

# Effects of Spark Plasma Sintering Conditions on the Anisotropic Thermoelectric Properties of Bismuth Antimony Telluride

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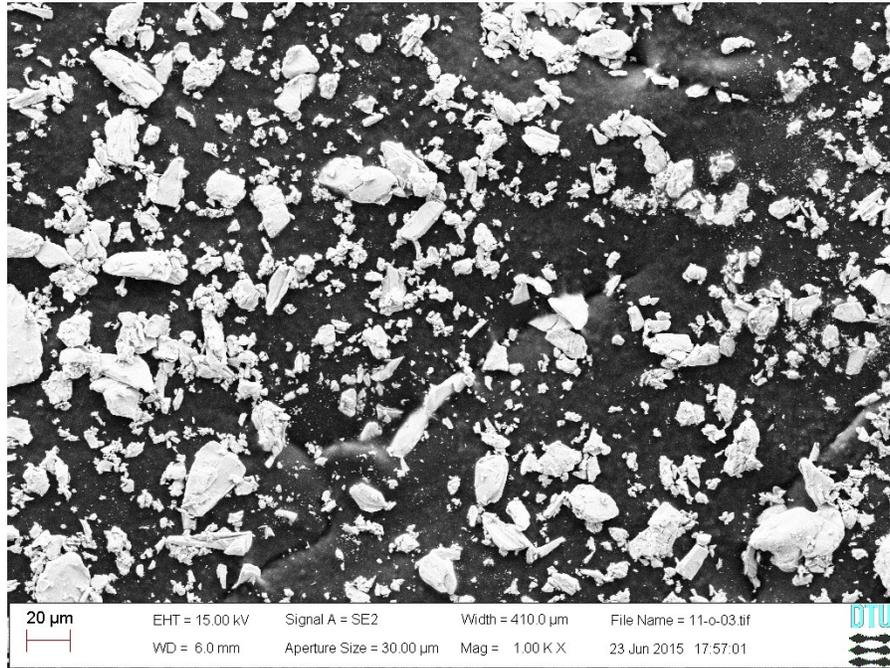
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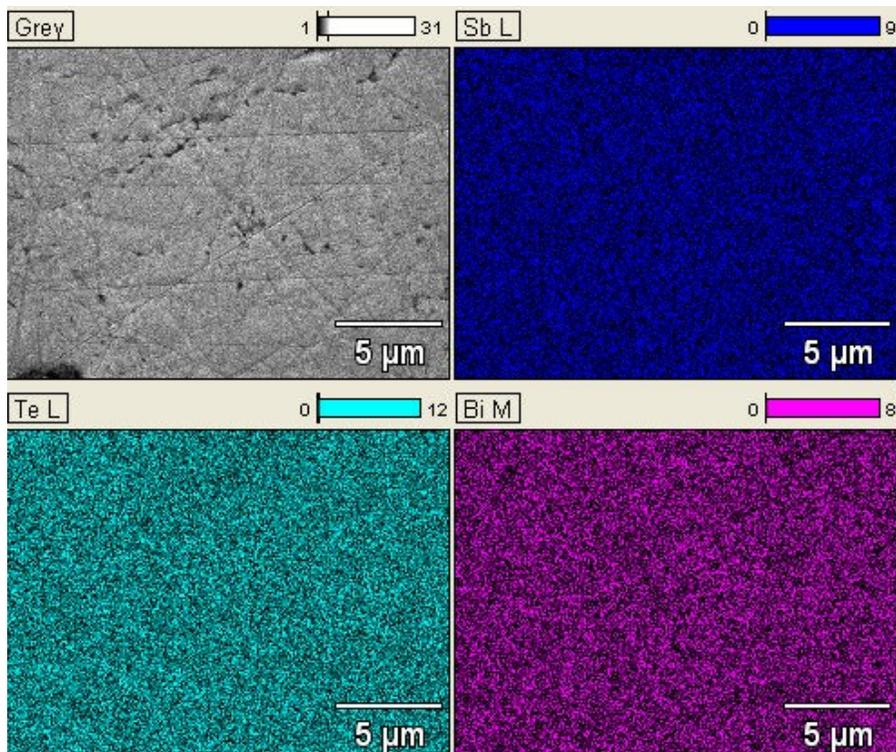
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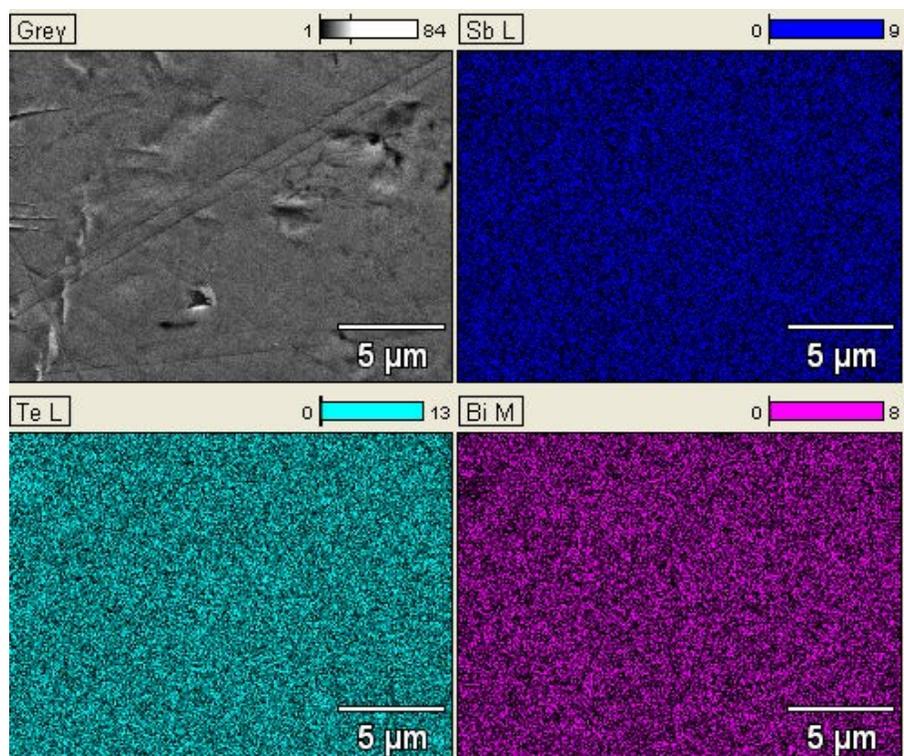
## 1. Supplement SEM images



