

## Supporting Information

### Smart Design of Wettability-Patterned Gradient on Substrate-Independent Coated Surfaces to Control Unidirectional Spreading of Droplet

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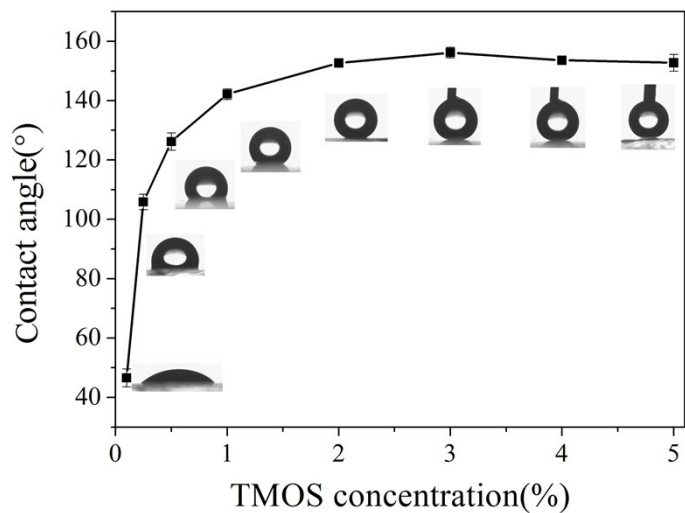
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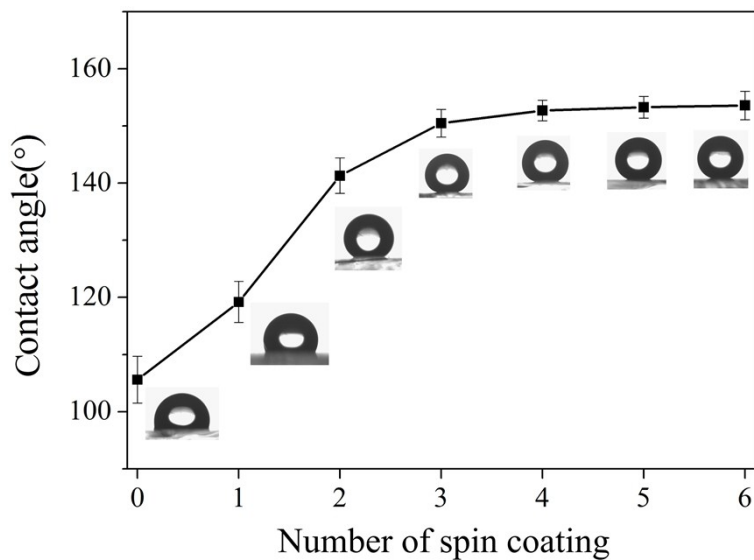
### Supplementary Analysis II:

