	-	96.90	24.52	28.01	31.0	48.6	0.2369	0.6380	-0.0717	$290K^{23}$
NaF	-	96.3	24.59	27.94	30.9	48.5	0.2374	0.6367	-0.0691	$300K^{23}$
NaBr	-	48.0	9.86	10.7	14.0	22.6	0.2504	0.5986	-0.0372	$4.2K^{*23}$
NaBr	-	46.45	9.88	10.6	13.7	22.1	0.2505	0.5985	-0.0326	80K* <sup>23</sup>
NaBr	-	41.53	9.95	10.17	12.4	20.5	0.2525	0.5928	-0.0107	240K* <sup>23</sup>
NaBr	-	40.92	9.97	10.11	12.3	20.3	0.2530	0.5914	-0.0069	260K* <sup>23</sup>
NaBr	-	40.31	9.99	10.05	12.1	20.1	0.2535	0.5899	-0.0030	280K* <sup>23</sup>
NaBr	-	39.70	10.01	9.98	11.9	19.9	0.2542	0.5880	-0.0015	300K* <sup>23</sup>
RbBr	-	38.63	4.74	4.085	9.2	16.0	0.2583	0.5762	0.0408	$4.2K^{*23}$
RbBr	-	38.53	4.74	4.083	9.2	16.0	0.2586	0.5755	0.0411	20K* <sup>23</sup>
RbBr	-	38.2	4.74	4.076	9.14	15.9	0.2588	0.5749	0.0418	40K* <sup>23</sup>
RbBr	-	37.75	4.74	4.068	9.04	15.7	0.2590	0.5744	0.0427	$60K^{23}$
RbBr	-	37.25	4.74	4.05	8.9	15.6	0.2593	0.5734	0.0443	80K* <sup>23</sup>
RbBr	-	31.35	5.12	3.77	7.51	13.9	0.2705	0.5418	0.0971	290K* <sup>23</sup>
RbBr	-	31.07	5.15	3.76	7.44	13.8	0.2714	0.5395	0.1007	300K* <sup>23</sup>
KCl	-	40.95	7.05	6.30	9	18	0.2795	0.5169	0.0409	Expt <sup>4</sup>
KCl	6.364	38.7	6.9	6.5	9	18	0.2734	0.5338	0.0269	This work
KCl	-	40.1	5.45	6.35	10.7	17.0	0.2391	0.6318	-0.0530	$300K^{25}$
KCl	-	36.9	5.40	6.21	10.0	15.9	0.2396	0.6302	-0.0509	$400K^{25}$
KCl	-	33.8	5.15	6.11	9.40	14.7	0.2364	0.6395	-0.0653	500K <sup>25</sup>
KCl	-	31.1	5.0	5.96	8.8	13.7	0.2355	0.6423	-0.0700	$600K^{25}$
KCl	-	28.2	4.8	5.79	8.2	12.6	0.2339	0.6468	-0.0786	700K <sup>25</sup>
KCl	-	25.5	4.5	5.57	7.5	11.5	0.2321	0.6522	-0.0930	800K <sup>25</sup>
KCl	-	23.5	4.6	5.57	7.1	10.9	0.2324	0.6514	-0.0890	850K <sup>25</sup>
LiI	6.013	33.7	13.1	13.9	12	20	0.2443	0.6164	-0.0381	This work
LiCl	-	49.27	23.1	24.95	19	32	0.2482	0.6051	-0.0581	Expt <sup>23</sup>
LiCl	-	51.8	21.9	23.6	20	32	0.2441	0.6171	-0.0545	This work
NaF	-	96.9	24.5	28.01	31	49	0.2368	0.6383	-0.0722	Expt <sup>23</sup>
NaF	-	127.4	25.6	33	39	60	0.2294	0.6604	-0.1252	This work
NaBr	-	40.0	10.0	10.02	12	20	0.2538	0.5892	-0.0009	Expt <sup>23</sup>
KF	-	64.9	15.2	12.32	16	32	0.2800	0.5157	0.0907	Expt <sup>25</sup>
RbCl	-	36.46	6.47	4.68	7.6	16.4	0.2993	0.4634	0.1087	Expt <sup>25</sup>
RbBr	-	31.35	5.12	3.774	6.4	13.9	0.3001	0.4612	0.0971	Expt <sup>25</sup>
RbI	-	25.75	3.4	2.778	5.1	10.9	0.2984	0.4658	0.0573	Expt <sup>25</sup>
NaH(NaCl)	-	47.3	2.5	22.5	22.5	17.4	0.0494	1.288	-1.147	Expt <sup>26</sup>
NaH(NaCl)	-	59.1	9.2	22.02	23.1	25.8	0.1550	0.8961	-0.4963	GGA <sup>20</sup>
NaH(CsCl)	-	73.02	11.9	30.11	30.3	32.3	0.1426	0.9385	-0.5642	GGA <sup>20</sup>
RbH(NaCl)	-	26.46	7.93	10.97	10.3	14.1	0.2072	0.7277	-0.2157	GGA <sup>20</sup>
RbH(CsCl)	-	42.0	1.4	12.0	14.8	14.9	0.1269	0.9933	-0.7098	GGA <sup>20</sup>
RbH(NaCl)	-	26.46	7.93	10.97	10.3	14.1	0.2072	0.7277	-0.2157	GGA <sup>20</sup>
RbH(CsCl)	-	42.0	1.4	12.0	14.8	14.9	0.1269	0.9933	-0.7098	GGA <sup>20</sup>
L1H(NaCl)	-	66.4	15.6	45.8	36.2	32.5	0.0946	1.1112	-0.9283	Expt <sup>20</sup>
LiH(NaCl)	-	84.7	14.0	48.9	42.9	37.6	0.0863	1.1423	-0.9287	this work
L1H(CsCl)	-	66.5	12.0	32.0	30.0	30.2	0.1265	0.9947	-0.6630	GGA <sup>20</sup>
KH(NaCl)	-	31.1	8.35	14.47	13.1	15.9	0.1766	0.8247	-0.3841	GGA <sup>26</sup>
KH(CsCl)	-	51.0	4.5	20.0	21.2	20.0	0.1078	1.062	-0.7750	GGA <sup>20</sup>
CsH(NaCl)	-	23.23	6.761	9.74	9.1	12.3	0.2021	0.7434	-0.2432	GGA <sup>20</sup>
CsH(CsCl)	-	38.0	3.2	6.5	9.8	14.8	0.2295	0.6599	-0.2230	GGA <sup>20</sup>

TABLE II: The calculated lattice parameters (in Å) and elastic properties (in GPa) of cubic structures, as well as experimental results(continued)

	0	0	0		D		<u>C</u> /D		N
Na	$\frac{C_{11}}{1.21}$	$C_{12}$	0.58	G 0.46	B 0.97	V 0.2742	$\frac{G/B}{0.5217}$	Cauchy Pressure/B	This work
Ne	1.31	0.05	0.58	0.40	0.87	0.2742	0.3317	0.0805	1 mis work $OCD_{2}$ 22 $7V^{27}$
INC No	1.200	0.752	0.055	0.427	0.89	0.2952	0.4798	0.1112	00Pa, 25.7K
INC A r	1.173	0.74	1.24	0.398	0.885	0.3040	0.4495	0.1058	00Pa, 24.5K
Ar	2.40	1.55	1.24	0.84	1.65	0.3017	0.4371	0.1370	00Pa,82K
Ar	2.38	1.30	1.12	0.75	1.83	0.3202	0.4085	0.2400	82.3K <sup>22</sup>
Ar	10	8.4	1.5	5.7	10.9	0.2770	0.5222	0.0823	2GPa, RT <sup>30</sup> 4CD- DT <sup>30</sup>
Ar	32	10.5	11.0	9.9	21.5	0.3003	0.4607	0.2185	$4$ GPa, $R1^{30}$
Ar	48	21.9	17.6	15.6	30.6	0.2820	0.5102	0.1405	6GPa,R1 <sup>50</sup>
Ar	/4	33.3	27.1	24.2	46.9	0.2800	0.5156	0.1323	10GPa,R1 <sup>30</sup>
Ar	109	44	41	37.4	65.7	0.2609	0.5689	0.0457	15GPa,RT <sup>30</sup>
Ar	142	54	54	49.8	83.3	0.2510	0.5970	0.0000	20GPa,RT <sup>30</sup>
Ar	178	63	68	63.6	101.3	0.2405	0.6275	-0.493	25GPa,RT <sup>30</sup>
Ar	211	/1	80	75.8	111.7	0.2347	0.6445	-0.0765	30GPa,RT <sup>50</sup>
Kr	4.99	2.86	2.69	1.85	3.57	0.2785	0.5197	0.0476	This work
Kr	5.14	2.84	2.68	1.9	3.61	0.2751	0.5292	0.0444	0GPa,10K <sup>51</sup>
Kr	2.89	1.85	1.44	0.96	2.20	0.3097	0.4359	0.1866	0GPa,114K <sup>27</sup>
Kr	2.657	1.725	1.261	0.85	2.04	0.3174	0.4157	0.2279	0GPa,115.6K <sup>32</sup>
Kr	14	8	11	7.8	10.0	0.1905	0.7800	-0.3000	2GPa,RT <sup>33</sup>
Kr	36	17	21	16.4	23.3	0.2149	0.7039	-0.1714	5GPa,RT <sup>33</sup>
Kr	71	29	34	28.0	43.0	0.2323	0.6518	-0.1163	10GPa,RT <sup>33</sup>
Kr	101	46	45	36.9	64.3	0.2591	0.5741	0.0155	15GPa,RT <sup>33</sup>
Kr	131	62	56	50	83.3	0.2510	0.5970	0.0000	20GPa,RT <sup>33</sup>
Kr	160	79	64	53.3	106.0	0.2848	0.5026	0.1415	25GPa,RT <sup>33</sup>
Kr	184	97	70	57.8	126.0	0.3009	0.4591	0.2143	30GPa,RT <sup>33</sup>
Kr	205	118	73	59.3	147.0	0.3222	0.4035	0.3061	35GPa,RT <sup>33</sup>
Xe	5.45	3.17	2.97	2.0	3.93	0.2803	0.5148	0.0509	This work
Xe	5.27	2.82	2.95	2.1	3.64	0.2604	0.5702	-0.0357	0GPa,10K <sup>34</sup>
Xe	2.98	1.9	1.48	0.99	2.26	0.3092	0.4373	0.1858	0GPa,156K <sup>35</sup>
Xe	7.20	5.15	2.92	1.92	5.83	0.3517	0.3292	0.3823	0.45GPa,296K <sup>36</sup>
Xe	19.1	13.1	8.55	5.6	15.1	0.3344	0.3723	0.3013	2.11GPa,296K <sup>36</sup>
Xe	24.7	17.2	10.9	7.1	19.7	0.3389	0.3610	0.3198	2.96GPa,296K <sup>36</sup>
Xe	28.9	19.3	12.6	8.6	22.5	0.3312	0.3804	0.2978	3.73GPa,296K <sup>36</sup>
Xe	36.7	24.0	14.8	10.5	28.2	0.3340	0.3733	0.3259	4.95GPa,296K <sup>36</sup>
Xe	43.0	28.7	18.3	12.6	33.5	0.3333	0.3751	0.3108	6.08GPa,296K <sup>36</sup>
Xe	55.7	37.5	22.5	15.6	43.5	0.3396	0.3592	0.3443	8.04GPa,296K <sup>36</sup>
Xe	63.7	42.3	26.7	18.5	49.4	0.3336	0.3743	0.3156	10.6GPa,296K <sup>36</sup>
Al-Li0.05	103.1	60.6	42.1	31.9	74.8	0.3127	0.4280	0.2474	EMT <sup>37</sup>
Al-Li0.10	101.1	58.2	43.3	32.6	72.5	0.3042	0.4505	0.2055	EMTO <sup>37</sup>
Al-Li0.15	94.7	54.9	42.5	31.3	68.2	0.3007	0.4598	0.1819	EMTO <sup>37</sup>
Al-Li0.20	91.0	50.1	40.9	30.9	63.7	0.2909	0.4859	0.1444	EMTO <sup>37</sup>
Fe-Cr0.025	284.2	131.5	108.6	94.3	182.4	0.2795	0.5170	0.1256	EMTO <sup>38</sup>
Fe-Cr0.05	280.0	126.9	112.8	96.6	177.9	0.2702	0.5427	0.0792	EMTO <sup>38</sup>
Fe-Cr0.075	283.5	127.2	117.5	99.8	179.3	0.2653	0.5565	0.0541	EMTO <sup>38</sup>
Fe-Cr0.10	287.8	127.9	120.7	102.3	181.2	0.2624	0.5647	0.0397	EMTO <sup>38</sup>
Fe-Cr0.125	292.3	129.5	122.4	103.9	183.8	0.2621	0.5656	0.0386	EMTO <sup>38</sup>
Fe-Cr0.15	296.8	131.7	124.1	105.4	186.7	0.2625	0.5644	0.0407	EMTO <sup>38</sup>
Fe-Cr0.175	305.0	137.2	125.6	106.8	193.1	0.2665	0.5532	0.0601	EMTO <sup>38</sup>
Fe-Cr0.2	305.5	136.3	126.0	107.4	192.7	0.2650	0.5574	0.0535	EMTO <sup>38</sup>
Fe-Cr0.2	305.5	136.3	126.0	107.4	192.7	0.2650	0.5574	0.0535	EMTO <sup>38</sup>
Fe-Mg0.025	263.7	125.3	103.6	88.1	171.4	0.2806	0.5141	0.1266	EMTO <sup>38</sup>
Fe-Mg0.05	235.8	112.7	101.0	82.8	153.7	0.2717	0.5386	0.0761	EMTO <sup>38</sup>
Fe-Mg0.075	211.0	102.4	98.9	77.8	138.6	0.2637	0.5610	0.0253	EMTO <sup>38</sup>
Fe-Mg0.1	189.7	93.4	97.9	73.6	125	0.2546	0.5867	-0.0359	EMTO <sup>38</sup>
NiCoFeCr	271	175	189.3	109.9	207	0.2358	0.6414	-0.0691	EMTO <sup>39</sup>
NiCoFeCrTi	184.5	170.9	127.0	47.3	175.4	0.3044	0.4497	0.2502	EMTO <sup>39</sup>
CuNiCoFeCrTi0.1	219.7	152.6	160.2	109.5	174.9	0.2410	0.6261	-0.0434	EMTO <sup>39</sup>
CuNiCoFeCrTi0.2	213.6	152.1	155.1	105.4	172.6	0.2464	0.6104	-0.0174	EMTO <sup>39</sup>
CuNiCoFeCrTi0.3	209.6	151.9	154.6	104.3	171.1	0.2467	0.6095	-0.0158	EMTO <sup>39</sup>
CuNiCoFeCrTi0.4	207.6	151.7	150.8	101.7	170.3	0.2511	0.5968	0.0053	EMTO <sup>39</sup>
CuNiCoFeCrTi0.5	198.4	151.0	142.7	95.1	166.8	0.2605	0.5701	0.0498	EMTO <sup>39</sup>
CuNiCoFeCrTi0	227.8	154.6	165.3	113.8	179.0	0.2377	0.6359	-0.0598	EMTO <sup>39</sup>
CuNiCoFeCrTi1	174.3	148.6	125.0	80.1	157.2	0.2821	0.5099	0.1502	EMTO <sup>39</sup>

