

**Supplementary material for**

**Sorption of perfluorooctane sulfonate and perfluorooctanoate on  
Polyacrylonitrile fibers-derived activated carbon fibers: In comparison with  
activated carbon**

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**Table 1** Characteristic parameters of polyacrylonitrile fibers (PANFs)

|                               | PANFs     |
|-------------------------------|-----------|
| Average diameter (μm)         | 17.05     |
| Tensile strength (eN/dtex)    | 4.5       |
| Elongation at break point (%) | 16-19     |
| Density (g/cm <sup>3</sup> )  | 1.19      |
| Linear density (dtex)         | 1.12-1.33 |
| Carbon content (%)            | 65        |
| Moisture content (%)          | 0.6-0.9   |
| Melting point (°C)            | 317       |

**Table 2** Characteristic parameters of PANFs-derived PACFs

|                                            | PANFs   |
|--------------------------------------------|---------|
| Specific surface areas (m <sup>2</sup> /g) | 1781.59 |
| Average diameter (μm)                      | 12.27   |
| Total pore volume (cm <sup>3</sup> /g)     | 0.94    |
| Carbon content (%)                         | 82      |
| Ash yield (%)                              | 2-3     |
| The loss of mass on drying method          | 35      |

### Sorption kinetics models

Pseudo-first-order and pseudo-second-order kinetics equations are represented as the functions of  $q_t$ ,  $q_e$  and  $t$ , which are given as below <sup>1</sup>:

Pseudo-first-order model:

$$\lg(q_e - q_t) = \lg q_e - \frac{k_1}{2.303} t \quad (3)$$

Pseudo-second-order model:

$$\frac{t}{q_t} = \frac{1}{k_2 q_e^2} + \frac{1}{q_e} t = \frac{1}{v_0} + \frac{t}{q_e} \quad (4)$$

Where  $k_1$  (1/h) and  $k_2$  (g/mmol/h) are the sorption rate constants of the pseudo-first-order model and the pseudo-second-order model, respectively.  $v_0$  is the initial adsorption rate (mmol/h/g). Other parameters are defined in equation (1).

### Intra-particle diffusion and Boy's film-diffusion models

The intra-particle diffusion model is shown as below <sup>2</sup>:

$$q_t = K_i t^{0.5} + C_i \quad (5)$$

Where  $K_i$  is the intra-particle diffusion rate constant (mmol/g·h<sup>1/2</sup>) at stage i and  $C_i$  is the intercept corresponding to stage i, which is proportional to the boundary layer thickness. The values of  $K_i$  and  $C_i$  can be evaluated from the linear plots of  $q_t$  versus  $t^{1/2}$ .

The Boy's film-diffusion model is shown as below <sup>3</sup>:

$$F = 1 - \left( \frac{6}{\pi^2} \right) \exp(-B_t) \quad (6)$$

Where  $F$  is the fractional attainment of equilibrium at different  $t$  (h), and  $B_t$  is a mathematical function of  $F$ .

$$F = \frac{q_e}{q_e} \quad (7)$$

$$B_t = -0.4977 - \ln(1 - F) \quad (8)$$

Where  $B_t$  can be calculated from equation (8) according to each value of  $F$ . The linearity of this plot provides a reliable information to identify that the rates of sorption is controlled by external mass transfer (film diffusion) or intraparticle diffusion.

### Sorption isotherm models

The Langmuir and Freundlich model equations are given as below <sup>4</sup>:

Langmuir model:

$$q_e = \frac{b q_m C_e}{1 + b C_e} \quad (9)$$

Freundlich model:

$$q_e = K_F C_e^n \quad (10)$$

Where  $C_e$  (mmol/L) and  $q_e$  (mmol/g) are the concentration of PFOS/PFOA in water and adsorbed on adsorbent reaching adsorption equilibrium, respectively.  $K_F$  and  $n$  are Freundlich constants related to adsorption capacity and adsorption intensity of the adsorbents, respectively.  $q_m$  (mmol/g) is the maximum sorption capacity, and  $b$  is the sorption equilibrium constant of Langmuir model related to the affinity of binding sites.

### Sorption site energy distributions

The approximate site energy distributions underlying Freundlich isotherm was introduced to relate the differences in sorption isotherms to alteration of energetic characteristics of different adsorbates-adsorbents interactions. It was based on the assumption of condensation approximation and expressed by the following equation (11) <sup>5</sup>.

$$\phi(\varepsilon) = \frac{K_F \cdot n \cdot S_w^n}{RT} \exp\left(\frac{-n\varepsilon}{RT}\right) \quad (11)$$

In the equation,  $\varepsilon$  is the net energy that equals to  $E_{\text{total}} - E_S$ , where  $E_{\text{total}}$  is the difference of sorption energy to a given site between adsorbate and water,  $S_w$  is the water solubility of the adsorbate, and  $E_S$  is the sorption energy at  $C_e = S_w$ .  $R$  is the universal gas constant, and  $T$  is the absolute temperature. Other parameters are defined in equation (10).

### References

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