**Figure S11.** Schematic illustration of drop motion

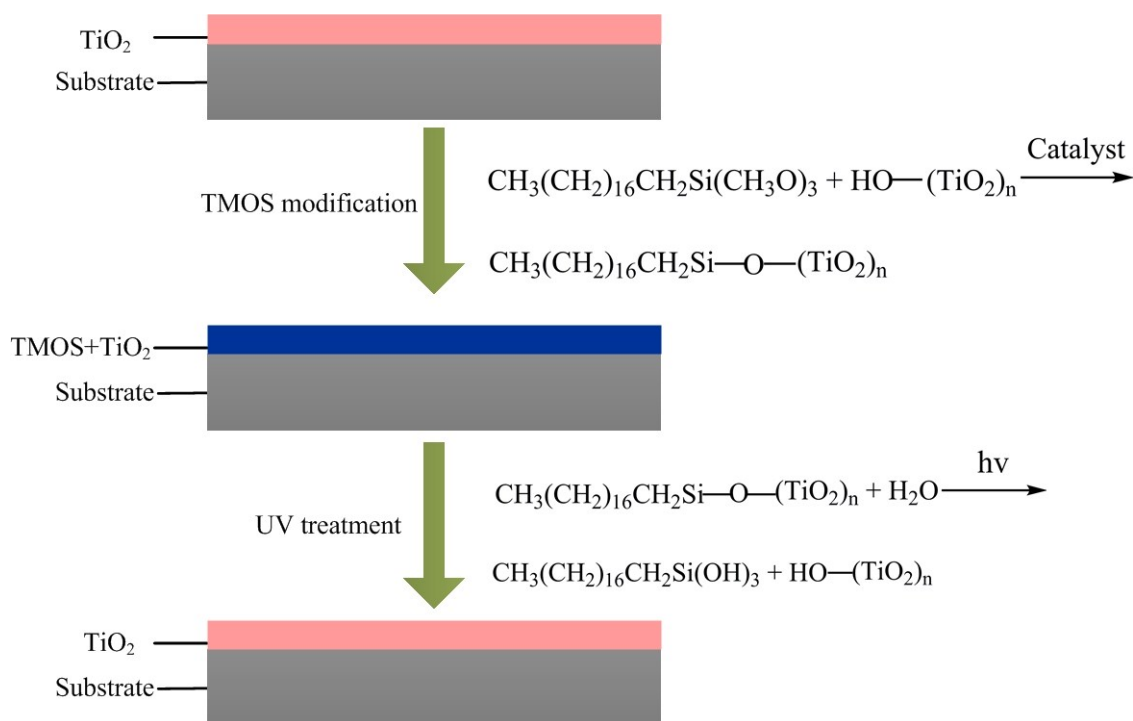
### Supplementary Analysis I:



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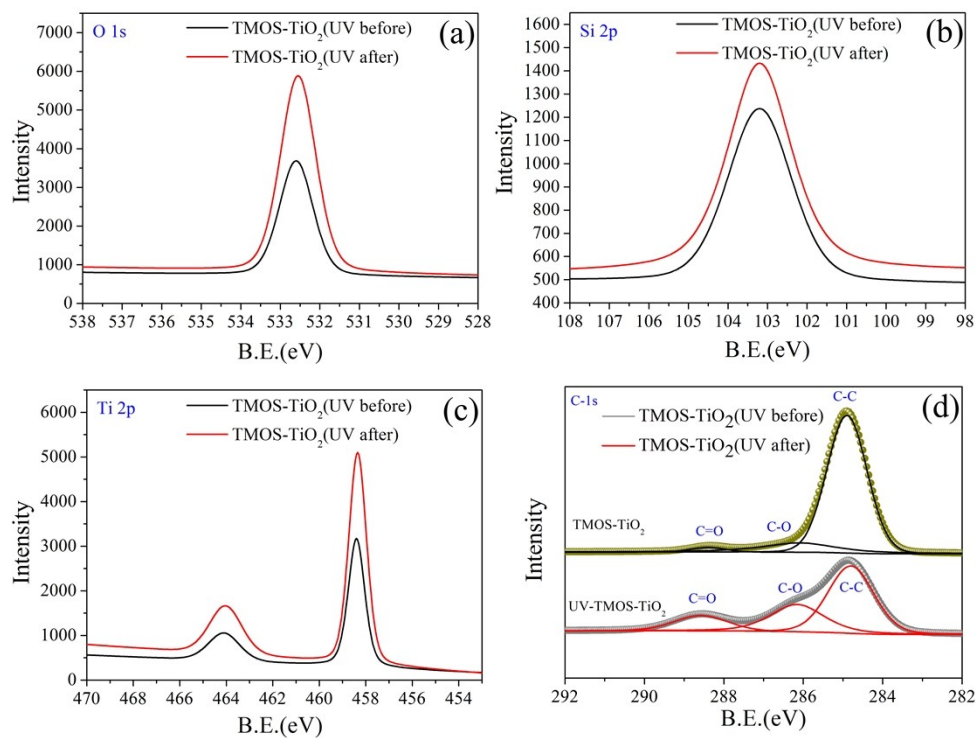
**Figure S2.** Effect of the number of spin coating on water contact angle on glass substrate.



