## **Supporting Information**

## Multifunctional Ultrathin Aluminum Foil: Oil/Water Separation and Particle Filtration

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**Figure S1. Bright iridescence formed by the regular micropore arrays due to the optical diffraction effect**. (a) The four iridescent patterns taken by different distance from the foils to the camera. The distances are 0, 5, 10, 15 cm, respectively. (b) The iridescent patterns taken by different angles to the optical axis, and the included angles are 0°, 5°, 10°, and 15°, respectively. All the samples are irradiated by white LED from the behind.



Figure S2. Uniformity analysis of the micropores formed by femtosecond laser perforating. (a) is the SEM image of the micropore arrays. The interval of the adjacent pores is 20  $\mu$ m. (b) is the mean diameter of the pores by averaging the X and Y directions in the blue area in (a). (c) is the analysis of the eccentricity of the each pore in the blue area in (a). It can be seen that all the eccentricity is less than 0.1, which means that the pores are very equivalent to roundness. From (b) and (c), it is indicated that regular micropores are arrayed on the aluminum foil surface.



Figure S3. The measurement of the surface roughness of the aluminum foil. (a) The untreated aluminum foil and the surface roughness is ~372.6 nm. (b) The femtosecond laser processed aluminum foil with pore diameter of ~ 8.9  $\mu$ m, and the surface roughness is ~709.9 nm. (c) The aluminum foil with pore size of ~ 14.6  $\mu$ m, and the roughness is ~864.7 nm. (d) The aluminum foil with pore size of ~ 24.8  $\mu$ m, and the roughness is ~1393 nm.



Figure S4. Optical microscope images of the micropores. From (a) to (h), the diameters are 2.4, 4.1, 8.2, 12.2, 15.9, 19.1, 27.7, and 32.2  $\mu$ m, respectively. The results indicate that not only the pores are uniformly distributed, but also the micropores can be tuned by changing the laser pulse energy and pulse numbers.



**Figure S5. Two-Dimensional Fast Fourier transformation (2D-FFT) analysis for the distribution of the micropores**. (a)-(c) depict the Fourier Transform profile of the SEM images in Figure 2(b). It can be seen that the frequency spectrum is distributed into ring and the radius of the ring is diffuse within a small range. This illustrates that the micropores are formed with characteristic periodic distribution in all directions.



Figure S6. Systematic study of the wettability of the micropore arrays. (a) is the water contact angle on micropores with different diameters and intervals. It is indicated that most of the contact angles are less than  $10^{\circ}$ , showing superhydrophilic nature. In addition, the contact angles are decreased with the increasing micropore diameters and decreasing intervals. (b) and (c) are the C<sub>8</sub>H<sub>18</sub> and C<sub>2</sub>H<sub>4</sub>Cl<sub>2</sub> contact angles on micropore arrays. It can be seen that all the contact angles are larger than  $150^{\circ}$ , exhibiting underwater superoleophobic property. From (b) and (c), it is observed that the oil contact angles are increased with the increasing micropore diameters and decreasing intervals. This study illustrates that the wettability can be accurately controlled by changing the micropore diameters and intervals.



Figure S7. Preparation of the oil/water mixtures. From (a) to (c), it can be seen that the undyed water,  $C_8H_{18}$ , and  $C_2H_4Cl_2$  are colorless transparent. The water presents blue color after it is dyed with methylene blue. Meanwhile, the  $C_8H_{18}$  and  $C_2H_4Cl_2$ show red color after dyed with Sudan IV. It is observed from (d) to (f) that the layered oil and water is formed due to  $C_8H_{18}$  is lighter than water while  $C_2H_4Cl_2$  is heavier than water.



**Figure S8. Calculation of the maximum height of the oil layer which can be supported by the aluminum foil**. To assess the separation capability, we calculated the maximum height of the oil layer that the aluminum foil can withstand which is deduced from equations (1) and (2)

$$P_{exp} = \rho g h_{max} \qquad (1)$$

$$P_{theor} = 2\gamma_{OW} \cos \theta_{OW} / d \qquad (2)$$

if the  $P_{exp}$  is equal to  $P_{theor}$ ,  $h_{max}$  can be expressed as

$$h_{\max} = \frac{2\gamma_{OW} \cos_{OW}}{\rho g d} \tag{3}$$

the surface tension  $\gamma_{OW}$  for C<sub>8</sub>H<sub>18</sub> and C<sub>2</sub>H<sub>4</sub>Cl<sub>2</sub> is 21.7 and 28.1 mN/m. The oil contact angles for C<sub>8</sub>H<sub>18</sub> and C<sub>2</sub>H<sub>4</sub>Cl<sub>2</sub> is 10.2° and 10.9°, respectively. In addition, the density  $\rho$  for C<sub>8</sub>H<sub>18</sub> and C<sub>2</sub>H<sub>4</sub>Cl<sub>2</sub> are 0.70 and 1.26 g/cm<sup>3</sup>. g is the gravitational acceleration, and the value is 9.8 N/kg. Hence, the maximum height for different diameters can be calculated, and the representative results can be seen in Figure S7.

Due to the fast and complete discharge of the water and oil from the separator (Figure 4c), the height of the oil layer can not exceed the critical height  $h_{max}$ .

Therefore, the oil/water separation in our experiments can not be affected by the intrusion pressure.

Supporting Information, Movie S1 The separation of light oil  $C_8H_{18}$  and water mixtures.

Supporting Information, Movie S2 The separation of heavy oil  $C_2H_4Cl_2$  and water mixtures.

Supporting Information, Movie S3 The continuous oil/water separation and the recovery of the oil.