TABLE III: The elastic properties (in GPa) of cubic structures, as well as experimental results(continued)

TABLE IV: The elastic properties (in GPa) of cubic structures, as well as experimental results(continued)

	C <sub>11</sub>	C <sub>12</sub>	C <sub>44</sub>	G	В	ν	G/B	Cauchy Pressure/B	Note
ZrO <sub>2</sub> -8mol%Y <sub>2</sub> O <sub>3</sub>	401.8	95.2	55.8	94.8	197.4	0.2930	0.4802	0.1996	RT* <sup>40</sup>
ZrO <sub>2</sub> -11.1mol%Y <sub>2</sub> O <sub>3</sub>	403.5	102.4	59.9	96.2	202.8	0.2953	0.4742	0.2096	RT* <sup>40</sup>
ZrO <sub>2</sub> -12.1mol%Y <sub>2</sub> O <sub>3</sub>	405.1	105.3	61.8	97.0	205.2	0.2957	0.4729	0.2120	RT* <sup>40</sup>
ZrO <sub>2</sub> -15.5mol%Y <sub>2</sub> O <sub>3</sub>	397.6	108.6	65.8	97.3	204.9	0.2950	0.4749	0.2088	RT* <sup>40</sup>
ZrO <sub>2</sub> -17.9mol%Y <sub>2</sub> O <sub>3</sub>	390.4	110.8	69.1	97.4	204.0	0.2941	0.4775	0.2044	RT*40
ZrO <sub>2</sub> -11.1mol%Y <sub>2</sub> O <sub>3</sub>	400.2	101.8	59.0	95.1	201.3	0.2959	0.4724	0.2127	373K* <sup>40</sup>
$ZrO_2$ -11.1mol% $Y_2O_3$	395.6	101.0	57.7	93.5	199.2	0.2971	0.4694	0.2174	473K* <sup>40</sup>
$ZrO_2$ -11.1mol% $Y_2O_3$	389.8	99.8	56.0	91.6	196.5	0.2983	0.4662	0.2229	573K* <sup>40</sup>
$ZrO_2$ -11.1mol% $Y_2O_3$	382.0	97.1	54.1	89.4	192.1	0.2986	0.4654	0.2239	673K* <sup>40</sup>
$ZrO_2$ -11.1mol% $Y_2O_3$	373.1	91.2	52.2	87.7	185.2	0.2955	0.4735	0.2106	773K* <sup>40</sup>
$ZrO_2$ -11.1mol% $Y_2O_3$	364.7	88.9	50.1	85.2	180.8	0.2964	0.4712	0.2146	873K* <sup>40</sup>
$ZrO_2$ -11.1mol% $Y_2O_3$	356.6	86.8	48.0	82.8	176.7	0.2974	0.4686	0.2195	973K* <sup>40</sup>
$ZrO_2$ -12.1mol% $Y_2O_3$	401.6	104.8	60.9	95.9	203.7	0.2965	0.4/0/	0.2155	373K*40
$ZrO_2$ -12.1mol% $Y_2O_3$	396.6	104.3	59.5	94.2	201.7	0.2979	0.4670	0.2221	4/3K***
$ZrO_2$ -12.1mol% $Y_2O_3$	391.2	102.9	57.9	92.4	199.0	0.2990	0.4643	0.2261	5/3K <sup>*+0</sup>
$ZrO_2$ -12.1mol% $Y_2O_3$	385.1	02.4	54.9	90.8	195.5	0.2987	0.4649	0.2255	0/3K*** 772V*40
$Z_1O_2$ -12.11101% $I_2O_3$ $Z_rO_12.1mol% V_0$	370.9	95.4	52.0	90.0	100.0	0.2941	0.4772	0.2047	972V *40
$Z_1O_2$ -12.11101% $I_2O_3$ $Z_rO_12.1mol%VO_2$	364.8	82.6	51.5	09.0 87.3	102.0	0.2090	0.4690	0.1852	073K*40
$Z_1O_2$ -12.11101% $I_2O_3$ $Z_rO_155mol%VO_2$	304.0	02.0	51.5 64.0	07.5	203.6	0.2079	0.4941	0.1700	973K*40
$Z_1O_2$ -15.5mol%V.O.	394.5	108.2	63.5	90.2 04.6	203.0	0.2939	0.4725	0.2120	73K* <sup>40</sup>
$ZrO_2$ -15.5mol% $V_2O_3$	384.7	107.5	61.0	02.8	100.2	0.2970	0.4650	0.2174	573K* <sup>40</sup>
$ZrO_2$ -15.5mol% $V_2O_3$	379.5	105.0	59.9	90.8	199.2	0.2904	0.4621	0.2294	673K* <sup>40</sup>
$ZrO_2$ -15.5mol% $V_2O_3$	373.6	102.0	57.7	88.9	190.5	0.2998	0.4616	0.2295	773K* <sup>40</sup>
$ZrO_2$ -15.5mol%Y <sub>2</sub> O <sub>3</sub>	366.8	98.2	553	86.9	192.0	0.2995	0.4630	0.2305	873K* <sup>40</sup>
$ZrO_2 - 15.5mol\% Y_2O_3$	360.2	96.3	52.6	84.3	184.3	0.3016	0.4574	0.2203	973K* <sup>40</sup>
$ZrO_2$ -17.9mol%Y <sub>2</sub> O <sub>2</sub>	387.0	109.9	68.1	96.3	202.3	0.2946	0.4760	0.2067	373K* <sup>40</sup>
$ZrO_2$ -17.9mol% $Y_2O_3$	382.8	108.9	66.7	94.8	200.2	0.2955	0.4735	0.2108	473K* <sup>40</sup>
$ZrO_2$ -17.9mol% $Y_2O_3$	378.1	107.5	65.2	93.2	197.7	0.2963	0.4714	0.2140	573K* <sup>40</sup>
$ZrO_{2}-17.9mol\%Y_{2}O_{3}$	373.4	105.6	63.3	91.5	194.9	0.2970	0.4695	0.2171	673K* <sup>40</sup>
ZrO <sub>2</sub> -17.9mol%Y <sub>2</sub> O <sub>3</sub>	368.2	100.5	61.2	90.3	189.7	0.2946	0.4760	0.2071	773K* <sup>40</sup>
$ZrO_2-17.9mol\%Y_2O_3$	361.4	98.1	58.8	87.9	185.9	0.2958	0.4728	0.2114	873K* <sup>40</sup>
$ZrO_2$ -17.9mol% $Y_2O_3$	353.8	94.0	56.2	85.7	180.6	0.2951	0.4745	0.2093	973K* <sup>40</sup>
Fe-30Al	147	96.3	116.3	79.9	113.2	0.2143	0.7058	-0.1767	273K*41
Fe-30Al	137.2	92.4	110.4	75.2	107.3	0.2159	0.7008	-0.1677	428K* <sup>41</sup>
Fe-30Al	134.2	91.4	108.9	73.9	105.7	0.2165	0.6991	-0.1656	473K* <sup>41</sup>
Fe-30Al	131.1	90.4	107.3	72.5	104.0	0.2171	0.6973	-0.1626	523K* <sup>41</sup>
Fe-30Al	128.3	89.6	105.3	70.9	102.5	0.2189	0.6917	-0.1532	573K* <sup>41</sup>
Fe-30Al	123.4	87.3	100.6	67.6	99.3	0.2226	0.6804	-0.1339	673K* <sup>41</sup>
Fe-30Al	117.9	83.8	95.1	63.9	95.2	0.2258	0.6710	-0.1187	773K* <sup>41</sup>
Fe-30Al	111.3	79.7	89.1	59.8	90.2	0.2287	0.6625	-0.1042	873K* <sup>41</sup>
Fe-30Al	103.9	75.8	86.1	57.3	85.2	0.2253	0.6725	-0.1209	973K* <sup>41</sup>
Fe-30Al	92.3	69.3	78.5	51.7	76.9	0.2256	0.6717	-0.1195	1173K* <sup>41</sup>
MgO	298.96	96.42	157.13	131.8	163.9	0.1831	0.8037	-0.3703	300K <sup>42</sup>
MgO	292.94	97.02	155.78	129.3	162.3	0.1852	0.7968	-0.3620	400K <sup>42</sup>
MgO	296.92	97.64	154.33	126.8	160.7	0.1876	0.7892	-0.3527	500K <sup>42</sup>
MgO	280.62	98.0	152.84	124.3	158.9	0.1897	0.7824	-0.3452	600K <sup>42</sup>
MgO	2/4.4/	98.43	151.31	121.8	15/.1	0.1921	0.7750	-0.3366	/00K <sup>42</sup>
MgO M-O	268.22	98.54	149.68	119.2	155.1	0.1941	0.7685	-0.3297	800K <sup>42</sup>
MgO M-O	261.94	98.62	148.1	110.0	155.1	0.1962	0.7620	-0.3233	900K <sup>42</sup>
MgO MaO	235.14	90./4 00 C	140.52	114.1	131.1	0.1984	0.7350	-0.3103	1000K <sup>*2</sup> 1100V <sup>42</sup>
MgO	249.52	90.0	144.//	111.3	146.9	0.2005	0.7483	-0.5101	1200K42
MgO	245.52	90.30	145.00	106.9	140.7	0.2023	0.7425	-0.3040	1200K 1200K <sup>42</sup>
MgO	237.13	98.05	141.55	100.5	144.4	0.2044	0.7302	-0.2997	1300K 1400K <sup>42</sup>
MgO	230.90	97.50	139.34	105.8	142.0	0.2002	0.7500	-0.3233	1400K 1500K <sup>42</sup>
MgO	224.00	96.44	136.24	08.0	137.2	0.2001	0.7249	-0.2920	1600K <sup>42</sup>
MgO	217.04	90.44	134.65	90.9 96.6	13/ 0	0.2090	0.7201	-0.2099	1700K <sup>42</sup>
MgO	213.43	95.09	133.12	9 <u>4</u> 4	137.7	0.2110	0 7115	-0.2887	1800K <sup>42</sup>
CaO	220.18	57 67	80.03	27.7 80.6	111 9	0.2097	0.7198	-0 1997	300K <sup>43</sup>
CaO	215.66	57.96	79 34	79 14	110.5	0.2110	0.7161	-0 1934	400K <sup>43</sup>
CaO	210.73	58.23	78.70	77.7	109.1	0.2121	0.7125	-0.1877	500K <sup>43</sup>
CaO	205.88	58.44	77.94	76.22	107.6	0.2134	0.7085	-0.1812	600K <sup>43</sup>
CaO	201.22	58.66	77.18	74.76	106.2	0.2149	0.7041	-0.1744	700K <sup>43</sup>
CaO	196.58	58.81	76.46	73.3	104.7	0.2162	0.7002	-0.1685	800K <sup>43</sup>
CaO	192.03	58.98	75.72	71.9	103.3	0.2176	0.6958	-0.1620	900K <sup>43</sup>
CaO	187.24	58.98	74.92	70.4	101.7	0.2189	0.6920	-0.1567	$1000K^{43}$
CaO	182.74	58.96	74.17	68.9	100.2	0.2200	0.6884	-0.1518	1100K <sup>43</sup>
CaO	178.11	58.99	73.48	67.6	98.7	0.2213	0.6845	-0.1468	$1200K^{43}$

TABLE V: The calculated lattice parameters (in Å) and elastic properties (in GPa) of hexagonal and tetragonal structure, as well as experimental results

