### **Supporting Information**

# Hybrid ultramicroporous materials (HUMs) with enhanced stability and trace carbon capture performance

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### **Experimental Procedures**

**Zeolite 13X** was obtained from Sigma-Aldrich. **SIFSIX-3-Ni**,<sup>[1]</sup> **Mg-MOF-74**,<sup>[2]</sup> **UiO-66- NH**<sub>2</sub>,<sup>[3]</sup> **Ni-MOF-74**<sup>[4]</sup> and **HKUST-1**<sup>[5]</sup> were synthesised according to literature procedures.

**Preparation of {**[Ni(pyrazine)<sub>2</sub>(TiF<sub>6</sub>)]<sub>n</sub>**} (TIFSIX-3-Ni).** Nickel hexafluorotitanate (0.500 g, 2.27 mmol) and pyrazine (2.50 g, 31.2 mmol) were dissolved in 1 mL of deionised water and stirred for 48 h at room temperature to yield an as yet uncharacterised polycrystalline precursor of TIFSIX-3-Ni (blue colour powder). The precursor was air dried and heated at 160 °C for 24 h to obtain the desired TIFSIX-3-Ni. Activation of TIFSIX-3-Ni was achieved by degassing the sample on a SmartVacPrep<sup>TM</sup> using dynamic vacuum and heating for 24 h (sample heated from RT to 160 °C with a ramp rate of 10 °C/min).

**Preparation of**  $\{[Ni(pyrazine)_2(NbOF_5)]_n\}$  (NbOFFIVE-1-Ni). The compound NbOFFIVE-1-Ni was synthesised and activated using a reported synthesis method.<sup>[6]</sup> Nickel nitrate hexahydrate (0.175 g, 0.602 mmol), niobium(V) oxide (0.0790 g, 0.297 mmol), pyrazine (0.384 g, 4.79 mmol) and hydrofluoric acid (0.26 mL, aqueous 48%, 7.17 mmol) were added to 3 mL of deionized water in a Teflon bomb and heated at 130 °C for 24 h . Violet coloured crystals were obtained upon cooling the reaction mixture to room temperature. The crystals obtained were washed with methanol to remove any traces of unreacted hydrofluoric acid. Activation of NbOFFIVE-1-Ni was carried out by degassing the methanol-washed sample on a SmartVacPrep<sup>TM</sup> using dynamic vacuum and heating for 24 h (sample heated from RT to 105 °C with a ramp rate of 10 °C/min).

**Powder X-ray Diffraction (PXRD).** Diffractograms were recorded using a PANalytical Empyrean<sup>TM</sup> diffractometer equipped with a PIXcel<sup>3D</sup> detector operating in scanning line detector mode with an active length of 4 utilizing 255 channels. The diffractometer is outfitted with an Empyrean Cu LFF (long fine-focus) HR (9430 033 7310x) tube operated at 40 kV and 40 mA and CuK $\alpha$  radiation ( $\lambda \alpha = 1.540598$  Å) was used for diffraction experiments. Continuous scanning mode with the goniometer in the theta-theta orientation was used to collect the data. Incident beam optics included the Fixed Divergences slit with anti-scatter slit PreFIX module, with a 1/8° divergence slit and a 1/4° anti-scatter slit, as well as a 10 mm fixed incident beam mask and a Soller slit (0.04 rad). Divergent beam optics included a P7.5 anti-scatter slit, a Soller slit (0.04 rad), and a Ni- $\beta$  filter. In a typical experiment, 20 mg of sample was dried, ground into a fine powder and was loaded on a zero

background silicon disks. The data was collected from 5°- 45° (20) with a step-size of 0.02626° and a scan time of 29 seconds per step. Crude data was analysed using the X'Pert HighScore Plus<sup>TM</sup> software V 4.1 (PANalytical, The Netherlands). Plots of stacked PXRD spectra for each adsorbent displaying the diffraction pattern for calculated and as synthesized materials are provided below (Fig. S2-S3). Additional plots of stacked PXRD spectra displaying patterns for calculated, pristine sample, and post-humidity chamber exposure (after 1, 7, and 14 d) are provided for each sorbent. (Fig. S12 and S14)