**Fig. S1** SEM of the Commercial  $\text{Bi}_{0.4}\text{Sb}_{1.6}\text{Te}_3$  powder

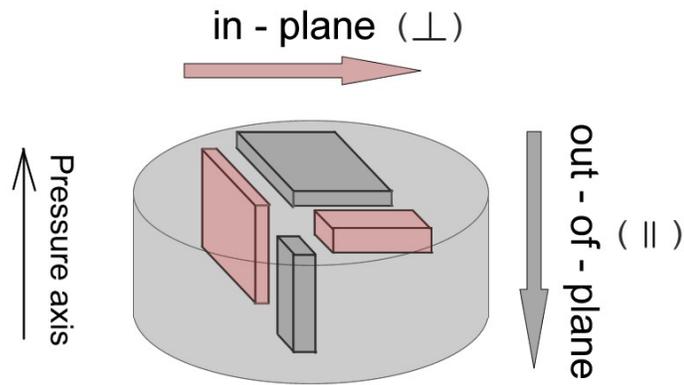


**Fig. S2** SEM-EDS element mapping of the specimen sintered by SPS at 653K.



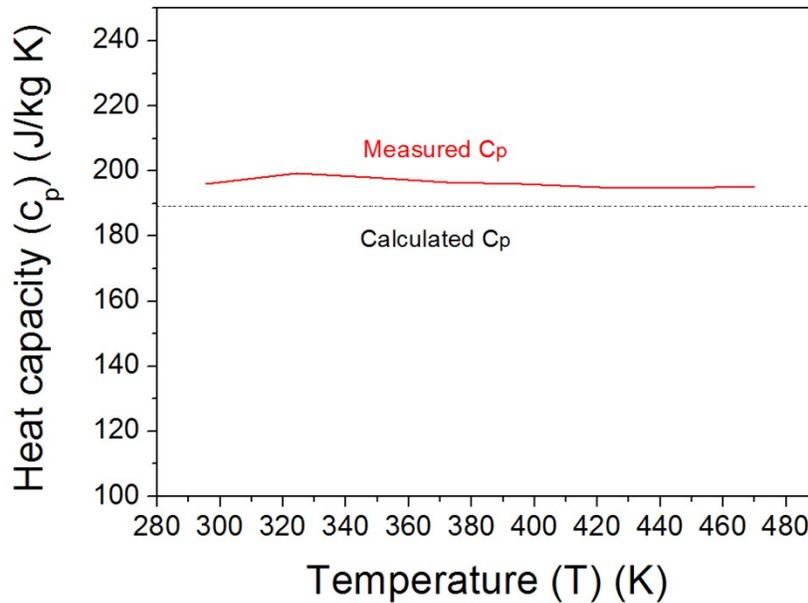
**Fig. S3** SEM-EDS element mapping of the specimen sintered by SPS at 773K.