	а	с	C <sub>11</sub>	C <sub>12</sub>	C <sub>13</sub>	C <sub>33</sub>	C <sub>44</sub>	C <sub>66</sub>	G	В	ν	G/B	Cauchy Pressure/B	Note
Ti	-	-	160	90	66	181	46.5	35	43	105	0.3184	0.4133	0.3548	Expt <sup>44</sup>
Zr	-	-	145.3	63.9	66.5	165.4	27.5	40.7	36	94	0.3322	0.3779	0.3297	Expt <sup>44</sup>
Sc	-	-	92.9	31.7	30.1	90.6	31.4	30.6	31	51	0.2479	0.6061	-0.0019	Calc <sup>44</sup>
Sc	-	-	99.3	39.7	29.4	107	27.7	29.8	31	56	0.2684	0.5478	0.1039	Expt <sup>44</sup>
Y	-	-	77.4	23.9	21.3	80.9	22.4	26.8	25	41	0.2427	0.6213	-0.049	Calc <sup>44</sup>
Y	-	-	77.9	29.2	21.0	76.9	24.7	24.4	26	43	0.2525	0.5928	0.0134	Expt <sup>44</sup>
Re	-	-	649	269.4	187.6	678.1	185	189.8	199	363	0.2678	0.5493	0.1134	Calc <sup>44</sup>
Re	-	-	634.4	266	202	701.1	169.1	184.2	189	368	0.2804	0.5145	0.1559	Expt <sup>44</sup>
Tb	-	-	73.8	20.3	18.1	75.2	24.1	26.8	26	37	0.2169	0.6978	-0.1677	Calc <sup>44</sup>
Tb	-	-	68.6	24.7	22.4	73.3	21.6	22.0	22	39	0.2580	0.5770	0.0451	Expt <sup>44</sup>
Tc	-	-	525.4	229.7	184.7	596.3	160	147.8	162	316	0.2807	0.5137	0.1686	Calc <sup>44</sup>
Ru	-	-	622.5	203	179.8	724.6	212.4	210	220	343	0.2361	0.6404	-0.0573	Calc <sup>44</sup>
Ru	-	-	563	188	168	624	181	187.5	191	311	0.2448	0.6149	-0.0201	Expt <sup>44</sup>
Gd	-	-	70.0	23.1	18.2	72.1	21.6	23.4	23	37	0.2378	0.6353	-0.0493	Calc <sup>44</sup>
Gd	-	-	67.8	25.6	20.7	71.2	20.8	21.1	22	38	0.2587	0.5751	0.0585	Expt <sup>44</sup>
Os	-	-	816.3	225.2	256.1	915	312.7	295.5	305	446	0.2218	0.6831	-0.1422	Calc <sup>44</sup>
Na <sub>2</sub> Bi	5.469	9.735	35.9	13.5	4.0	40.9	7.0	11.2	10	17	0.2490	0.6029	-0.0202	This work
Na <sub>2</sub> Bi	5.448	9.655	-	-	-	-	-	-						Expt <sup>45</sup>
K <sub>2</sub> Bi	6.217	11.044	20.0	9.4	3.0	24.7	4.2	5.3	6	11	0.2735	0.5336	0.1372	This work
Graphene	2 4 6 9	8 346	896.6	176.0	23.0	104.3	40.7	360.3	136	177	0 1931	0 7715	-0 5713	This work*
Graphene	2.46	-	-	-	-	-	-	360.3	150	177	0.1701	0.7710	0.0715	Exnt
NaBi	3 4 4 3	4 886	64.6	197	13.6	467	115	91	14	29	0 2933	0 4796	0.2153	This work
	-	000	345	125	120	305	11.5	110	117	201	0.2555	0.5807	0.0422	Expt <sup>46</sup>
GaN			367	125	103	405	05	116	117	201	0.2507	0.5575	0.0422	$Calc^{46}$
GaN			300	145	105	308	105	122.5	120	202	0.2049	0.5575	0.0559	Expt <sup>46</sup>
InN	-	-	100	145	121	182	105	122.5	22	130	0.2399	0.3718	0.0339	Cala <sup>16</sup>
IIIN DoN	-	-	190 570	252	202	102	110	45	152	250	0.4237	0.1008	0.0175	Cale <sup>47</sup>
Do N	-	-	570	232	202	794 970	102	139	212	339	0.3133	0.4203	0.2380	Cale <sup>47</sup>
$Re_2N$	-	-	657	237	238	870 704	192	212.3	213	407	0.2770	0.5259	0.1111	Calc <sup>47</sup>
	-	-	210	240	244	794	198	204.5	215	401	0.2742	0.3317	0.1110	Calc <sup>48</sup>
Z110 7=0	-	-	210	121	105	211	43	44.5	40	144	0.5550	0.5195	0.4825	Calc <sup>10</sup>
ZnO Zn Al	-	-	191.9	107.5	88.0	21/	38.3	42.5	= =	102	0 2722	0 5241	0.1604	Calc <sup>10</sup>
$Zr_2AI$	-	-	1/8.08	85.10	53.25	180.08	57.19	46.4	22	103	0.2/33	0.5341	0.1694	$Calc^{20}$
$Zr_4Al_3$	-	-	218.20	40.11	57.23	213.10	/4.6	89	80	106	0.1985	0.7546	-0.3112	$Calc^{20}$
$Zr_5Al_4$	-	-	184./3	/6.54	48.72	192.69	30.36	54	46	101	0.3026	0.4546	0.2024	$Calc^{20}$
$ZrAl_2$	-	-	236.81	46.65	57.05	217.22	90.01	95.0	90	112	0.1836	0.8020	-0.3615	Calc <sup>20</sup>
$Pd_3Zr$	-	-	268	90	99	305	70	89	82	157	0.2778	0.5217	0.0955	
parahydrogen	-	-	0.334	0.13	0.056	0.408	0.104	0.102	82	157	0.2778	0.5217	0.0955	13.2K <sup>4</sup>
SnO <sub>2</sub>	-	-	260	197	117	429	131	225	109	200	0.2703	0.5426	-0.1049	Calc <sup>50</sup>
$SnO_2$	-	-	262	177	156	449	103	207	102	212	0.2937	0.4784	0.054	Expt <sup>30</sup>
$IrN_2$	-	-	322	301	217	553	103	273	83	294	0.3705	0.2835	0.2419	Calc
$V_2B$	-	-	496	94	122	442	223	197	200	234	0.1673	0.8550	-0.4352	Calc <sup>51</sup>
Nb <sub>2</sub> B	-	-	439	89	143	361	164	145	150	221	0.2226	0.6807	-0.1743	
Ta <sub>2</sub> B	-	-	475	101	154	393	173	175	165	240	0.2207	0.6864	-0.1938	
$V_3B_2$	-	-	551	89	132	459	215	183	202	252	0.1836	0.8021	-0.3517	
$Nb_3B_2$	-	-	474	92	121	449	169	135	164	229	0.2108	0.7167	-0.1983	
$Ta_3B_2$	-	-	506	126	141	470	204	150	182	255	0.2121	0.7125	-0.1704	Calc <sup>51</sup>
$VB_2$	-	-	672	120	130	470	223	276	237	283	0.1718	0.8402	-0.4405	
NbB <sub>2</sub>	-	-	602	106	186	429	218	248	209	286	0.20/1	0.7279	-0.3037	
TaB <sub>2</sub>	-	-	596	142	196	427	190	227	190	297	0.2362	0.6402	-0.1331	Calc <sup>51</sup>
$C_4$	-	-	932.6	172.1	58.5	1189.6	446.7	324.5	422	403	0.1121	1.046	-0.6708	
Sn	-	-	74.2	58	22.2	81.2	23.4	9.9	17	48	0.3388	0.3612	0.4904	
$ZrAl_3$	-	-	203.98	65.35	44.7	202.2	81.06	100.21	82	102	0.1824	0.8057	-0.3489	Calc <sup>20</sup>
$Zr_5Al_3$	-	-	183.2	67.59	61.27	167.57	32.65	64.61	47	101	0.2999	0.4618	0.1979	Calc <sup>20</sup>
$Pd_{11}Zr_9$	-	-	171	127	116	187	36	23	30	139	0.4003	0.2136	0.6641	Calc <sup>53</sup>
$PdZr_2$	-	-	197	86	106	149	64	47	49	126	0.3292	0.3856	0.3214	Calc <sup>53</sup>
MoSi <sub>2</sub>	-	-	410	114.9	87.5	514	207	200	190.7	212.1	0.1541	0.8991	-0.4823	Calc <sup>54</sup>
WSi <sub>2</sub>	-	-	442.8	121.7	81.0	552.3	211.6	217.5	203.5	222.4	0.1494	0.9151	-0.5089	Expt <sup>54</sup>
WSi <sub>2</sub>	-	-	372	116	81.6	596	211	236	197	208	0.1401	0.9471	-0.5996	Calc <sup>54</sup>
MoSi <sub>2</sub>	-	-	403.7	114.5	88.0	505.3	202.7	194.8	186.5	209.9	0.1572	0.8888	-0.4646	Expt <sup>54</sup>
MoSi <sub>2</sub>	-	-	345	109	87.7	547	190	220	178.8	197.7	0.1525	0.9046	-0.5393	Calc <sup>54</sup>
CrSi <sub>2</sub>	-	-	372.2	45.3	82.6	385.2	149.1	163.5	153	171.9	0.1563	0.8916	-0.5370	Expt <sup>54</sup>
CrSi <sub>2</sub>	-	-	372	45.3	68.3	441	146	163	157.4	171.1	0.1481	0.9195	-0.5708	Calc <sup>54</sup>
VSi <sub>2</sub>	-	-	357.8	50.6	68.1	422.3	146	153.6	152.3	167.2	0.1507	0.9108	-0.5410	Expt <sup>54</sup>
VSi <sub>2</sub>	-	-	356	50.6	67.0	430	135.7	154	148.3	167.0	0.1574	0.8800	-0.5153	Calc <sup>54</sup>
NbSi <sub>2</sub>	-	-	380.2	75.9	88.3	468	145.3	152.2	153.2	191.5	0.1843	0.7996	-0.3480	Expt <sup>54</sup>
NbSi <sub>2</sub>	-	-	380	75.9	80.4	508	144	152	155.8	191.8	0.1803	0.8124	-0.3652	Calc <sup>54</sup>
TaSi <sub>2</sub>	-	-	375	78.4	90.1	476.7	143.7	148.5	151.1	192.4	0.1887	0.7855	-0.3215	Expt <sup>54</sup>
TaSi <sub>2</sub>	-	-	375	78.4	82.1	517	142	148	153.4	192.7	0.1854	0.7962	-0.3361	Calc <sup>54</sup>

TABLE VI: The elastic properties (in GPa) of cubic, tetragonal and orthorhombic structure, as well as experimental results.