**Thermogravimetric Analysis (TGA).** Thermograms were recorded under nitrogen using TGA instrument TA Q50 V20.13 Build 39. Platinum pans and a flow rate of 60 mL/min for the nitrogen gas were used for the experiments. The data was collected in the High Resolution Dynamic mode with a sensitivity of 1.0, a resolution of 4.0, and a temperature ramp of 20 °C/min up to 500 °C. The data was evaluated using the T.A. Universal Analysis suite for Windows XP/Vista Version 4.5A. Plots of stacked thermograms for each microporous sorbent are provided below (Fig. S4–S5).

**Gas Sorption Measurements.** Ultra-high-purity grade  $N_2$  and  $CO_2$  were used for gas sorption experiments. Adsorption experiments (up to 1 bar) for different pure gases were performed on Micromeritics TriStar II PLUS and Micromeritics 3 Flex surface area and pore size analyser. Measurements with  $N_2$  at 77 K were conducted on a Micromeritics TriStar II PLUS instrument. Brunauer-Emmett-Teller (BET) surface areas were determined from the  $N_2$  adsorption isotherms at 77 K using the Micromeritics Microactive software except for **NbOFFIVE-1-Ni** and **TIFSIX-3-Ni** whose BET surface areas were determined from the CO<sub>2</sub> adsorption isotherms collected at 298 K. About 200 mg of activated samples were used for the measurements. Very low pressure CO<sub>2</sub> measurements were performed on a Micromeritics 3 Flex surface area and pore size analyser at 273, 283, 293 and 298 K. A Julabo temperature controller was used to maintain a constant temperature in the bath through the duration of the experiment. Samples were degassed on a Smart VacPrep instrument prior to the analysis.

**TGA-Temperature-Programmed Desorption (TPD) Studies.** Gas mixing rig coupled independently with a TGA instrument TA Q50 V20.13 Build 39 and mass spectrometer (MS) Agilent 5975 MSD was used for the TGA-TPD studies, see Fig. S1. A typical test involved activating the sample by heating at desired temperature under a 60 mL/min flow of nitrogen

gas and then cooling it down to 30 °C before the introduction of the desired gas mixture. Gas ratios was controlled and monitored by mass flow controller whereas moisture was introduced by passing the pre-mixed gas mixture through a gas bubbler containing water. Increase in weight was monitored until it began to plateau along with exposure time and gas flow conditions. Composition of the adsorbed species was analysed during the desorption cycle using the mass spectrometer. Custom-made fixed-bed flow system consisting of gas delivery system, a reactor housed in a furnace and a mass spectrometer detection system was used for the TPD experiments. Amount of guest adsorbed and the temperature at which desorption occurs can be figured out using the TPD profiles. A typical CO<sub>2</sub> TPD profile tells us about the amount of CO<sub>2</sub> adsorbed and the range of desorption temperature. It is carried out by placing the sorbent in a quartz tubular reactor and the sample is fixed within it using quartz wool. Helium is passed through the reactor until a constant signal is recorded by the mass spectrometer followed by increase in temperature at the rate of 10 °C/min to the desired temperature so as to remove the impurities. Once the impurities are flushed out, the sample is cooled down to 30 °C and the gas mixture is introduced till the desired loading is obtained. Once the desired adsorption parameters are obtained, gas flow is switched to nitrogen to flush out the excessive CO<sub>2</sub> in the system. Once the CO<sub>2</sub> concentration reaches the background levels, carrier gas is switched to helium (it is not detected by the MS, ensuring that all desorbed species from the adsorbents are detected) and the temperature of the reactor is raised at the rate of 10 °C/min. Composition of the desorbed gas was monitored by MS thus helping us to figure out the identity and quantity of each component present in the desorbed gas.