## 2. SPS sample cutting schematics.



**Fig. S4** SPS sample cutting schematics. The red specimens were measured for in-plane thermoelectric properties, and the grey specimens were measured for out-of-plane thermoelectric properties.

## 3. Heat capacity $C_p$



**Fig S5.** Temperature dependence of the specific heat at constant pressure for  $\text{Bi}_{0.4}\text{Sb}_{1.6}\text{Te}_3$  samples, the red line represents the measured value by DSC, and the dotted line represents the calculated values by Dulong-petit law.

#### 4. Metal droplets squeezed out of graphite die after SPS sintering



**Fig. S6** Spilled droplets squeezed out of graphite die after SPS sintering at 723 K (left) and 773 K (right).

#### 5. Calculations of Lorenz number $L_o$

According to the measured  $n$  and estimated  $m^*$  values, a simple parabolic band model can be applied by employing the following equations:

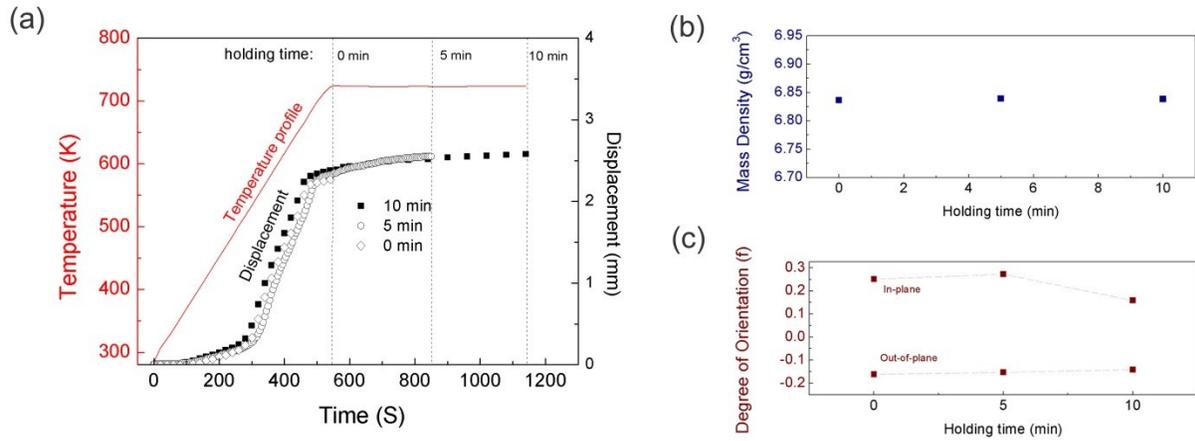
$$F_\lambda(\xi) = \int_0^\infty \frac{x^\lambda dx}{1 + \text{Exp}(x - \xi)} \quad (\text{S1})$$

$$L_o = \left( \frac{k_B^2}{q^2} \right) (3F_0 F_2 - 4F_1^2) / F_0^2 \quad (\text{S2})$$