	C	C	C	C	C	C	C	C	C	G	D		C/P	Caughy Drassurg/D	Noto
	C <sub>11</sub>	C <sub>12</sub>	C <sub>13</sub>	C <sub>23</sub>	C <sub>22</sub>	C33	<u>C44</u>	C55	C66	0	D	V	0/0	Cauchy Flessure/B	Note
TiSi <sub>2</sub>	317.5	29.35	38.45	86.0	320.4	413.2	112.5	75.8	117.5	117.0	148.9	0.1887	0.7856	-0.3403	Calc <sup>34</sup>
TiSi <sub>2</sub>	276	29.9	33.4	93.5	302	394	119	755	134	116.2	140.9	0.1765	0.8249	-0.3944	Calc <sup>54</sup>
Mo(Si.Al) <sub>2</sub>	402.8	74.2	107.1	-	-	434.4	148.2	-	164.3	155.3	201.4	0.1932	0.7714	-0.3258	RT <sup>55</sup>
Mo(Si Al)	398.0	75.2	107.8	_	_	430.6	146.4	_	161 7	153.1	200.4	0 1956	0 7638	-0.3121	400K <sup>55</sup>
$M_{0}(S; A1)$	202.1	72.9	107.0			420.7	144.2		150.5	150.0	106.6	0.1047	0.7667	0.2171	500K55
$MO(SI,AI)_2$	392.1	75.0	105.5	-	-	420.7	144.5	-	159.5	130.8	190.0	0.1947	0.7007	-0.31/1	500K
$Mo(S1,AI)_2$	388.4	73.7	105.3	-	-	416.3	142.1	-	157.6	148.7	195.3	0.1963	0.7615	-0.3090	600K <sup>33</sup>
$Mo(Si,Al)_2$	384.1	73.2	105.1	-	-	410.3	140.5	-	155.6	146.8	193.5	0.1973	0.7585	-0.3044	700K <sup>55</sup>
Mo(Si,Al) <sub>2</sub>	379.8	73.4	104.3	-	-	405.9	138.6	-	153.1	144.7	191.7	0.1984	0.7549	-0.2973	800K <sup>55</sup>
Mo(Si Al)	375.5	73.6	106.5	_	-	403.2	136.7	-	151.2	142.5	191.4	0.2018	0.7445	-0.2815	900K <sup>55</sup>
$M_0(Si Al)$	371.3	73.5	106.5	_	_	308.8	135.0	_	1/0 3	140.6	180.0	0.2032	0.7401	-0.2745	10001255
$M_{-}(S; A)$	266 4	73.5	100.5	-	-	202.0	122.0	-	146.7	120.0	109.9	0.2032	0.7401	-0.27+5	110001
$MO(S1,A1)_2$	300.4	75.0	106.5	-	-	393.9	132.9	-	140.7	138.3	188.1	0.2047	0.7353	-0.2000	1100K <sup>55</sup>
$Mo(S1,AI)_2$	361.1	71.9	105.1	-	-	385.6	130.7	-	144.8	136.0	185.3	0.2051	0.7342	-0.2658	1200K <sup>33</sup>
$TiO_2$	646	250	229	283	475	635	148	203	246	180	362	0.2869	0.4968	0.1520	Calc <sup>56</sup>
$ZrO_2$	619	176	210	224	450	632	107	178	174	160	320	0.2858	0.4998	0.1573	Calc <sup>56</sup>
HfO	664	193	236	235	575	640	137	185	165	176	355	0.2873	0.4958	0.1660	Calc <sup>56</sup>
FaB	502	185	160	136	773	574	271	102	221	230	315	0.2075	0.7206	0.2211	Cale <sup>57</sup>
TeD <sub>2</sub>	100	165	100	150	725	J74 451	2/1	150	221	230	270	0.2000	0.7290	-0.2211	
FeB <sub>4</sub>	409	101	101	152	/68	451	216	154	222	189	278	0.2226	0.6807	-0.1416	Calc
VB	560	126	130	130	559	572	248	248	188	223	274	0.1800	0.8135	-0.3630	Calc <sup>31</sup>
NbB	513	119	148	148	513	505	219	219	158	192	262	0.2058	0.7321	-0.2300	Calc <sup>51</sup>
TaB	545	117	169	169	545	518	222	222	163	196	280	0.2155	0.7023	-0.1811	Calc <sup>51</sup>
VER	616	83	134	140	634	477	224	265	234	234	270	0 1646	0 8641	-0.4513	Calc <sup>51</sup>
Nh D	525	117	169	157	527	152	221	205	104	201	267	0.1077	0.7574	0.1515	Calo <sup>51</sup>
INU5D6	555	11/	100	157	557	432	227	245	194	202	207	0.1977	0.7574	-0.2793	
$1a_5B_6$	552	139	167	164	563	484	227	233	194	205	282	0.2078	0./15/	-0.21/6	Calc <sup>51</sup>
$V_3B_4$	475	135	135	90	636	626	235	263	229	235	272	0.1644	0.8647	-0.4501	Calc <sup>31</sup>
$Nb_3B_4$	521	123	155	133	549	553	222	220	217	212	272	0.1899	0.7817	-0.3045	Calc <sup>51</sup>
$Ta_3B_4$	531	135	167	156	559	557	209	211	214	206	285	0.2086	0.7232	-0.2061	Calc <sup>51</sup>
$V_2B_2$	484	128	129	98	642	639	254	248	229	239	274	0.1621	0.8721	-0.4582	Calc <sup>51</sup>
Nb <sub>2</sub> B <sub>2</sub>	400	148	162	106	574	591	218	240	238	221	277	0.1851	0 7971	-0.3368	Calc <sup>51</sup>
$T_0 B$	517	162	161	137	582	603	210	210	230	217	201	0.1001	0.7/12	0.2430	Cale <sup>51</sup>
$1a_2D_3$	J17 411	102	101	157	502	410	211	106	233	217	291	0.2019	0.7442	-0.2439	
T1B	411	91	107	61	524	410	189	186	193	185	206	0.1552	0.8953	-0.4992	Calc <sup>30</sup>
$Nb_6Sn_5$	266.5	83	90.4	110.6	228.2	410	210.4	65.5	62.9	54	141	0.3304	0.3824	0.3081	Calc <sup>18</sup>
$NbSn_2$	180.8	77.3	68.9	60.1	178.5	188.3	52.5	37.3	57.4	51	107	0.2924	0.4818	0.1847	Calc <sup>18</sup>
ZrAl	142.87	64.66	92.6	49.26	217.32	193.33	70.28	116.67	62.22	68	107	0.2388	0.6325	-0.1331	Calc <sup>20</sup>
Zr <sub>2</sub> Al <sub>3</sub>	226.06	46.84	48.31	67.91	203.50	203.01	74.73	76.07	56.91	72	107	0.2240	0.6766	-0.1397	Calc <sup>20</sup>
Pd <b>Z</b> r	169.6	108.1	134.7	126.7	230.4	229.5	70.6	67.5	16.6	42	149	0 3714	0.2813	0 4797	Calc <sup>21</sup>
Ti0 25Mo0 75	363.6	151.5	151.7	120.7	250.1	227.5	62	07.5	10.0	76.0	222.2	0.3/17	0.2015	0.1727 0.4028(207)	Cale <sup>59</sup>
TI0.25W100.75	303.0	131.5	-	-	-	-	10.4	-	-	10.9	170.4	0.3447	0.3403	0.4026(207)	
110.5M00.5	224.0	146.6	-	-	-	-	10.4	-	-	18.2	172.4	0.4490	0.1056	0.7900(52.8)	Calc
T10.75Mo0.25	160.5	125.6	-	-	-	-	34.1	-	-	26.0	137.2	0.4107	0.1899	0.6667(73.5)	Calc <sup>39</sup>
Ti0.25Nb0.75	203.5	126.8	-	-	-	-	21.3	-	-	27.0	152.4	0.4163	0.1773	0.6924(76.5)	Calc <sup>59</sup>
Ti0.5Nb0.5	155.4	124.7	-	-	-	-	12.8	-	-	13.8	134.9	0.4507	0.1020	0.8293(39.9)	Calc <sup>59</sup>
Ti0.75Nb0.25	128.5	115.5	-	-	-	-	14.9	-	-	10.7	119.8	0.4567	0.0891	0.8395(31.1)	Calc <sup>59</sup>
Ti0 25Ta0 75	207.0	145.3	_	_	_	_	55.6	_	_	43.9	165.9	0 3784	0 2646	0.5408(121.0)	Calc <sup>59</sup>
T:0 5T-0 5	162.4	122.0	_	_	-	-	20.0	_	_	72.9	142.0	0.3704	0.2040	0.5400(121.0)	Cala <sup>59</sup>
TIU.3 Ta0.3	105.4	132.0	-	-	-	-	39.0	-	-	20.0	145.0	0.4110	0.10/4	0.0339(73.7)	
Ti0.75Ta0.25	129.9	121.6	-	-	-	-	38.6	-	-	16.9	124.4	0.4351	0.1357	0.6674(48.4)	Calc <sup>55</sup>
Ti0.25V0.75	213.0	132.2	-	-	-	-	29.6	-	-	33.5	159.1	0.4016	0.2107	0.6447(93.9)	Calc <sup>59</sup>
Ti0.5V0.5	169.6	122.3	-	-	-	-	33.6	-	-	29.2	138.1	0.4012	0.2114	0.6424(81.8)	Calc <sup>59</sup>
Ti0.75V0.25	123.9	116.9	-	-	-	-	36.3	-	-	15.4	119.2	0.4380	0.1293	0.6760(44.3)	Calc59
Ti0 25W0 75	374.8	184.2	_	_	-	_	817	_	_	86.9	247 7	0 3430	0 3508	0.4138(233.4)	Calc <sup>59</sup>
T:0 5W0 5	220.0	161.2					50.0			11.0	100 6	0.2010	0.2251	0.6025(124.6)	Cala <sup>59</sup>
TI0.5 W 0.5	239.9	105.9	-	-	-	-	50.9	-	-	44.0	190.0	0.3910	0.2551	0.0055(124.0)	
Ti0.75W0.25	169.2	134.2	-	-	-	-	32.4	-	-	25.3	145.9	0.4180	0.1735	0.6979(71.8)	Calc <sup>55</sup>
Zr0.25Mo0.75	342.4	134.5	-	-	-	-	49.7	-	-	67.1	203.8	0.3516	0.3293	0.4161(181.4)	Calc <sup>59</sup>
Zr0.5Mo0.5	208.5	124.3	-	-	-	-	29.2	-	-	33.8	152.4	0.3967	0.2220	0.6242(94.5)	Calc <sup>59</sup>
Zr0.75Mo0.25	138.4	104.2	-	-	-	-	16.6	-	-	16.8	137.2	0.4307	0.1453	0.7578(48.1)	Calc59
Zr0 25Nb0 75	196.2	118 5	_	_	_	_	179	_	_	24.6	144 4	0.4195	0 1700	0.6967(69.7)	Calc <sup>59</sup>
Z=0.5Nb0.5	144.4	100.0					10.2			10 2	120.2	0.4290	0.1512	0.0007(00.1)	Cala <sup>59</sup>
ZIU.JINUU.J	144.4	108.5	-	-	-	-	10.5	-	-	10.2	120.5	0.4200	0.1312	0.7479(32.0)	
Zr0./5Nb0.25	112.8	98.3	-	-	-	-	19.8	-	-	13.2	103.1	0.4384	0.1284	0.7612(38.1)	Calc
Ag	120.5	92.0	-	-	-	-	44.6	-	-	28	101.5	0.3726	0.2785	0.4670	400K <sup>60</sup>
Ag	117.0	90.0	-	-	-	-	42.6	-	-	26	99	0.3753	0.2719	0.4788	500K <sup>60</sup>
Ag	113.5	88.0	-	-	-	-	40.7	-	-	25.6	96.5	0.3781	0.2653	0.4902	600K <sup>60</sup>
Aø	110.0	86.0	-	-	-	-	38.8	-	_	24	94	0.3811	0.2584	0.5021	700K <sup>60</sup>
Δσ	106.5	84 5	_	_	_	_	36.0	_	_	227	91.8	0 3855	0.2480	0 5183	800K <sub>60</sub>
115	100.5	160 5	-	-	-	-	JU.9 41 0	-	-	22.1	100.0	0.3033	0.1500	0.5105	4001×60
Au	107	100.5	-	-	-	-	41.0	-	-	20.8	199.9	0.4250	0.1580	0.7029	400K <sup>60</sup>
Au	185	158	-	-	-	-	39.7	-	-	25.8	167	0.4266	0.1544	0.7084	500K00
Au	182	155.5	-	-	-	-	38.3	-	-	25.0	164.3	0.4275	0.1524	0.7132	600K <sup>60</sup>
Au	178.5	153	-	-	-	-	36.9	-	-	24.1	161.5	0.4289	0.1493	0.7189	700K <sup>60</sup>
Au	175.5	150.5	-	-	-	-	35.5	-	-	23.4	158.8	0.4299	0.1472	0.7240	$800K^{60}$

TABLE VII: The elastic properties (in GPa) of actinide and lanthanide intermetallic compounds, as well as experimental results.

	C <sub>11</sub>	C <sub>12</sub>	C <sub>13</sub>	C <sub>23</sub>	C <sub>22</sub>	C <sub>33</sub>	C <sub>44</sub>	C <sub>55</sub>	C <sub>66</sub>	G	В	ν	G/B	Cauchy Pressure/B	Note
Pu-1at%Ga	36.28	26.73	-	-	-	-	33.59	-	-	22.1	29.9	0.2039	0.7378	-0.2293	Expt <sup>61</sup>
α-U	215	46	22	108	199	267	124	73	74	84	113	0.2019	0.7441	-0.2799	Expt <sup>62</sup>
α-U	299	59	30	144	231	364	100	150	132	114	149	0.1933	0.7711	0.3343	Calc <sup>62</sup>
<i>β</i> -U	220	107	79	-	-	201	65	-	36	57	130	0.3090	0.4378	0.3271	Calc <sup>62</sup>
$\alpha$ -UH <sub>3</sub>	217	37	-	-	-	-	65	-	-	74	97	0.1957	0.7635	-0.2887	0GPa <sup>63</sup>
$\alpha$ -UH <sub>3</sub>	240	42	-	-	-	-	70	-	-	80	108	0.2016	0.7449	-0.2593	5GPa <sup>63</sup>
$\alpha$ -UH <sub>3</sub>	260	45	-	-	-	-	66	-	-	80	117	0.2200	0.6885	-0.1800	10GPa <sup>63</sup>
$\alpha$ -UH <sub>3</sub>	274	46	-	-	-	-	60	-	-	78	122	0.2370	0.6378	-0.1148	15GPa <sup>63</sup>
$\alpha$ -UH <sub>2</sub>	297	61	-	-	-	_	60	-	-	79	140	0.2622	0.5652	-0.0072	20GPa <sup>63</sup>
$\alpha$ -UH <sub>2</sub>	213	50	-	-	-	_	48	-	-	59	104	0.2607	0.5695	-0.0192	GGA <sup>64</sup>
$\alpha$ -UH <sub>2</sub>	216	57	_	_	_	-	50	-	-	60	110	0.2684	0.5478	0.0636	LDA <sup>64</sup>
$\alpha$ -UH <sub>2</sub>	221	63	_	_	_	-	53	-	-	62	116	0.2719	0.5379	0.0865	LDA+U <sup>64</sup>
B-UH <sub>2</sub>	201	92	_	_	_	-	57	-	-	56	128	0.3096	0.4363	0.2727	LDA <sup>64</sup>
B-UH	201	70	_	_	_	_	58	-	_	65	121	0.2727	0.5356	0.0994	LDA+U <sup>64</sup>
B-UH	222	102	_	_	_	_	60	-	_	61	144	0.3141	0.2225	0.2923	GGA <sup>64</sup>
UN	423.9	98.1	_	_	_	_	75.7	_	_	103	207	0.2855	0.1213	0.1084	Exnt <sup>65</sup>
	381	113	_	_	_	_	54.6	_	_	79	207	0.2000	0.3004	0.1004	AFM-SOC <sup>66</sup>
UN.	405 A	137.3	-	-	-	-	54.0 65.6	-	-	00	257	0.3275	0.3902	0.2000	GG 167
	493.4	137.5	-	-	-	-	55.3	-	-	22 80	257	0.3283	0.3074	0.2793	$GGA + U2^{67}$
	400.2	140.5	-	-	-	-	41.2	-	-	76	250	0.3430	0.3480	0.3438	$CCA + U4^{67}$
	403.0	140.2	-	-	-	-	41.5	-	-	/0	200	0.3007	0.2927	0.4034	GGA+04
$UO_2$	269.5	110./	-	-	-	-	39.7	-	-	00	209	0.3238	0.3993	0.2824	Expt <sup>1</sup>
$UO_2$	309.4	112.5	-	-	-	-	01.7	-	-	83	198	0.3139	0.4190	0.2304	GGA
$UO_2$	343.1	121.3	-	-	-	-	62.7	-	-	/9	195	0.3218	0.4043	0.3001	GGA+U <sup>00</sup>
$UO_2$	440.6	141.3	-	-	-	-	88.1	-	-	109	241	0.3034	0.4525	0.2207	LDA <sup>00</sup>
$UO_2$	382.3	136.5	-	-	-	-	64.5	-	-	84	218	0.3300	0.3834	0.3269	LDA+U <sup>08</sup>
$UO_2$	386.4	118.0	-	-	-	-	63.9	-	-	86.4	207	0.3171	0.4166	0.2608	R109
$UO_2$	317.9	118.3	-	-	-	-	59.8	-	-	73.5	184.8	0.3244	0.3977	0.3165	1200K <sup>69</sup>
$UO_2$	253.9	96.2	-	-	-	-	49.6	-	-	59.8	148.8	0.3228	0.4018	0.3132	2060K <sup>69</sup>
$UO_2$	233.3	80.4	-	-	-	-	48.2	-	-	58.0	131.4	0.3075	0.4417	0.2451	2250K <sup>69</sup>
$UO_2$	219.5	90.7	-	-	-	-	43.0	-	-	50.6	133.6	0.3320	0.3785	0.3569	2370K <sup>69</sup>
$UO_2$	217.3	97.2	-	-	-	-	43.0	-	-	49.2	137.2	0.3399	0.3583	0.3949	2460K <sup>69</sup>
$UO_2$	212.8	92.6	-	-	-	-	40.7	-	-	47.6	132.7	0.3398	0.3588	0.3912	2580K <sup>69</sup>
$UO_2$	196.7	94.5	-	-	-	-	36.4	-	-	41.7	128.6	0.3536	0.3244	0.4519	2670K <sup>69</sup>
$UO_2$	178.3	93.6	-	-	-	-	32.7	-	-	36.3	121.8	0.3646	0.2977	0.4999	2760K <sup>69</sup>
$UO_2$	146.1	78.7	-	-	-	-	27.5	-	-	29.8	88.5	0.3485	0.3371	0.5786	2930K <sup>69</sup>
UC	315	77	-	-	-	-	61	-	-	80	156	0.2815	0.5116	0.1023	Expt <sup>70</sup>
UC	315	136	-	-	-	-	72	-	-	79	196	0.3230	0.4015	0.3271	GGA+U3 <sup>70</sup>
$UC_2$	292	154	58	-	-	512	46	-	143	87	180	0.2927	0.4812	0.0637	GGA+U3 <sup>71</sup>
$U_2C_3$	383	121	-	-	-	-	91	-	-	105	208	0.2837	0.5056	0.1440	GGA+U3 <sup>71</sup>
$UB_2$	450.4	58.6	102.3	-	-	497.2	262.6	-	195.9	217	213	0.1197	1.0188	-0.6986	This work
$UB_4$	558.4	118.9	80.9	-	-	569.1	223	-	226.4	228	250	0.1500	0.9130	-0.4998	This work
$UB_{12}$	488.9	118.1	-	-	-	-	254.1	-	-	224	242	0.1460	0.9267	-0.5628	This work(0GPa)
$UB_{12}$	673.1	212.2	-	-	-	-	329.3	-	-	285	366	0.1904	0.7802	-0.3201	This work(50GPa)
$UB_{12}$	807.8	295.1	-	-	-	-	392.1	-	-	331	466	0.2131	0.7096	-0.2081	This work(100GPa)
$U_2Ti$	293.6	81	28.2	-	-	310	133.9	-	106.3	124	130	0.1375	0.9562	-0.5037	This work
$U_2Ti$	285	74	28	-	-	300	129	-	105.5	121	125	0.1346	0.9661	-0.5282	Calc <sup>72</sup>
U <sub>2</sub> Ti	295.1	89.4	30.1	-	-	310.8	128	-	102.9	120	133	0.1520	0.9063	-0.4182	Calc <sup>72</sup>
U <sub>2</sub> Ti	464.3	189.3	71.4	-	-	489.3	167.9	-	137.5	164	231	0.2121	0.7125	0.0969	20GPa <sup>72</sup>
U <sub>2</sub> Ti	603.6	285.7	117.9	-	-	657.1	200	-	159.0	197	322	0.2465	0.6101	0.0692	40GPa <sup>72</sup>
U <sub>2</sub> Ti	664.3	332.1	139.3	-	-	732.1	214.3	-	166.1	210	364	0.2583	0.5764	0.1251	50GPa <sup>72</sup>
U <sub>2</sub> Ti	928.6	571.4	246.4	-	-	1150	128	-	178.6	195	570	0.3468	0.3412	0.4483	100GPa <sup>72</sup>
NpN	402	140	-	-	-	_	38.4	-	_	64	227	0.3704	0.2837	0.4469	NM <sup>66</sup>
NnN	331	54.2	_	_	_	-	79.1	-	-	99	140	0.2129	0.7100	0.1783	FM <sup>66</sup>
NnN	341	97.7	_	_	_	-	60.8	-	-	81	170	0.2957	0.4731	0.2167	AFM <sup>66</sup>
NnN	359	112	_	_	_	-	50.4	-	-	73	194	0 3334	0 3748	0.3170	NM-SOC <sup>66</sup>
NnN	330	86.4	_	_	_	_	60.7	-	_	81	168	0.2929	0.4805	0.1533	FM-SOC <sup>66</sup>
NnN	330	94.2	_	_	_	_	61.8	_	_	82	176	0.2921	0.4639	0.1843	AFM-SOC <sup>66</sup>
PuN	280	89.6					66.2		_	7/	1/0	0.2991	0.5013	0.1596	AFM-SOC <sup>66</sup>
Ce	280	17	-	-	-	-	15	-	-	11.2	21	0.2052	0.5015	0.1590	Cale <sup>73</sup>
Ce	20	26.4	-	-	-	-	20.0	-	-	11.2	20.2	0.2703	0.3419	0.0908	Cale <sup>73</sup>
	51.9 01	∠0.4 50	-	-	-	-	20.9 27	-	-	14.0	50.2	0.2091	0.4908	0.1019	Calc <sup>73</sup>
$CeH_2 - CaF_2$	84 07 (	52 55	-	-	-	-	27	-	-	21.9	02.7	0.3436	0.3493	0.3989	
$CeH_2 - CaF_2$	ð/.0	22	-	-	-	-	5/	-	-	20.0	03.9	0.3219	0.4043	0.2733	Expt <sup>73</sup>
$CeH_2 - FeS_2$	118	31	-	-	-	-	33	-	-	30.9	51.0	0.2450	0.0144	-0.0555	$Calc'^3$
$CeH_2 - AIB_2$	90	21	53	-	-	51.55	33	-	-	23.6	51.0	0.2992	0.4635	0.1128	
$CeH_2 - ReB_2$	114	41	18	-	-	56.11	12	-	-	50.4	56.0	0.2705	0.5418	0.0937	Calc <sup>73</sup>
$CeH_3 - BiF_3$	96	35	-	-	-	-	19	-	-	23.0	55.3	0.3175	0.4154	0.2892	Calc' <sup>3</sup>
$CeH_3$ -ReO <sub>3</sub>	71	49	-	-	-	-	9	-	-	9.8	56.3	0.4181	0.1731	0.7101	Cale's
$CeH_3 - P-3C1$	89	20.8	21	-	-	104	23	-	-	30.6	45.2	0.2289	0.6619	-0.1693	Calc <sup>13</sup>