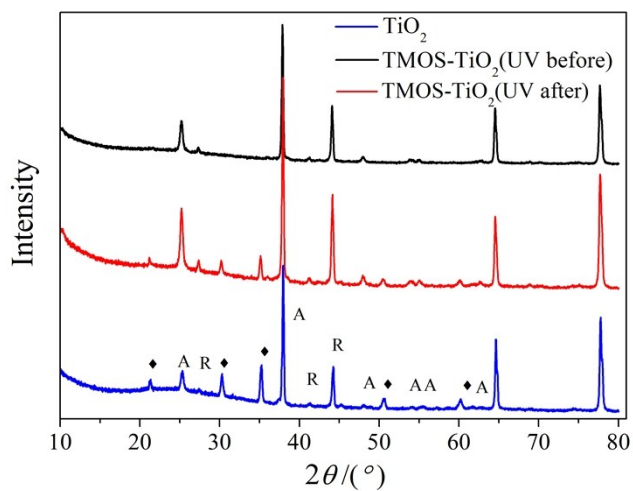
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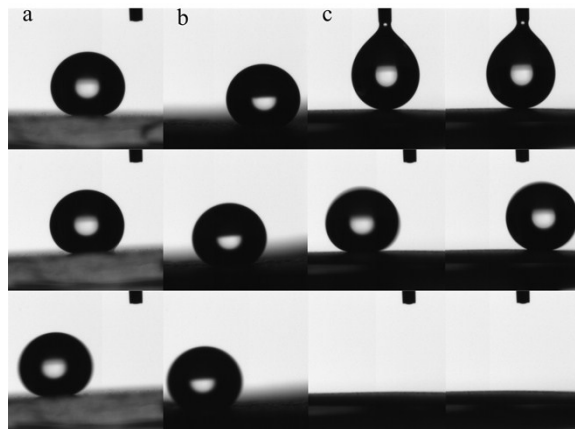
Sample	Atomic concentration (at.%)			
	O	Ti	C	Si
TMOS- $\text{TiO}_2$	33.8	11.0	49.3	5.9
UV irradiated TMOS- $\text{TiO}_2$	61.8	19.9	11.1	7.2



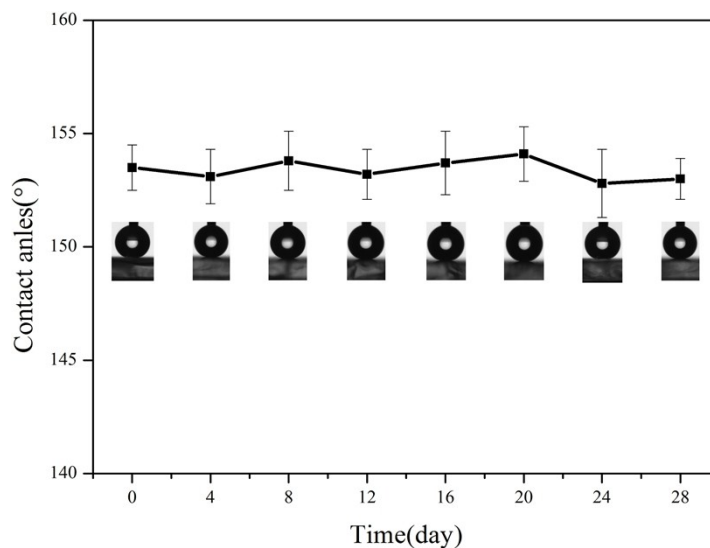
**Figure S4.** XPS spectra of (a) O 1s, (b) Si 2p, (c) Ti 2p and (d) C 1s for the TMOS-TiO<sub>2</sub> coatings before and after UV irradiation for 30 minutes.