A typical direct air capture (DAC) test, involves activation of sample as per the reported conditions followed by exposure to the laboratory environment for 24 h. Analysis of the exposed sample is carried out using TPD studies to determine the composition of the adsorbed gas.

Accelerated Stability Protocol. In pharmaceutical industry, there exists a well-established criteria for the determination of a compound's stability to long-term and accelerated storage conditions.<sup>[7]</sup> The procedure incorporates all possible storage conditions from different regions around the globe. Approved as a unified testing condition by International Conference of Harmonization (ICH) it consists of long-term, intermediate and accelerated storage storage conditions valid for the USA, EU and Japan. Proven by Arrhenius equation to be a

valid model, accelerated stability conditions mimic an acceleration of the storage at ambient conditions and accelerated stability testing for 6 months is similar to two years of long-term storage conditions.<sup>[8]</sup> In a typical experiment, pristine sample of the adsorbent under investigation was prepared and placed into an environment where relative humidity temperature and were controlled. To achieve 75% relative humidity at 40 °C, saturated aq. NaCl solution is placed in a desiccator stored at 40 °C. Adsorbents were placed in a separate, open glass vial and stored within the desiccator. They were exposed to this temperature and humidity continuously and aliquots were removed for analysis (PXRD, TGA, and gas sorption) after 1, 7, and 14 d.



Scheme of Thermogravimetric (TGA)-Temperature-Programmed Desorption (TPD).

Figure S1: Schematic of gas mixing system, TGA uptake analysis and TPD analysis units.

# Powder X-ray Diffraction for TIFSIX-3-Ni.



Figure S2: PXRD of TIFSIX-3-Ni.

Powder X-ray Diffraction for NbOFFIVE-1-Ni.



Figure S3: PXRD of NbOFFIVE-1-Ni.

Powder X-ray Diffraction for Mg-MOF-74.



**Figure S4**: PXRD of **Mg-MOF-74** as synthesised and after sorption *vs*. the calculated pattern.

Powder X-ray Diffraction for UiO-66-NH<sub>2</sub>.



Figure S5: PXRD of UiO-66-NH<sub>2</sub> as synthesised and after sorption vs. the calculated pattern.

Powder X-ray Diffraction for HKUST-1.



Figure S6: PXRD of HKUST-1 as synthesised and after sorption vs. the calculated pattern.

Thermogravimetric Analysis for TIFSIX-3-Ni.



Figure S7: TGA of TIFSIX-3-Ni.

### Thermogravimetric Analysis for NbOFFIVE-1-Ni.





Thermogravimetric Analysis for SIFSIX-3-Ni.



Figure S9: TGA of SIFSIX-3-Ni

### CO<sub>2</sub> Sorption Isotherm for TIFSIX-3-Ni.



Figure S10: CO<sub>2</sub> sorption isotherms for TIFSIX-3-Ni.

CO<sub>2</sub> Isosteric Heat of Adsorption for TIFSIX-3-Ni.



Figure S11: CO<sub>2</sub> isosteric heat of adsorption for TIFSIX-3-Ni.



Figure S12:  $CO_2$  (black) and  $N_2$  (red) sorption isotherms for TIFSIX-3-Ni

Sorption Isotherms for NbOFFIVE-1-Ni.



Figure S13:  $CO_2$  (black) and  $N_2$  (red) sorption isotherms for NbOFFIVE-1-Ni.

### **Isosteric Heats of Adsorption Calculations**

The  $Q_{st}$  of CO<sub>2</sub> for TIFSIX-3-Ni, SIFSIX-3-Ni, NbOFFIVE-1-Ni, UiO-66-NH<sub>2</sub>, Zeolite 13X, HKUST-1, Mg-MOF-74 were calculated from the low pressure CO<sub>2</sub> adsorption isotherms collected at 273, 283 and 293 K.