	C <sub>11</sub>	C <sub>12</sub>	C <sub>13</sub>	C <sub>23</sub>	C <sub>22</sub>	C <sub>33</sub>	C <sub>44</sub>	C55	C <sub>66</sub>	G	В	ν	G/B	Cauchy Pressure/B	Note
ZrB <sub>12</sub>	443	129	-	-	-	-	265	-	-	215	234	0.1482	0.9193	-0.5820	Expt <sup>74</sup>
$ZrB_{12}$	437.9	146.3	-	-	-	-	256.2	-	-	204	244	0.1721	0.8392	-0.4513	0GPa <sup>74</sup>
$ZrB_{12}$	483.6	174.8	-	-	-	-	275	-	-	218	278	0.1888	0.7855	-0.3608	10Gpa <sup>74</sup>
$ZrB_{12}$	527.6	203.6	-	-	-	-	291.4	-	-	230	312	0.2036	0.7389	-0.2818	20GPaCalc <sup>74</sup>
$ZrB_{12}$	611.5	322.1	-	-	-	-	258.8	-	-	253	376	0.2255	0.6720	-0.1682	40GPaCalc <sup>74</sup>
$ZrB_{12}$	651.7	285.0	-	-	-	-	335.3	-	-	263	407	0.2341	0.6462	-0.1235	50GPaCalc <sup>74</sup>
$HfB_{12}$	436.4	156.1	-	-	-	-	250.8	-	-	199	250	0.1855	0.7958	-0.3795	0GPaCalc <sup>74</sup>
$HfB_{12}$	483.1	185.8	-	-	-	-	267.6	-	-	211	285	0.2026	0.7419	-0.2871	10GPaCalc <sup>74</sup>
$HfB_{12}$	530.1	213.9	-	-	-	-	285.1	-	-	225	315	0.2146	0.7048	-0.2230	20GPaCalc <sup>74</sup>
$HfB_{12}$	618.5	270.4	-	-	-	-	315.4	-	-	248	386	0.2353	0.6430	-0.1164	40GPaCalc <sup>74</sup>
$HfB_{12}$	661.4	296.4	-	-	-	-	328.1	-	-	259	418	0.2430	0.6202	-0.0758	50GPaCalc <sup>74</sup>
$LuB_{12}$	460.4	114.7	-	-	-	-	248	-	-	215	230	0.1441	0.9333	-0.5797	0GPaCalc <sup>74</sup>
$LuB_{12}$	504.8	138.4	-	-	-	-	268.5	-	-	230	261	0.1585	0.8842	-0.4994	10GPaCalc <sup>74</sup>
$LuB_{12}$	554.3	167.0	-	-	-	-	284.4	-	-	244	296	0.1770	0.8234	-0.3965	20GPaCalc <sup>74</sup>
$LuB_{12}$	638.9	219.0	-	-	-	-	316	-	-	268	359	0.2009	0.7472	-0.2702	40GPaCalc <sup>74</sup>
$LuB_{12}$	679.3	243.1	-	-	-	-	328.1	-	-	279	389	0.2107	0.7170	-0.2188	50GPaCalc <sup>74</sup>
$YB_{12}$	464.3	107.4	-	-	-	-	252	-	-	219	226	0.1337	0.9695	-0.6388	0GPaCalc <sup>74</sup>
$YB_{12}$	513.1	135.2	-	-	-	-	270.4	-	-	234	266	0.1600	0.8792	-0.5075	10GPaCalc74
$YB_{12}^{12}$	559.3	161.5	-	-	-	-	287.8	-	-	248	294	0.1707	0.8439	-0.4294	20GPaCalc <sup>74</sup>
$YB_{12}$	646	214.5	-	-	-	_	287.8	-	-	272	358	0.1972	0.7587	-0.2869	40GPaCalc <sup>74</sup>
$YB_{12}$	686.9	241.1	-	-	-	_	330.9	-	-	282	390	0.2081	0.7247	-0.2304	50GPaCalc <sup>74</sup>
$\gamma$ -TiAl	186.6	75.0	75.0	-	-	182.9	108.8	_	81.2	78.3	111.8	0.2162	0.7001	-0.1789	0K <sup>75</sup>
$\gamma$ -TiAl	182.8	75.2	75.0	-	-	176.9	103.5	-	81.2	74.5	110.3	0.2243	0.6756	-0.1351	298K <sup>75</sup>
$\gamma$ -TiAl	179.7	75.3	75.3	-	-	173.7	100.5	-	74.4	72.3	109.4	0.2293	0.6608	-0.1110	443K <sup>75</sup>
$\gamma$ -TiAl	178.0	75.6	75.5	-	-	172.1	99.0	-	73 3	71.1	109.0	0.2321	0.6523	-0.0972	523K <sup>75</sup>
$\gamma$ -TiAl	172.5	75.2	75.7	-	-	167.3	94.8	-	70.6	67.9	107.3	0.2387	0.6329	-0.0676	723K <sup>75</sup>
$\gamma$ -TiAl	150.3	76.0	76.0	_	_	152.6	81.6	-	63.8	56.9	107.5	0.2507	0.5638	0.0327	1273K <sup>75</sup>
S-ZnO	189.8	102.2	93.7	_	_	192.0	45.2	-	43.8	46.0	128.7	0.2027	0.3576	0.4155	
S-ZnO	190	110	90	_	_	196	30	_	40	42.3	120.7	0.3516	0.3293	0.4713	Expt <sup>76</sup>
V <sup>0</sup> -1	182.0	96.8	827	_	_	192.8	44 5	-	42.6	45.7	120.1	0.3311	0.3200	0.3846	Calc <sup>76</sup>
$V^{+2}-1$	180.7	112.1	97.5	_	_	192.0	35.9	-	34.3	37.4	120.1	0.3686	0.2879	0.5371	Calc <sup>76</sup>
$V_0^{0}$	169.7	88.0	873	_	_	163.5	38.3	_	40.6	39.4	114 1	0.3452	0.5638	0.4224	Calc <sup>76</sup>
$P_0^2$	682	188	131	_	_	1118	290	_	247	294.1	369.6	0.1855	0.7958	-0 2949	Calc <sup>77</sup>
0.32B.	629	167	135	_	_	1006	256	_	231	269.4	342.8	0.1887	0.7950	-0 2844	Calc <sup>77</sup>
0.52By	596	167	182	_	_	922	200	_	214	236.0	346.0	0.1007	0.6821	-0.1329	Calc <sup>77</sup>
$1.30B_V$	543	170	226	_	_	667	195	_	186	190.2	329.9	0.2582	0.5766	0.0227	Calc <sup>77</sup>
HA	137.2	44 5	57.8	_	_	164.8	42.3	_	46 35	44 7	83.7	0.2502	0.5700	0.0227	Calc <sup>78</sup>
НΔ	137	42.5	54.9	_	_	172	39.6	_	47 25	44.6	82.6	0.2731	0.5397	0.0639	Expt <sup>78</sup>
$HA-V_{H}$	129.0	27.6	69.5	_	_	158.6	47.8	-	50.7	44.8	80.4	0.2713	0.5578	-0.0087	Calc <sup>78</sup>
$H_{A}$	113.7	43.5	47 1	_	_	163.9	30.0	_	35.1	39.5	72.9	0.2010	0.5370	0.1069	Calc <sup>78</sup>
HA-Vou	109.0	28.4	62.7	-	-	160.1	42.1	-	40.3	39.2	72.3	0.2701	0.5429	0.0602	Calc <sup>78</sup>
$HA-V^{2+}$	116.2	53.4	40.7	-	-	156.0	31.7	-	31.4	35.1	72.9	0.2925	0.4816	0.2128	Calc <sup>78</sup>
HA- $V^{2+}$	77.0	21.9	70.4	-	-	1191	34.1	-	27 55	26.5	66.5	0.3241	0 3984	0.4609	Calc <sup>78</sup>
Ni Ca2	246 58	147.24	-	_	_	-	124.97	_	-	94.85	180.35	0.2763	0.5259	0.1235	MD <sup>79</sup>
Ni_1at%H	246.50	148.04	_	_	_	_	127.57	_	_	93.28	180.95	0.2703	0.5255	0.1200	MD <sup>79</sup>
Ni_2at%H	246.93	148.81	_	_	_	_	122.50		_	91 74	181.52	0.2800	0.5155	0.1576	MD <sup>79</sup>
Ni-3at%H	240.93	140.01	_	_	_	_	117.83		_	90.21	182.09	0.2027	0.3002	0.1743	MD <sup>79</sup>
Ni_Aat%H	247.13	150.34					115.46			88.67	182.67	0.2074	0.4954	0.1745	MD <sup>79</sup>
Ni-5at%H	247.55	151.1	_	-	-	-	113.40	-	-	87.15	182.07	0.2911	0.4054	0.1909	MD <sup>79</sup>
	277.55	101	- 98.9	-	-	105	65	_	-	56.5	130.24	0.2247	0.5011	0.2074	Expt <sup>80</sup>
RaTiO	233	107	11/	-	-	160	56.2	-	104	58.2	130.2	0.2055	0.3011	0.1202	Expt Expt <sup>80</sup>
	176 1	86.9	68 3	-	-	190 5	50.2 50.8	-	44.6	50.2	100 0	0.3132	0.4562	0.1370	4K <sup>81</sup>
Ti	162 /	92 N	60.J	-	-	180.7	26.0 26.7	_	35.0	13 A	107.3	0.3020	0.4042	0.2687	208K <sup>81</sup>
Ti	152.4	92.0	60 5	-	-	172 /	43.7	-	28.5 28.5	79.4 38 7	107.3	0.3219	0.4042	0.3007	273K <sup>81</sup>
Ti	120.0	00.7	68.9	-	-	157.4	73. <del>1</del> 32.7	-	20.J	26.1	08.0	0.3373	0.3044	0.5145	073K <sup>81</sup>
Ti	129.9 07 7	99.2 87 7	00.0	-	-	157.0	37.5	-	25.4	20.1 87 7	137.0	0.3700	0.2057	0.5154	1273 K <sup>82</sup>
11	//./	04.1	-	-	-	-	J1)	-	<u></u>		1.77.7	V	1.4700	V/	$i \leftarrow i \downarrow i \downarrow i \downarrow$

TABLE VIII: The elastic properties (in GPa) of some intermetallic compounds under the pressure and temperature, as well as experimental results.