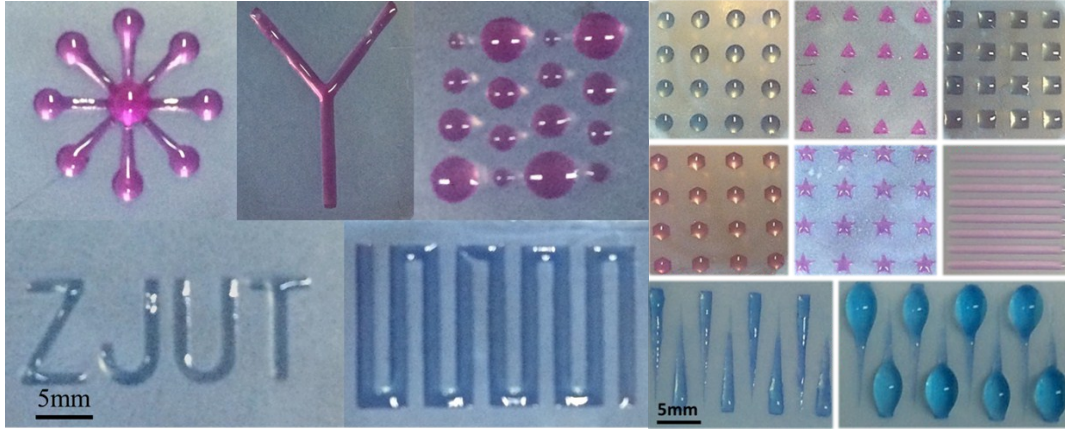
**Figure S5.** XRD patterns of TiO<sub>2</sub> and TMOS-TiO<sub>2</sub> coatings before and after UV irradiation for 30 minutes. (A: anatase; R: rutile).