The Clausius-Clapeyron equation was used for the calculation of  $Q_{st}$  where virial-type equations were used to fit ten points in the adsorption data between 0 and 3000 ppm (0.3 mbar) at multiple temperatures (Equation 1). The fit for each of the compounds is shown below. All fitting was performed using Origin Pro 8.

$$\ln P = \ln n + (\frac{1}{T^2}) \sum_{i=0}^{j} a_i n^i + \sum_{i=0}^{k} b_i n^i$$

The  $Q_{\rm st}$  was then calculated from the virial model using Equation 2.

$$-Q_{st} = -R \sum_{i=0}^{j} a_i n^i$$





Figure S14: Fitting of the isotherm data of HKUST-1 to the virial equation.

Parameters	Value	Standard Error
a0	-2769.29899	12.84396
al	-39.83251	13.18102
a2	-18.68377	6.89145
a3	8.48644	3.71636
a4	-1.23229	0.64041
a5	0	0
b0	18.96836	0.04548
b1	0.21259	0.04645
b2	0	0
b3	0	0
Reduced Chi-Sqr	1.77634E-5	
Adj. R-Square	0.99999	

Table S1: Fitting parameters for HKUST-1.





Figure S15: Fitting of the isotherm data of UiO-66-NH<sub>2</sub> to the virial equation.

Demonsterne	XZ-1	Standard France
Parameters	value	Standard Error
	4652 20220	124.02026
au	-4032.39339	134.02030
91	651 0126	491 60026
aı	051.0120	471.00020
a2.	-636 66509	429 18299
a3	224.05882	105.79837
a4	-0.95913	2.45873
a5	0	0
b0	25.81332	0.463
1.1	1.00017	1.6015
61	-1.82217	1.6815
<u> </u>	2 22851	1 42052
02	2.23831	1.43932
b3	_0.79225	0 33345
	-0.19225	0.55545
Reduced Chi-Sar	0.00231	
Adj. R-Square	0.99941	
5 - 1		

Table S2: Fitting parameters for UiO-66-NH<sub>2</sub>.



**Q**<sub>st</sub> Calculation - Virial Fitting for Mg-MOF-74

Figure S16: Fitting of the isotherm data of Mg-MOF-74 to the virial equation.

Table	<b>S3</b> :	Fitting	parameters	for	Mg-	MOF	-74.

Parameters	Value	Standard Error
a0	-5097.16475	18.97529
al	574.65484	82.27637
a2	-321.76928	83.09131
a3	82.79407	17.78506
a4	-17.52221	4.63194
a5	0	0
b0	15.93129	0.06358
b1	-1.50837	0.26696
b2	0.68876	0.23788
b3	0	0
Reduced Chi-Sqr	6.37182E-6	
Adj. R-Square	0.99999	



**Q**<sub>st</sub> Calculation - Virial Fitting for Zeolite 13X

Figure S17: Fitting of the isotherm data of Zeolite 13X to the virial equation.

Table S4: Fitting parameters for Zeolite 13X.

Parameters	Value	Standard Error
a0	-4800.00613	132.39722
al	797.61373	176.85271
a2	-676.20166	219.18557
a3	433.94642	160.8827
a4	-104.16306	40.50343
a5	0	0
b0	19.70324	0.46117
b1	0.19534	0.45833
b2	0	0
b3	0	0
Reduced Chi-Sqr	7.78166E-4	
Adj. R-Square	0.99954	



# **Q**<sub>st</sub> Calculation - Virial Fitting for SIFSIX-3-Ni

Figure S18: Fitting of the isotherm data of SIFSIX-3-Ni to the virial equation.

Table S5: Fitting parameters for SIFSIX-3-Ni.