TABLE IX: The elastic properties (in GPa) of potential structural materials for nuclear reactors, as well as experimental results.

	C <sub>11</sub>	C <sub>12</sub>	C <sub>13</sub>	C <sub>33</sub>	C <sub>44</sub>	C <sub>66</sub>	G	В	ν	G/B	Cauchy Pressure/B	Note
ZrC	470	100			160	-	170	223	0.1970	0.7593	-0.2687	Expt <sup>83</sup>
SiC	390	142			256	-	191	225	0.1683	0.8518	-0.5074	Expt <sup>14</sup>
SiC	420	126			287	-	219	224	0.1308	0.9795	-0.7188	Expt <sup>13</sup>
T <sub>12</sub> SC	-	-	-	-	-	-	125	145	0.16	-	-	Expt <sup>o+</sup>
$\alpha$ -11 <sub>3</sub> S1C <sub>2</sub>	360	84 86	101	330 249	158	1380	142	182	0.1910	0.7762	-0.3054	FLAPW <sup>05</sup>
$p = 11_3 \text{ SIC}_2$ Fe=19Cr=10Ni	204.6	137.7	- 09	540	126.2	1370	801	160	0.2077	0.7202	-0.2312	Expt <sup>86</sup>
Fe-12Cr-12Ni	210.9	140.3	-	-	120.2	-	88	164	0.2032	0.5349	0.1086	Expt <sup>86</sup>
Fe-12Cr-18Ni	233.2	162.7	_	-	122.5	_	88	168	0.2750	0.5549	0.2153	Expt <sup>86</sup>
Fe-18Cr-8Ni	209	133.0	-	-	121	-	88	153	0.2595	0.5727	0.0758	Expt <sup>87</sup>
Fe-18Cr-12Ni	191.2	117.9	-	-	138.6	-	98	142	0.2204	0.6874	-0.1454	Expt <sup>86</sup>
Fe-18Cr-12Ni	215.9	144.6	-	-	128.9	-	89.1	160	0.2652	0.5569	0.0719	Expt <sup>86</sup>
Fe-18Cr-14Ni	198	125	-	-	122	-	88	149.3	0.2542	0.5881	0.0201	Expt <sup>86</sup>
Fe-18Cr-19Ni	191	119	-	-	124	-	89	143	0.2428	0.6210	-0.0350	Expt <sup>86</sup>
Fe-19Cr-10Ni	207	132	-	-	123	-	89.1	157	0.2621	0.5656	0.0573	Expt <sup>86</sup>
Fe-19Cr-14Ni	205	133	-	-	127	-	91	157	0.2580	0.5771	0.0382	Expt <sup>86</sup>
Fe-19Cr-19Ni	204	133	-	-	126	-	89	156.7	0.2594	0.5731	0.0447	Expt <sup>86</sup>
Fe-19Cr-24Ni	215.2	144.0	-	-	125.8	-	90	168	0.2730	0.5350	0.1085	Expt <sup>87</sup>
Fe	276	173.5	-	-	136.3	-	102	208	0.2885	0.4924	0.1719	Expt <sup>oo</sup>
Co	239.8	163.4	-	-	133.4	-	95	189	0.2841	0.5045	0.1588	Expt <sup>86</sup>
INI Ea 15Cr 15Ni	251.0	134.4	-	-	122.0	-	93	167	0.28/3	0.4957	0.1/34	Expl <sup>00</sup>
Fe-15Cr-15Ni	213.0	137	-	-	130	-	97.2	163	0.2515	0.5905	0.0001	200K <sup>87</sup>
Fe-15Cr-15Ni	214.9	137	-	-	134	-	90.0	163	0.2520	0.5920	0.0123	200K 220K <sup>87</sup>
Fe-15Cr-15Ni	214.7	137	_	-	133	_	95.3	162.8	0.2551	0.5005	0.0104	220K 230K <sup>87</sup>
Fe-15Cr-15Ni	213.1	137	_	-	133	-	95.0	162.4	0.2552	0.5853	0.0246	240K <sup>87</sup>
Fe-15Cr-15Ni	213.2	137	-	-	132	-	94.4	162.4	0.2565	0.5813	0.0308	250K <sup>87</sup>
Fe-15Cr-15Ni	212.6	137	-	-	132	-	94.3	162.2	0.2565	0.5814	0.0308	260K <sup>87</sup>
Fe-15Cr-15Ni	212.1	137	-	-	132	-	94.2	162.0	0.2565	0.5815	0.0309	270K <sup>87</sup>
Fe-15Cr-15Ni	211.8	137	-	-	131	-	93.6	161.9	0.2576	0.5781	0.0371	280K <sup>87</sup>
Fe-15Cr-15Ni	211.4	137	-	-	131	-	93.5	161.8	0.2577	0.5797	0.0371	290K <sup>87</sup>
Fe-15Cr-15Ni	211	137	-	-	130	-	93	162	0.2591	0.5739	0.0433	295K <sup>87</sup>
Ti <sub>2</sub> AlB	196.4	87.1	58.0	209.0	75.3	54.7	67	112	0.2512	0.5963	0.0674	PAW <sup>88</sup>
Zr <sub>2</sub> AlB	176.7	70.0	51.4	175.7	52.0	53.4	55	97	0.2617	0.5667	0.0824	PAW <sup>88</sup>
$Hf_2AIB$	203.8	76.5	58.5	200	67.5	63.7	67	110	0.2469	0.6990	0.0172	PAW <sup>00</sup>
$V_2$ AIB	285.1	85./	9/./	2/8.5	138.8	99.7	101	15/	0.2127	0./108	-0.1/5/	PAW <sup>66</sup> DAW <sup>88</sup>
	205.0	91.4	101.7	249.2	123.5	90.1 114 A	101	175	0.2400	0.0280	-0.0003	PAW <sup>88</sup>
$Cr_2 AlB$	208.8	90.8 81.9	129.8	270.2	140.0	108.5	121	174	0.2249	0.6954	-0.1293	$P\Delta W^{88}$
MonAlB	316.6	105.4	1517	269.0	161.1	105.5	118	191	0.2438	0.6199	-0.0251	PAW <sup>88</sup>
Sc <sub>2</sub> AlC	179.2	65.3	34.2	194.5	45.2	57.0	56	91	0.2447	0.6154	-0.0148	PAW <sup>88</sup>
Ti <sub>2</sub> AlC	304.4	65.4	64.0	269.9	105.7	119.5	112	140	0.1857	0.7953	-0.3412	PAW <sup>88</sup>
$Zr_2AlC$	259.2	64.7	63.3	225.3	85.0	97.3	90	125	0.2093	0.7212	-0.2174	PAW <sup>88</sup>
Hf <sub>2</sub> AlC	291.1	74.5	72.2	255.0	99.2	108.3	102	141	0.2083	0.7243	-0.2150	PAW <sup>88</sup>
V <sub>2</sub> AlC	330.2	74.3	107.1	321.1	149.3	128.0	130	173	0.1991	0.7529	-0.2771	PAW <sup>88</sup>
Nb <sub>2</sub> AlC	318.9	89.4	120.8	296.5	141.2	114.8	118	177	0.2282	0.6639	-0.1291	PAW <sup>88</sup>
Ta <sub>2</sub> AlC	349.0	125.3	132.2	338.2	153.3	111.9	125	202	0.2432	0.6197	-0.0191	PAW <sup>88</sup>
$Cr_2AlC$	369.8	86.1	108.7	362.5	142.9	141.9	139	190	0.2065	0.7298	-0.2370	PAW <sup>88</sup>
Mo <sub>2</sub> AIC	354.4	98.0	146.6	359.0	144.4	128.2	127	205	0.2431	0.6199	-0.0683	PAW <sup>66</sup>
$Sc_2AIN$	210.3	69.6	54.0	217.7	/0.9	/0.4	/3	110	0.2291	0.6613	-0.0802	PAW <sup>88</sup>
$T_{12}AIN$	310.2 269.9	09.7	94.7	291.5	127.9	123.3	120	11/2	0.2012	0.7401	-0.2709	PAW <sup>30</sup> DAW <sup>88</sup>
Hf. AIN	200.0	70.9 84 5	07.2 103.1	245.5	109.1	90.0	90	163	0.2213	0.0842	-0.3034	PAW <sup>88</sup>
VaAIN	301.7	44.8	131.4	331.7	143.1	128.5	121	169	0.2229	0.7175	-0.2820	PAW <sup>88</sup>
Nb <sub>2</sub> AlN	340.4	149.9	110.6	332.3	147.7	95.3	119	195	0.2468	0.6095	0.0449	PAW <sup>88</sup>
Ta <sub>2</sub> AlN	351.9	174.1	142.8	372.5	160.0	88.9	119	222	0.2727	0.5359	0.1533	PAW <sup>88</sup>
$Cr_2AlN$	286.7	74.9	144.5	376.7	88.2	105.9	95	181	0.2764	0.5256	0.0599	PAW <sup>88</sup>
Ti <sub>3</sub> AlC <sub>2</sub>	368	81	76	313	130	143	135	168	0.1833	0.8029	-0.3456	PAW <sup>89</sup>
$Zr_3AlC_2$	322	73	75	270	106	124	113	151	0.2003	0.7490	-0.3385	PAW <sup>89</sup>
$Hf_3AlC_2$	357	82	83	283	126	138	127	165	0.1930	0.7722	-0.3000	PAW <sup>89</sup>
$V_3AlC_2$	415	88	113	361	163	163	156	202	0.1936	0.7701	-0.3094	PAW <sup>89</sup>
Nb <sub>3</sub> AlC <sub>2</sub>	331	131	126	321	137	100	113	194	0.2556	0.5839	0.0515	PAW <sup>89</sup>
$Ta_3AlC_2$	417	118	187	351	177	150	147	241	0.2466	0.6099	-0.0456	PAW <sup>89</sup>
$Cr_3AlC_2$	381	100	136	381	118	141	117	209	0.2649	0.5582	0.0258	PAW <sup>89</sup>
$Mo_3AlC_2$	370	159	140	361	121	105	113	220	0.2800	0.5155	0.1661	PAW <sup>89</sup>
$W_3AIC_2$	392 246	181	1/7	389 250	121	106	112	249 196	0.3047	0.4490	0.2628	PAW °7
$T_3 SIC_2$	300 357	94 04	07	332 322	133	130	141 122	100	0.19/0	0.7374	-0.2337	GGA <sup>90</sup>
$Ti_3 OC_2$	346	94 Q2	27 8∆	313	143	132	133	162	0.2048	0.7330	-0.2250	$GG^{490}$
Ti <sub>2</sub> GeC	279	99	95	283	125	90	104	158	0.2306	0.6569	-0.0666	LDA <sup>91</sup>

TABLE X: The elastic properties (in GPa) of potential structural materials for nuclear reactors, as well as experimental results(continued).