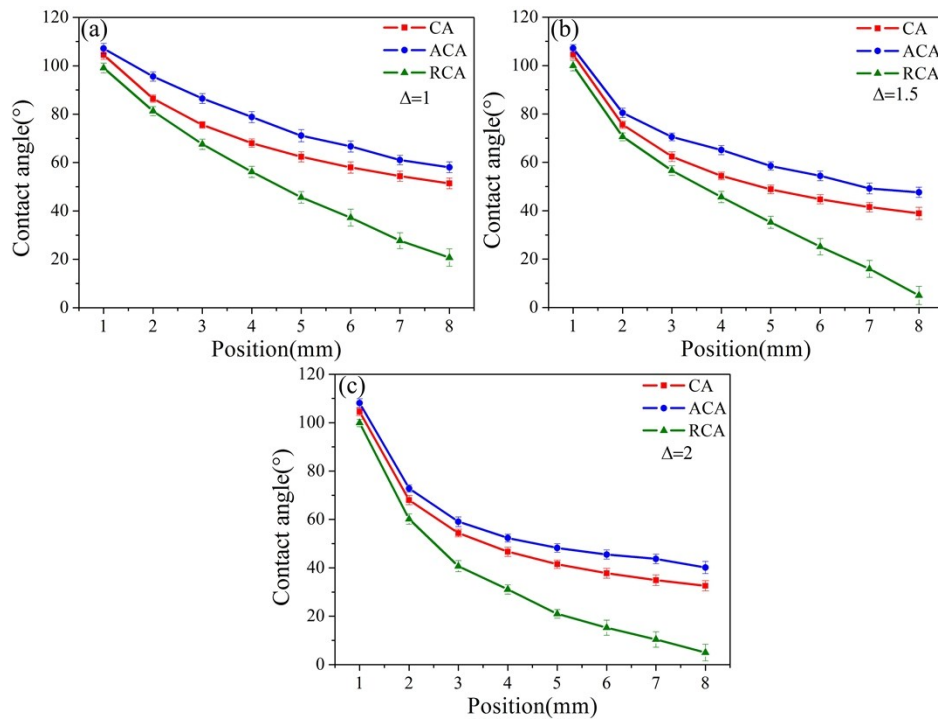
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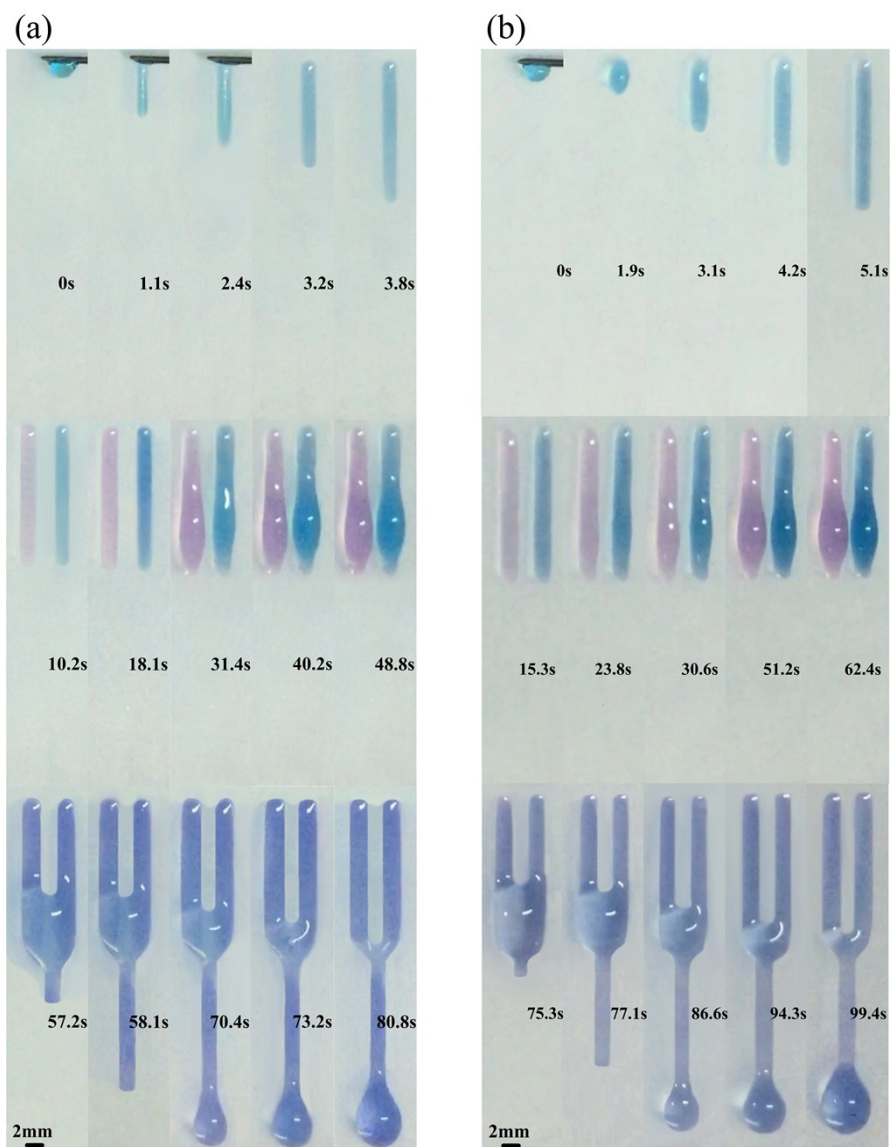
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**Figure S9.** Water contact angles (CAs), advancing contact angles (ACAs) and receding contact angles (RCAs) as functions of positions on three unidirectional channels with the spacing  $P$  between two adjacent stripes of (a) 20  $\mu\text{m}$ , (b) 30  $\mu\text{m}$  and (c) 40  $\mu\text{m}$ .