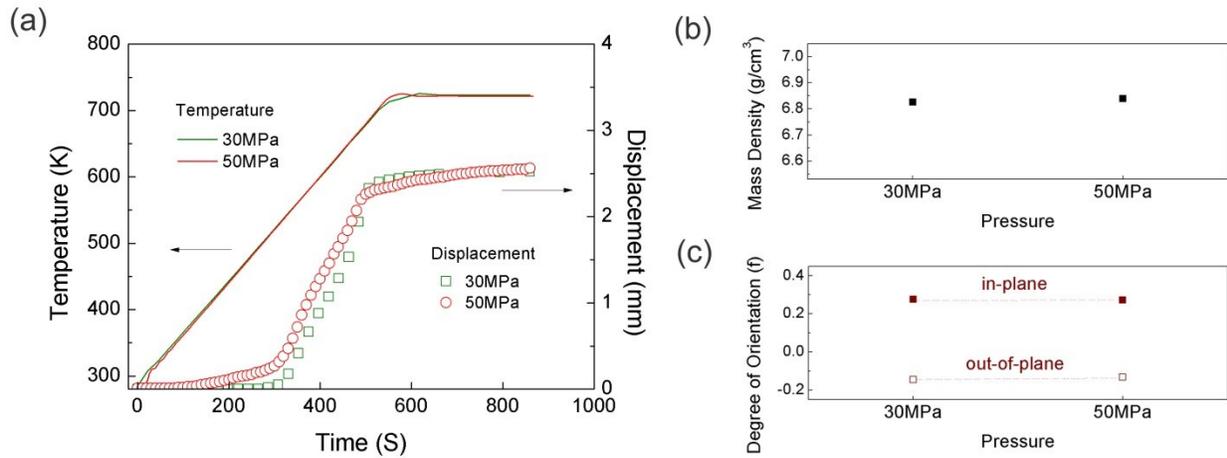
where  $F_\lambda(\xi)$  is the Fermi integral and  $\xi$  is the reduced electrochemical potential.  $\lambda$  is a scattering parameter and 0 is assumed for acoustic phonon scattering, 1 for optical phonons scattering, and 2 for ionized impurity scattering.  $k_B$  is the Boltzmann constant,  $q$  is the unit charge of electron.  $\xi$  is calculated from the measurement Seebeck coefficient ( $S$ ) using the following equation:

$$S = -\frac{k_B}{q} \left[ \frac{(2 + \lambda)F_{\lambda+1}}{(1 + \lambda)F_{\lambda}} - \xi \right] \quad (\text{S3})$$

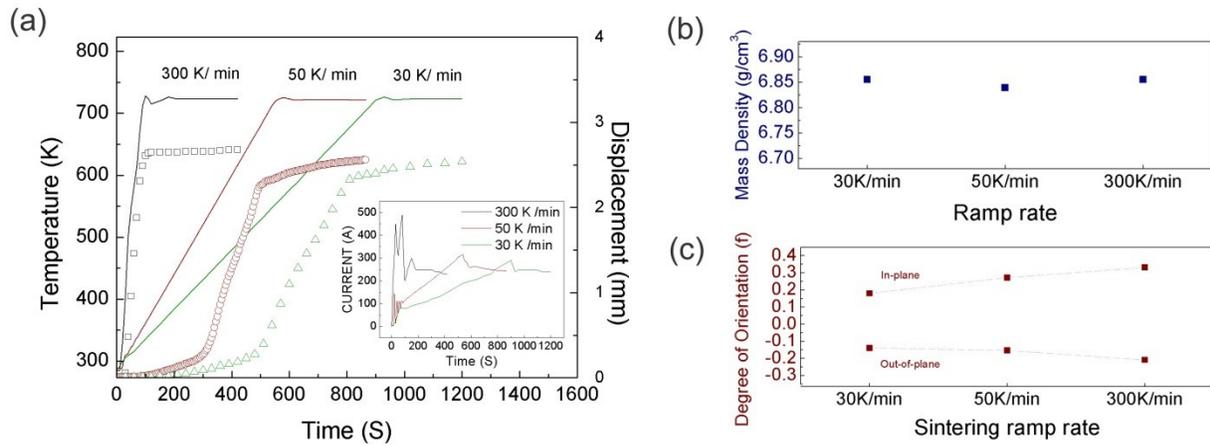
**6. Sintering profiles of samples sintered with variable holding time, pressure, and ramp-rate.**



**Fig. S7.** (a) Sintering profile for SPS sintering with variable holding time. (b) Mass density of the samples as a function of holding time. (c) Degree of orientation as a function of holding time.



**Fig. S8** (a) Sintering profile for SPS sintering with variable pressure. (b) Mass density of the SPS sintered samples with variable uniaxial pressure. (c) Degree of orientation as a function of uniaxial pressure.



**Fig. S9** (a) Sintering profile for SPS sintering with variable ramp-rate. The inset shows the current profile during SPS sintering. (b) Mass density of the samples sintered with variable ramp-rate. (c) Degree of orientation of the samples sintered with variable ramp-rate.