	C <sub>11</sub>	C <sub>12</sub>	$C_{13}$	C <sub>33</sub>	$C_{44}$	C <sub>66</sub>	G	В	ν	G/B	Cauchy Pressure/B	Note
V <sub>2</sub> GeC	282	121	144	259	160	80.5	108	182	0.2532	0.5908	0.0672	LDA <sup>91</sup>
Cr <sub>2</sub> GeC	315	148	146	354	89	83.5	88	207	0.3130	0.4273	0.2937	LDA <sup>91</sup>
Zr <sub>2</sub> GeC	224	105	108	243	99	59.5	74	148	0.2856	0.5004	0.1842	LDA <sup>91</sup>
Nb <sub>2</sub> GeC	308	133	168	306	177	87.5	119	206	0.2590	0.5744	0.0884	LDA <sup>91</sup>
Mo <sub>2</sub> GeC	331	136	184	342	123	97.5	100	223	0.3052	0.4478	0.2235	LDA <sup>91</sup>
Hf <sub>2</sub> GeC	269	96	125	278	128	86.5	97	167	0.2568	0.5804	0.0194	LDA <sup>91</sup>
Ta <sub>2</sub> GeC	370	147	194	389	220	111.5	149.9	243.4	0.2445	0.6161	0.0195	LDA <sup>91</sup>
W <sub>2</sub> GeC	340	146	222	368	117	97.0	96.7	244	0.3963	0.3250	0.3156	$LDA^{91}$
Ti-GaC	314	66	50	272	122	124	121	1/1	0.3703	0.8627	-0.4306	$LDA^{92}$
$I_2 GaC$	374	88	135	310	1/0	1/1 5	121	107	0.1050	0.6704	-0.4500	LDA $LDA^{92}$
$T_2 C_2 C_2$	420	101	135	222	149	141.5	152	217	0.2200	0.0704	-0.1713	LDA 1 DA <sup>92</sup>
$1a_2 \text{OaC}$	420	101	140	212	1/5	139.5	120	217 101	0.2100	0.0929	-0.2013	
V <sub>2</sub> GaC	343	0/	124	312	157	138	133	181	0.2044	0.7362	-0.2877	$LDA^{-1}$
V	232.4	119.36	-	-	45.95	-	50	157	0.3563	0.31/9	0.4675	$4.2K^{93}$
V	227.95	118.75	-	-	42.55	-	47	155	0.3624	0.3031	0.4911	300K <sup>33</sup>
Ta	267.95	162.4	-	-	86.75	-	71	198	0.3394	0.3597	0.3829	4.2K <sup>94</sup>
Та	266.86	162.17	-	-	85.49	-	70	197	0.3407	0.3563	0.3891	100K <sup>94</sup>
Ta	264.82	161.29	-	-	83.32	-	69	195.8	0.3426	0.3516	0.3982	$200K^{94}$
Та	262.77	160.88	-	-	81.44	-	67	194.8	0.3448	0.3463	0.4077	300K <sup>94</sup>
Ta90W10	287.98	162.11	-	-	87.21	-	76.5	204	0.3333	0.3750	0.3670	$4.2K^{94}$
Ta90W10	286.78	161.98	-	-	86.28	-	75.8	203.6	0.3344	0.3722	0.3718	100K <sup>94</sup>
Ta90W10	284.73	161.73	-	-	84.68	-	74.5	202.7	0.3363	0.3675	0.3801	200K <sup>94</sup>
Ta90W10	282.51	161.24	-	-	83.15	-	73.3	201.7	0.3380	0.3633	0.3872	300K <sup>94</sup>
Ta70W30	325.95	173.26	-	-	87.31	-	82.7	224.1	0.3357	0.3691	0.3834	$4.2K^{94}$
Ta70W30	325.10	172.67	-	-	86.93	-	82.5	223.5	0.3357	0.3690	0.3837	100K <sup>94</sup>
Ta70W30	323.12	171.60	_	_	86.23	-	81.9	222.1	0 3359	0.3686	0 3844	200K <sup>94</sup>
Ta70W30	321.13	170.42	_	_	85 56	_	81.3	222.1	0.3359	0.3685	0.3846	300K <sup>94</sup>
Ta50W50	371 14	185.65	_	_	86 72	_	89.1	247.5	0.3393	0.3599	0.3007	$4.2 K^{94}$
Ta50W50	370.38	185.10			87.07		80.2	247.5	0.3397	0.3577	0.3074	1.2K 100K <sup>94</sup>
Ta50W50	268 50	103.19	-	-	87.07	-	89.2	240.9	0.3367	0.3014	0.3974	200K94
Ta50W50	266.59	103.03	-	-	07.49	-	09.4	243.4	0.3370	0.3043	0.3920	200K <sup>9</sup>
Ta50W50	424.65	102.23	-	-	00.05	-	09.7	245.7	0.3301	0.3079	0.3800	500K
1a55W07	434.03	191.29	-	-	114.43	-	117.5	272.4	0.3118	0.4305	0.2821	4.2K <sup>2</sup>
Ta33W6/	433.50	191.13	-	-	114.30	-	11/.0	2/1.9	0.3118	0.4303	0.2825	100K <sup>94</sup>
Ta33W67	430.52	190.88	-	-	114.05	-	116.3	270.8	0.3121	0.4296	0.2838	200K <sup>54</sup>
Ta33W67	426.86	189.97	-	-	113.84	-	115.7	268.9	0.3119	0.4300	0.2831	300K <sup>94</sup>
Ta17W83	481.68	196.41	-	-	139.32	-	140.6	291.5	0.2922	0.4825	0.1958	$4.2K^{94}$
Ta17W83	480.49	196.21	-	-	139.07	-	140.3	290.9	0.2923	0.4821	0.1964	$100K^{94}$
Ta17W83	476.94	196.42	-	-	138.34	-	139.1	289.9	0.2932	0.4798	0.2003	$200K^{94}$
Ta17W83	473.12	196.72	-	-	137.68	-	137.9	288.9	0.2941	0.4774	0.2044	300K <sup>94</sup>
W	530.25	201.90	-	-	160.92	-	162.2	311.4	0.2780	0.5210	0.1316	$4.2K^{94}$
W	529.81	199.98	-	-	160.83	-	162.5	309.9	0.2769	0.5242	0.1263	100K <sup>94</sup>
W	526.42	200.75	-	-	159.58	-	160.9	309.3	0.2784	0.5201	0.1331	200K <sup>94</sup>
W	521.48	201.01	-	-	158.50	-	159.2	307.8	0.2795	0.5171	0.1381	300K <sup>94</sup>
V	237	122	-	-	47.08	-	82.7	224.1	0.3357	0.3691	0.3834	$4.2K^{95}$
V	236.09	121.09	-	-	46.145	-	50.4	159.4	0.3570	0.3161	0.4701	100K <sup>95</sup>
V	233.38	120.72	-	-	44.800	-	49.1	158.3	0.3594	0.3102	0.4797	200K <sup>95</sup>
V	230.98	120.17	-	-	43.768	-	48	157	0.3611	0.3062	0.4863	300K <sup>95</sup>
V	281.72	124.63	-	-	36.09	-	49.6	177.0	0.3716	0.2800	0.5002	EMTO <sup>96</sup>
V-2.5Cr	285.81	125.15	_	_	35.38	_	49.5	178.7	0.3733	0.2768	0.5023	EMTO <sup>96</sup>
V-5Cr	289 59	125.48	_	_	34 37	-	19.1	180.2	0 3751	0 2726	0.5057	EMTO <sup>96</sup>
V-7 5Cr	292.85	125.84	_	_	33.20	-	48.5	181.5	0.3773	0.2674	0.5104	EMTO <sup>96</sup>
V10Cr	296.66	125.01	_	_	32.15	-	48.2	182.7	0.3789	0.2635	0.5124	EMTO <sup>96</sup>
V-2 5Ti	275.2	123.49	_	_	36.60	_	49.2	174 1	0.3708	0.2828	0.4992	EMTO <sup>96</sup>
V_5Ti	260.21	122.12	_	_	37.03	_	19.2	171.3	0.3700	0.2020	0.1992	EMTO <sup>96</sup>
V 7 5T;	269.21	122.40	-	-	27.05	-	40.9	162.0	0.3097	0.2000	0.4965	EMTO96
V-7.511	205.45	121.55	-	-	20 22	-	40.7	166.9	0.3084	0.2005	0.4905	EMTO%
V-1011	237.71	120.55	-	-	26.52	-	40.3	175.0	0.30/1	0.2910	0.4940	EMIO <sup>26</sup>
V-2.5CF-2.511	279.70	123.82	-	-	30.11	-	49.4	1/5.8	0.3715	0.2811	0.4989	EMIO <sup>26</sup>
V-2.5Cr-511	2/3.49	122.72	-	-	36.76	-	49.2	1/3.0	0.3700	0.2846	0.4969	EMIO <sup>36</sup>
v-2.5Cr-7.5Ti	207.53	121.67	-	-	57.27	-	48.9	1/0.3	0.3689	0.2874	0.4956	EMITO <sup>20</sup>
v-2.5Cr-10Ti	201.76	120.70	-	-	37.94	-	48.8	16/.7	0.36/5	0.2907	0.4934	EMTO
v-4Cr-4Ti	2/8.56	123.34	-	-	36.16	-	49.4	1/5.1	0.3711	0.2819	0.4979	EMTO
V-5Cr-2.5Ti	283.72	124.23	-	-	35.47	-	49.4	177.4	0.3726	0.2784	0.5004	EMTO <sup>90</sup>
V-5Cr-5Ti	277.78	123.02	-	-	36.24	-	49.4	174.6	0.3708	0.2827	0.4970	EMTO <sup>96</sup>
V-5Cr-7.5Ti	271.64	121.97	-	-	36.85	-	49.1	171.9	0.3695	0.2859	0.4953	EMTO <sup>96</sup>
V-5Cr-10Ti	265.81	120.92	-	-	37.53	-	48.9	169.2	0.3680	0.2895	0.4928	EMTO <sup>96</sup>
V-7.5Cr-2.5Ti	287.22	124.30	-	-	34.62	-	49.2	178.6	0.3739	0.2752	0.5021	EMTO <sup>96</sup>
V-7.5Cr-5Ti	282.71	122.87	-	-	35.68	-	49.6	176.2	0.3713	0.2816	0.4950	EMTO <sup>96</sup>
V-7.5Cr-7.5Ti	275.88	122.25	-	-	36.51	-	49.4	173.5	0.3699	0.2849	0.4943	EMTO <sup>96</sup>
V-7.5Cr-10Ti	269.97	121.12	-	-	37.17	-	49.3	170.7	0.3684	0.2886	0.4917	EMTO <sup>96</sup>
V-10Cr-2.5Ti	291.44	124.77	-	-	33.76	-	53.9	179.4	0.3635	0.3004	0.5037	EMTO <sup>96</sup>
V-10Cr-5Ti	285 66	123.62	_	_	35.03	-	534	177 6	0 3633	0 3008	0 4987	EMTO <sup>96</sup>

TABLE XI: The elastic properties (in GPa) of potential structural materials for nuclear reactors, as well as experimental results(continued).

	Cu	Cu	Cu	Caa	Си	C	G	B	V	G/B	Cauchy Pressure/B	Note
V 10C 7 5T	200.01	122 12	C13	C33	26.05	C 66	50	175	0 2702	0.2842		EMTO <sup>96</sup>
V-10Cr-7.511	280.81	122.13	-	-	30.05	-	50	175	0.3702	0.2842	0.4918	EMIO <sup>26</sup>
V-10Cr-1011	2/4.0/	121.35	-	-	36.90	-	50	172	0.3686	0.2879	0.4903	EMIO
Nb	244.1	130	-	-	27.8	-	37.2	168.0	0.3968	0.2216	0.6082	300K <sup>97</sup>
Nb90Zr10	229.2	124.8	-	-	27.0	-	35.3	159.6	0.3971	0.2210	0.6128	300K <sup>97</sup>
Nb80Zr20	203	114	-	-	27.1	-	33.0	143.6	0.3930	0.2303	0.6049	300K <sup>97</sup>
Nb70Zr30	180.8	106.4	-	-	28.6	-	31.7	131.2	0.3879	0.2422	0.5930	300K <sup>97</sup>
Nb60Zr40	164.9	100.0	-	-	30.0	-	31.0	121.6	0.3827	0.2545	0.5755	300K <sup>97</sup>
Nb50Zr50	151.8	96.6	_	_	31.8	_	30.0	115.0	0 3798	0.2613	0 5635	300K <sup>97</sup>
Nb307r70	124.4	88 7			33.6		26.2	100.3	0.3708	0.2614	0.5445	300K <sup>97</sup>
NUJUZI70	124.4	124.4	-	-	247	-	20.2	156.2	0.3790	0.2014	0.5445	1500K
IND	220.1	124.4	-	-	34.7	-	39.5	150.5	0.3835	0.2525	0.5739	1500K <sup>97</sup>
Nb90Zr10	204.2	119.2	-	-	34.6	-	37.6	147.5	0.3826	0.2547	0.5734	1500K <sup>37</sup>
Nb80Zr20	177.4	108.1	-	-	33.4	-	33.9	131.2	0.3811	0.2583	0.5694	1500K <sup>97</sup>
Nb70Zr30	156.9	101.5	-	-	33.1	-	30.8	119.9	0.3817	0.2569	0.5702	1500K <sup>97</sup>
Nb60Zr40	144.9	96.4	-	-	31.4	-	28.3	112.6	0.3840	0.2515	0.5774	1500K <sup>97</sup>
Nb50Zr50	131.3	92.6	-	-	30.5	-	25.5	105.4	0.3885	0.2409	0.5886	1500K <sup>97</sup>
Nb30Zr70	111.9	84.0	-	_	28.7	-	21.5	93.3	0.3931	0.2303	0.5927	1500K <sup>97</sup>
Nb50Zr50	155.6	96.9	-	_	33.2	_	31.6	116.5	0 3756	0 2713	0 5469	5K <sup>97</sup>
Nb50Zr50	1/0	05.0	_	_	31.0	_	20.6	113.6	0.3700	0.2710	0.5634	500K <sup>97</sup>
Nb50Zr50	141.2	93.9	-	-	21.7	-	29.0	110.1	0.2722	0.2009	0.5054	1000K <sup>97</sup>
NU50Z150	141.2	94.5	-	-	20.7	-	21.9	10.1	0.3652	0.2334	0.5755	1500K <sup>97</sup>
ND50Zr50	132	92.5	-	-	30.7	-	25.7	105.7	0.38/4	0.2434	0.5849	1500K <sup>27</sup>
Cr-0.67%V	379.6	78.2	-	-	102.73	-	119.8	178.7	0.2259	0.6706	-0.1373	80K <sup>98</sup>
Cr-0.67%V	378.8	78.1	-	-	102.64	-	119.6	178.3	0.2259	0.6709	-0.1376	$100K^{98}$
Cr-0.67%V	375.3	77.5	-	-	102.23	-	118.9	176.8	0.2253	0.6726	-0.1399	150K <sup>98</sup>
Cr-0.67%V	370.3	76.1	-	-	101.76	-	118.0	174.2	0.2237	0.6774	-0.1473	200K <sup>98</sup>
Cr-0.67%V	366.1	74.3	-	-	101.41	-	117.4	171.6	0.2215	0.6840	-0.1580	230K <sup>98</sup>
Cr-0.67%V	363.9	72.9	_	_	101 30	_	117 1	169.9	0 2197	0.6895	-0.1672	240K <sup>98</sup>
Cr-0.67%V	362.8	71.9	_	_	101.50	_	1171	168.9	0.2197	0.6035	-0.1739	245K <sup>98</sup>
Cr = 0.67%V	260.0	79.5	_	_	101.27	_	117.1	175.2	0.2104	0.677	0.1206	250K98
$C_{1} = 0.07\%$ V	272.0	10.5	-	-	101.22	-	117.0	175.5	0.2270	0.0074	-0.1290	250K <sup>98</sup>
Cr-0.6/%V	372.8	82.9	-	-	101.12	-	116.8	1/9.5	0.2326	0.6508	-0.1015	260K <sup>26</sup>
Cr-0.67%V	373.2	85.9	-	-	100.72	-	116.1	181.7	0.2365	0.6393	-0.0816	300K <sup>98</sup>
Cr-0.67%V	371.8	88.0	-	-	100.23	-	115.2	182.6	0.2393	0.6313	-0.0670	350K <sup>98</sup>
Cr-1.5%V	383.4	102.2	-	-	102.10	-	116.1	195.9	0.2526	0.5924	0.0005	80K <sup>98</sup>
Cr-1.5%V	382.4	102.1	-	-	101.97	-	115.8	195.5	0.2526	0.5924	0.0007	100K <sup>98</sup>
Cr-1.5%V	380.1	101.6	-	-	101.59	-	115.3	194.4	0.2525	0.5929	0.0001	130K <sup>98</sup>
Cr-1.5%V	378.5	101.5	-	-	101.33	-	114.9	193.8	0.2526	0.5926	0.0009	150K <sup>98</sup>
Cr-1 5%V	377.7	101.6	_	_	101.20	_	114.6	193.6	0.2528	0 5919	0.0021	160K <sup>98</sup>
Cr 1.5%V	377.3	101.0			101.20		11/1.0	103.0	0.2520	0.5023	0.0014	165K <sup>98</sup>
Cr 1.5%V	280.7	101.4	-	-	1101.15	-	120.6	106.9	0.2327	0.5925	0.0014	170K <sup>98</sup>
$C_{1} = 1.5\%$ V	200.7	104.0	-	-	101.02	-	120.0	190.0	0.2450	0.0127	-0.0275	170K
Cr-1.5%V	382.1	106.4	-	-	101.02	-	114.4	198.3	0.2580	0.5//1	0.0271	1/5K <sup>20</sup>
Cr-1.5%V	382.0	106.6	-	-	101.00	-	114.4	198.4	0.2582	0.5764	0.0282	180K <sup>98</sup>
Cr-1.5%V	381.9	107.1	-	-	100.91	-	114.2	198.7	0.2588	0.5748	0.0312	190K <sup>98</sup>
Cr-1.5%V	381.5	107.2	-	-	100.83	-	114.1	198.6	0.2590	0.5743	0.0321	$200K^{98}$
Cr-1.5%V	379.5	108.2	-	-	100.36	-	113.2	198.6	0.2605	0.5701	0.0395	250K <sup>98</sup>
Cr-1.5%V	376.4	107.9	-	-	99.88	-	112.5	197.4	0.2606	0.5697	0.0406	300K <sup>98</sup>
Cr-1.5%V	373.4	108.2	-	_	99.42	_	111.6	196.6	0.2614	0.5676	0.0447	350K <sup>98</sup>
Cr	394.1	88.5	_	_	103 75	_	121.2	190.4	0 2374	0.6367	-0.0801	0K <sup>9</sup>
Cr	303.2	88 2			103.73		121.2	190.1	0.2370	0.6378	0.0001	50K <sup>9</sup>
Cr	200.0	00.2 07.4	-	-	102.75	-	121.1	109.9	0.2370	0.0378	-0.0818	100K <sup>9</sup>
Cr	389.8	87.4	-	-	103.28	-	120.4	188.2	0.2304	0.0393	-0.0844	100K
Cr	389.4	87.4	-	-	103.04	-	120.1	188.1	0.2367	0.6388	-0.0832	110K <sup>2</sup>
Cr	388.0	87.2	-	-	102.35	-	119.5	187.5	0.2372	0.6372	-0.0808	120K <sup>9</sup>
Cr	386.5	95.3	-	-	101.33	-	117.2	192.4	0.2468	0.6092	-0.0313	125K <sup>9</sup>
Cr	380.4	91.0	-	-	101.93	-	117.3	187.5	0.2411	0.6258	-0.0583	130K <sup>9</sup>
Cr	380.3	92.7	-	-	102.28	-	117.3	188.6	0.2425	0.6219	-0.0508	135K <sup>9</sup>
Cr	378.7	92.9	-	-	102.35	-	117.0	188.2	0.2425	0.6219	-0.0502	140K <sup>9</sup>
Cr	378 5	94 5	-	_	102.38	_	1167	189.2	0 2441	0.6171	-0.0417	145K <sup>9</sup>
Cr	374.7	00.0			101.00		11/ 0	101.5	0.2/00	0.6002	-0.0100	185K <sup>9</sup>
Cr	272.0	<i>99.9</i>	-	-	101.99	-	114.9	191.5	0.2499	0.0002	-0.0109	200K <sup>9</sup>
Cr	312.9	99.5	-	-	101.60	-	114.0	190.5	0.2494	0.0010	-0.0151	200K <sup>9</sup>
Cr	364.7	90.9	-	-	101.15	-	114.2	182.2	0.2407	0.6269	-0.0563	250K <sup>2</sup>
Cr	348.4	70.2	-	-	100.71	-	114.6	162.9	0.2150	0.7036	-0.1873	300K <sup>9</sup>
Cr	345.1	66.3	-	-	100.67	-	114.7	159.2	0.2096	0.7204	-0.2158	305K <sup>9</sup>
Cr	337.2	57.4	-	-	100.70	-	114.9	150.7	0.1960	0.7626	-0.2874	310K <sup>9</sup>
Cr	354.2	72.4	-	-	100.67	-	115.2	166.3	0.2186	0.6926	-0.1699	315K <sup>9</sup>
Cr	356.4	75.0	-	-	100.64	-	115.1	168.8	0.2222	0.6820	-0.1519	320K <sup>9</sup>
Cr	358.4	774	_	_	100 53	_	114.9	171.1	0 2254	0.6721	-0.1352	330K <sup>9</sup>