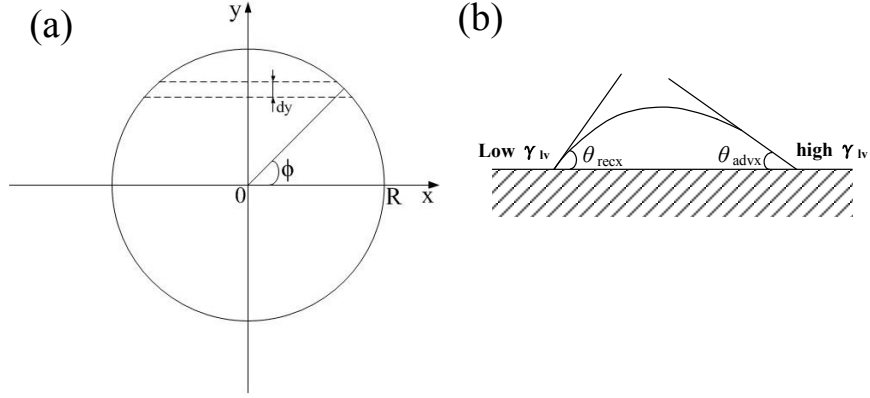
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(a)  $V_{\text{water}}:V_{\text{ethanol}}=2:1$ ; (b)  $V_{\text{water}}:V_{\text{ethanol}}=4:1$ . The scale bar is 2 mm.



## Supplementary Analysis II:

### Droplet motion on wettability-patterned gradient surface



**Figure S11.** Schematic illustration of drop motion

As can be seen from Figure S11, for a thin strip of liquid thickness  $dy$  parallel to the spreading direction, the wettability gradient force ( $F_D$ ) at the  $k$  location which drives the droplet toward more wettable region of the surface can be described as<sup>33,37,38,78</sup>

$$\begin{aligned} F_D &= \gamma_{lv} \int_{-R}^R [(\gamma_{SV} - \gamma_{SL})_n - (\gamma_{SV} - \gamma_{SL})_0] dy \\ &= 2R \int_0^{\frac{\pi}{2}} [(\gamma_{SV} - \gamma_{SL})_n - (\gamma_{SV} - \gamma_{SL})_0] \cos \phi d\phi \end{aligned} \quad \text{S(1)}$$

According to the Young's equation,  $\gamma_{LV} = \frac{\gamma_{SV} - \gamma_{SL}}{\cos \theta}$ , the  $F_D$  can be rewritten as

$$\begin{aligned} F_D &= 2R \int_0^{\frac{\pi}{2}} \gamma_{LV} (\cos \theta_n - \cos \theta_0) \cos \phi d\phi \\ &= 2R \int_0^{\frac{\pi}{2}} \gamma_{LV} (\cos \theta_n - \cos \theta_{n-1} + \cos \theta_{n-1} - \cos \theta_{n-2} + \dots + \cos \theta_1 - \cos \theta_0) \cos \phi d\phi \\ &= 2R \gamma_{LV} \sum_{n=1}^k (\cos \theta_n - \cos \theta_{n-1}) \end{aligned} \quad \text{S(2)}$$

where  $R$  is the base radius of the droplet to contact surface in the  $x$  direction just before unidirectional spread, and  $\gamma_{LV}$  is the surface tension of droplet.  $\theta_n$  corresponds to the apparent

contact angle of droplet on the  $n^{\text{th}}$  wettability pattern of one channel. The similar technique based on Eq. (2) can be applied for the analysis of hysteresis force ( $F_H$ )

$$F_H = 2R\gamma_{lv} \sum_{n=1}^k \int_0^{\frac{\pi}{2}} (\cos \theta_{rn} - \cos \theta_{an}) \cos \phi d\phi = 2R\gamma_{lv} \sum_{n=1}^k (\cos \theta_{rn} - \cos \theta_{an}) \quad , \quad \text{S(3)}$$

where  $\theta_{an}$  and  $\theta_{rn}$  correspond to the advancing contact angle and the receding contact angle on the  $n^{\text{th}}$  wettability pattern of one channel.