Parameters	Value	Standard Error
a0	-5275.96689	35.74562
al	-658.17726	87.8135
a2	639.49304	52.52675
a3	-367.67605	26.83061
a4	99.0502	6.83313
a5	0	0
b0	22.41777	0.1273
b1	1.56213	0.31722
b2	-0.15424	0.17365
b3	0	0
Reduced Chi-Sqr	1.94117E-5	
Adj. R-Square	0.99999	



# $Q_{\rm st}$ Calculation - Virial Fitting for TIFSIX-3-Ni



Parameters	Value	Standard Error
a0	-5643.77909	233.09913
al	-3582.12507	699.32213
a2	4493.99446	749.85233
a3	-2281.59589	340.83247
a4	436.56659	55.92704
a5	0	0
b0	25.43248	0.18808
b1	0	0
b2	0	0
b3	0	0
Reduced Chi-Sqr	3.15597E-4	
Adj. R-Square	0.9996	

Table St	6 <sup>.</sup> Fitting	narameters	for	TIFSIX-3-Ni
I abic Su	J. Fuung	parameters	101	111 <sup>-</sup> 51 <b>A-</b> 3-141

## DAC TPD for TIFSIX-3-Ni.



Figure S20: DAC test TPD for TIFSIX-3-Ni

# DAC TPD for NbOFFIVE-1-Ni.



Figure S21: DAC test TPD for NbOFFIVE-1-Ni

### Accelerated Stability Test for TIFSIX-3-Ni.



Figure S22: PXRD for TIFSIX-3-Ni after accelerated stability test.



Figure S23: Sorption for TIFSIX-3-Ni after accelerated stability test.

### Accelerated Stability Test for NbOFFIVE-1-Ni.



Figure S24: PXRD for NbOFFIVE-1-Ni after accelerated stability test.



Figure S25: Sorption for NbOFFIVE-1-Ni after accelerated stability test.

### VT-PXRD for TIFSIX-3-Ni.



Figure S26: VT-PXRD of TIFSIX-3-Ni. This series of diffractograms shows the temperature-induced transformation {rear to front} of the precursor (red: 25 °C) into TIFSIX-3-Ni (orange: 140 °C).

VT-PXRD for SIFSIX-3-Ni.



Figure S27: VT-PXRD of SIFSIX-3-Ni.

#### **Rietveld Fitting of the PXRD Pattern for TIFSIX-3-Ni.**

Powder diffraction data used for structure solution was obtained from beamline i11 at the Diamond Light Source ( $\lambda = 0.82620(6)$  and zero point = -0.0367(1)).<sup>[9]</sup> Due to the high energy X-ray source, two second scans using a positional scanning detector was used to collect data from a powder sample sealed in a 0.6 mm quartz capillary tube. Analysis of the powder data was carried out in GSAS-II;<sup>[10]</sup> the lattice parameters were determined and structure factors obtained by use of the Pawley method. A Monte Carlo/simulated annealing method was used for structure solution using free moving rigid bodies obtained from the Cambridge Structural Database (CSD)<sup>[11]</sup> (CSD refcode: PETWIW = TiF<sub>6</sub>, AHADUI = pyrazine). (See **Table S7** for crystallographic details).



**Figure S28**: Diffractograms for the Rietveld refinement of **TIFSIX-3-Ni**. Inset depicts a more detailed view of the high angle data  $(2\text{\AA} < d < 1\text{\AA})$ 

Table	S7.	Crystal	logran	hic	data	for	TIFSIX	.3-Ni
I able	57.	CI ystan	iograp	me	uata	101	TILDIV	-3-141

Spacegroup	P4/mmm
a (Å)	6.99007(18)
c (Å)	7.81267(21)
V (Å <sup>3</sup> )	381.735(15)
R <sub>p</sub>	0.04482
R <sub>wp</sub>	0.07356
R <sub>bragg</sub>	0.09798
R <sub>exp</sub>	0.01609
Goodness-of-fit	4.58

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