	CP class	Eigenvalue1	Eigenvalue2	Eigenvalue3	$\Delta  ho$	charge density
Diamond-C	Bond	-4.731E-1	-4.731E-1	3.796E-1	-5.667E-1	2.404E-1
Diamond-C	Ring	-1.694E-2	6.183E-2	6.244E-2	1.073E-1	2.123E-2
Diamond-C	Cage	2.500E-2	2.500E-2	2.500E-2	7.499E-2	1.312E-2
Diamond-Si	Bond	-7.280E-2	-7.280E-2	2.156E-2	-1.240E-1	8.340E-2
Diamond-Si	Ring	-2.078E-3	7.253E-3	7.314E-3	1.249E-2	5.366E-3
Diamond-Si	Cage	2.742E-3	2.742E-3	2.742E-3	8.220E-3	3.113E-3
Diamond-SI-HSE	Bond	-/./4/E-2	-/./4/E-2	1./14E-2	-1.3/8E-1	8.085/E-2
Diamond-SI-HSE	King	-2.190E-3	7.074E-3	7.074E-3	1.313E-2	3.3/3E-3 2.1947E-2
Diamond-SI-HSE	Cage	2.890E-3	2.890E-3	2.890E-3	8.0808E-3	3.184/E-3
fee Ti	Dond	-1.300E-03	-1.300E-03	-1.300E-03	-4.080E-03	2.972E-02
1cc-11	Bond	-2.493E-03	-2.493E-03	1.750E-05	-3.092E-03	2.971E-02
fee Ti	King	-3.304E-03	3.030E-03	3.243E-02	5.038E-02	2.797E-02
fee Zr	Cage	4.800E-04	4.800E-04	4.800E-04	1.442E-05	2.439E-02
foo Zr	Dond	-4.23/E-04	-4.237E-04	-4.237E-04	-1.2/1E-03	2.040E-02
fee Zr	Dona	-8.391E-04	-0.391E-04	0.080E-04	-1.110E-03	2.040E-02
fee Zr	Corro	-3.331E-03	2.233E-03	2.830E-02	2.323E-02	2.335E-02 2.100E-02
fee Al	Dond	1.000E-03	2.570E.02	1.000E-03	2.039E-02	3.199E-03 2.007E 2
fee Al	Donu	-1.04JE-2	-2.370E-03	1.313E-02	1.14/E-4	3.007E-2
fee Al	C aita	-2.002E-03	4.776E-03	4.776E-03	0.934E-03	2.01/E-2 1.600E 2
fee Al	U-site	7.032E-03	7.032E-03	7.032E-03	2.290E-02	1.090E-2
fee Cu	I-Sile Dond	2.311E-03	2.511E-05	2.311E-03	7.332E-03	2.000E-2 2.924E-02
fee Cu	Donu	-2.077E-02	-1.510E-02	1.002E-01	0.425E-02	3.624E-02
fee Cu	C aita	-9.079E-03	2.190E-02	2.190E-02	3.411E-02 2.072E-02	3.142E-02
fee Cu	U-site	9.909E-03	9.909E-03	9.909E-03	2.975E-02	2.069E-02
fee Au	I-site Bond	1.095E-02	1.095E-02	1.095E-02	5.265E-02	3.044E-02 3.708E-02
fcc-Au	Donu Ring	-2.014E-02	-1.991E-02	2 030F-02	7.472E-02	2.578E-02
fcc-Au	O_site	8 820E-03	2.700E-02 8.820E-03	2.939E-02	4.040E-02	1 310E-02
fcc-Au	T-site	1.488E-02	1.488E-02	1.488E-02	2.040E-02 4.463E-02	2 371E-02
bcc-Mo	Bond	-0.0225	-0.0223	0.0796	0.035	0.050
bcc-Mo	Ring	-0.0225	0.0225	0.0095	0.035	0.037
bcc-Mo	Cage	0.0048	0.0025	0.0057	0.015	0.035
bcc-Nh	Bond	-0.0158	-0.0158	0.0900	0.015	0.0414
bcc-Nb	Ring	-0.0016	0.0190	0.0082	0.0148	0.0307
bcc-Nb	Cage	0.0010	0.0029	0.0134	0.0191	0.0296
hcn-Ti	Nuclei	-0.0016	0.0082	0.0082	-0.0065	0.0335
hcp-Ti	Bond1	0.0029	0.0029	0.0134	-8.074E-5	0.0311
hcp-Ti	Bond2	0.0029	0.0029	0.0134	-0.0062	0.0335
NaCl	Bond1	-2.291E-3	-1.158E-3	1.537E-2	1.192E-2	4.630E-3
NaCl	Bond2	-1.098E-2	-1.097E-2	7.881E-2	5.686E-2	1.180E-2
NaCl	Ring	-2.207E-3	4.412E-3	1.103E-2	1.324E-2	4.270E-3
NaCl	Cage	1.520E-3	1.520E-3	1.520E-3	4.561E-3	1.877E-3
KCl	Bond	-8.756E-03	-8.755E-03	5.886E-02	4.135E-02	1.139E-02
KCl	Ring	-9.270E-04	2.892E-04	6.398E-03	5.760E-03	2.146E-03
KCl	Cage	6.080E-04	6.080E-04	6.080E-04	1.824E-03	7.640E-04
Graphene	Bond	-2.821E-04	-2.810E-04	4.757E-03	4.194E-03	1.307E-03
Diamond-C	Bond	-4.731E-1	-4.731E-1	3.796E-1	-5.667E-1	2.404E-1
Diamond-Si	Bond	-7.280E-2	-7.280E-2	2.156E-2	-1.240E-1	8.340E-2
Diamond-Si-HSE	Bond	-7.747E-2	-7.747E-2	1.714E-2	-1.378E-1	8.6857E-2
fcc-Ti	Bond	-2.493E-03	-2.493E-03	1.750E-03	-3.092E-03	2.971E-02
fcc-Zr	Bond	-8.591E-04	-8.591E-04	6.080E-04	-1.110E-03	2.640E-02
fcc-Al	Bond	-1.045E-2	-2.570E-03	1.313E-02	1.147E-4	3.007E-2
fcc-Cu	Bond	-2.077E-02	-1.516E-02	1.002E-01	6.423E-02	3.824E-02
fcc-Au	Bond	-2.014E-02	-1.991E-02	1.148E-01	7.472E-02	3.708E-02
bcc-Mo	Bond	-0.0225	-0.0223	0.0796	0.035	0.050
bcc-Nb	Bond	-0.0158	-0.0158	0.0900	0.0584	0.0414
hcp-Ti	Bond1	0.0029	0.0029	0.0134	-8.074E-5	0.0311
hcp-Ti	Bond2	0.0029	0.0029	0.0134	-0.0062	0.0335
NaCl	Bond1	-2.291E-3	-1.158E-3	1.537E-2	1.192E-2	4.630E-3
NaCl	Bond2	-1.098E-2	-1.097E-2	7.881E-2	5.686E-2	1.180E-2
KCl	Bond	-8.756E-03	-8.755E-03	5.886E-02	4.135E-02	1.139E-02

TABLE XII: The calculated Eigenvalue of Hessian matrix at critical points and  $\triangle \rho$ .

TABLE XIII: The charge density (in electrons per Bohr<sup>3</sup>), laplacian of charge density (in electrons per Bohr<sup>5</sup>) at bonding critical points, shear modulus (in GPa), bulk modulus (in GPa), G/B and Poisson's ratio for fcc and bcc metals.

	$ ho_b$	$\Delta  ho$	θ	$< tan(\theta) >$	G	В	G/B	ν
fcc-Au	3.708E-2	7.472E-2	22.67	0.4177	24	185	0.1301	0.4376
fcc-Pt	5.185E-2	9.207E-2	24.35	0.4526	40	247	0.1620	0.4231
fcc-Pd	4.034E-2	7.732E-2	23.45	0.4338	40	166	0.2391	0.3893
fcc-Cu	3.824E-2	6.423E-2	22.95	0.4235	39	156	0.2499	0.3847
fcc-Al	3.007E-2	1.147E-4	35.15	0.7040	26	79	0.3319	0.3506
fcc-Ir	6.300E-2	8.789E-2	25.90	0.4857	218	348	0.6279	0.2404
bcc-Nb	4.140E-2	5.844E-2	22.72	0.4188	24	174	0.1368	0.4346
bcc-V	4.291E-2	6.023E-2	21.22	0.3884	41	184	0.2251	0.3953
bcc-Ta	4.792E-2	8.588E-2	21.61	0.3963	64	196	0.3262	0.3529
bcc-Mo	5.423E-2	7.932E-2	24.67	0.4595	125	265	0.4729	0.2958
bcc-W	6.054E-2	7.371E-1	24.10	0.4474	151	305	0.4955	0.2874
bcc-Cr	5.570E-2	7.866E-2	24.53	0.4564	137	256	0.5330	0.2737
Diamond-Si	8.340E-2	-1.240E-2	61.45	1.8476	63	89	0.7038	0.2150
Diamond	2.404E-1	-5.667E-1	48.15	1.1164	519	434	1.195	0.073
SiC	1.185E-01	3.001E-2	34.04	0.676	187	212	0.8803	0.1597
ZnS	6.809E-02	8.202E-02	28.99	0.554	32	70	0.4562	0.3020

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