# On the Growth Morphology and Crystallography 

## of Epitaxial $\mathrm{CdTe} / \mathrm{Cu}_{7} \mathrm{Te}_{4}$ Interface

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## Supplymentary Materials

## The detailed NCSL calculation process on the $\mathrm{CdTe} / \mathrm{Cu}_{7} \mathrm{Te}_{4}$ interface

According to the defination of NCSL, the basal vectors of CdTe substrate $\boldsymbol{R}_{\mathbf{S} 1}, \boldsymbol{R}_{\mathbf{S} 2}$ and $\boldsymbol{R}_{\mathbf{F} 1}$,
$\boldsymbol{R}_{\mathbf{F} 2}$ can be written as:

$$
\begin{align*}
& R_{S 1}=a_{1}\left[\begin{array}{l}
1 \\
0
\end{array}\right], R_{S 2}=\frac{\sqrt{2}}{2} a_{1}\left[\begin{array}{l}
0 \\
1
\end{array}\right]  \tag{S1}\\
& R_{F 1}=c\left[\begin{array}{l}
1 \\
0
\end{array}\right], R_{F 2}=\frac{\sqrt{3}}{2} a_{2}\left[\begin{array}{l}
0 \\
1
\end{array}\right] \tag{S2}
\end{align*}
$$

Here, $a_{1}$ and $a_{2}, c$ represents the lattice parameter of CdTe and $\mathrm{Cu}_{7} \mathrm{Te}_{4}$ respectively.

After the rotation process, the vectors $\boldsymbol{R}_{\mathbf{R F} 1}$ and $\boldsymbol{R}_{\mathbf{R F} 2}$ can also be obtained:

$$
\begin{equation*}
\left(R_{R F 1}, R_{R F 2}\right)=(Z / \theta)\left(R_{F 1}, R_{F 2}\right) \tag{S3}
\end{equation*}
$$

Here, $(Z / \theta)$ represents the rotation matrix which can be expressed as:

$$
(Z / \theta)=\left[\begin{array}{cc}
\cos \theta & -\sin \theta  \tag{S4}\\
\sin \theta & \cos \theta
\end{array}\right]
$$

In this case, the Eq. (S3) can be written as:

$$
\left(R_{R F 1}, R_{R F 2}\right)=\left[\begin{array}{cc}
\cos \theta & -\sin \theta  \tag{S5}\\
\sin \theta & \cos \theta
\end{array}\right]\left[\begin{array}{cc}
c & \frac{0}{3} \\
0 & \frac{\sqrt{3}}{2} a_{2}
\end{array}\right]=\left[\begin{array}{cc}
\cos \theta & -\frac{\sqrt{3}}{2} a_{2} \sin \theta \\
\operatorname{csin} \theta & \frac{\sqrt{3}}{2} a_{2} \cos \theta
\end{array}\right]
$$

Therefore,

$$
\begin{equation*}
R_{R F 1}=c\left[\frac{\cos \theta}{\sin \theta}\right], R_{R F 2}=\frac{\sqrt{3}}{2} a_{2}\left[\frac{-\sin \theta}{\cos \theta}\right] \tag{S6}
\end{equation*}
$$

In this case, the NCSL basal vectors $\boldsymbol{V}_{\mathbf{1}}$ and $\boldsymbol{V}_{\mathbf{2}}$ can be expressed as:

$$
\begin{gather*}
V_{1}=m R_{S 1}+n R_{S 2}=a_{1}\left[\begin{array}{c}
m \\
0
\end{array}\right]+\frac{\sqrt{2}}{2} a_{1}\left[\begin{array}{l}
0 \\
n
\end{array}\right]=a_{1}\left[\begin{array}{c}
\frac{m}{2} \\
\frac{\sqrt{2}}{2}
\end{array}\right]  \tag{S7}\\
V_{2}=p R_{R F 1}+q R_{R F 2}=p c\left[\begin{array}{c}
\cos \theta \\
\sin \theta
\end{array}\right]+\frac{\sqrt{3}}{2} q a_{2}\left[\begin{array}{c}
-\sin \theta \\
\cos \theta
\end{array}\right]=\left[\begin{array}{l}
p c \cos \theta-\frac{\sqrt{3}}{2} q a_{2} \sin \theta \\
p c \sin \theta+\frac{\sqrt{3}}{2} q a_{2} \cos \theta
\end{array}\right] \tag{S8}
\end{gather*}
$$

Here, $m, n, p$ and $q$ are all integers. According to the defination of NCSL, $\boldsymbol{V}_{1}$ and $\boldsymbol{V}_{2}$ should be equal, the 2 vectors must have the same vector module and parallel to each other. Therefore, combine the Eq. (S7) and (S8), the following equation can be obtained:

$$
\left\{\begin{array}{l}
m a_{1}=p c \cos \theta-\frac{\sqrt{3}}{2} q a_{2} \sin \theta  \tag{S9}\\
\frac{\sqrt{2}}{2} n a_{1}=p c \sin \theta+\frac{\sqrt{3}}{2} q a_{2} \cos \theta
\end{array}\right.
$$

From Eq. (S9), the expressions of $\tan \theta, \Sigma$ and the relationship between the 4 integers can be obtained accordingly:

$$
\left\{\begin{array}{l}
m^{2} a_{1}^{2}+\frac{1}{2} n^{2} a_{1}^{2}=p^{2} c^{2}+\frac{3}{4} q^{2} a_{2}^{2}  \tag{S10}\\
\tan \theta=\frac{2 \sqrt{2} n p c-2 \sqrt{3} m q a_{2}}{4 m p c+\sqrt{6} n q a_{2}} \\
\Sigma=\frac{V_{\text {Super }}}{V_{\text {Unit }}}=\frac{4 p^{2} c^{2}+3 q^{2} a_{2}^{2}}{2 \sqrt{3} a_{2} c}
\end{array}\right.
$$

According to the TEM results in Fig. 2, the parallel relationship of ${ }^{(1 \overline{1} 1)}{ }_{C d T e} / /(0001){ }_{C u_{7} T e}$ can be obtained. In addition, it is also noticed that the interplanar distance of ${ }^{(0001)}{ }_{C u_{7}{ }_{7} e_{4}}(0.7211$ $\mathrm{nm})$ is very close to that of ${ }^{(0110)}{ }_{C u_{7} T e}(0.7218 \mathrm{~nm})$. This means that the established $\mathrm{Cu}_{7} \mathrm{Te}_{4}$ unit cell is similar to square. To simplify the calculation, the following relations can be set:

$$
\left\{\begin{array}{l}
\frac{\sqrt{3}}{3} a_{1}=\frac{1}{2} c  \tag{S11}\\
c=\frac{\sqrt{3}}{2} a_{2}
\end{array}\right.
$$

In this case, Eq. (S10) can be simplified to be:

$$
\left\{\begin{array}{l}
\frac{3}{4} m^{2}+\frac{3}{8} n^{2}=p^{2}+q^{2}  \tag{S12}\\
\tan \theta=\frac{\sqrt{2} n p-2 m q}{2 m p+\sqrt{2} n q} \\
\Sigma=\frac{V_{\text {Super }}}{V_{\text {Unit }}}=p^{2}+q^{2}
\end{array}\right.
$$

Under the principle that the value of the 4 integers should be as small as possible, the calculation results are summarized in Table S1. The rotation angle of $\pm 54.74^{\circ}$ and $\pm 35.26^{\circ}$ refer to the variant 1 and 2 of $\mathrm{Cu}_{7} \mathrm{Te}_{4}$ respectively. The same $\Sigma$ values suggest the equivalent status of the COR obtained by applying the rotation along the 4 rotation angles.

Table S1 The calculation results of the $\mathrm{CdTe} / \mathrm{Cu}_{7} \mathrm{Te}_{4}$ interface

| $m$ | $n$ | $p$ | $q$ | $\tan \theta$ | $\theta$ | $\Sigma$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2 | 4 | 3 | 0 | $\sqrt{2}$ | $54.74^{\circ}$ | 9 |
| -2 | 4 | 3 | 0 | $-\sqrt{2}$ | $-54.74^{\circ}$ | 9 |
| 2 | 4 | 0 | 3 | $-\frac{\sqrt{2}}{2}$ | $-35.26^{\circ}$ | 9 |
| -2 | 4 | 0 | 3 | $\frac{\sqrt{2}}{2}$ | $35.26^{\circ}$ | 9 |

