## **Supporting Information**

## A Theoretical Study on Anion Sensing Mechanism of Multi-phosphonium Triarylboranes: Intramolecular Charge Transfer and Configurational Changes

Haamid R. Bhat<sup>‡</sup> and Prakash C. Jha\*<sup>†</sup>

<sup>‡</sup> Computational Chemistry Laboratory, School of Chemical Sciences, Central University of Gujarat, Gandhinagar, India, 382030.

<sup>†</sup> Centre for Applied Chemistry, Central University of Gujarat, Gandhinagar, India, 382030.

\*Corresponding author. Tel.: +91 886 682 3510

E-mail address: prakash.jha@cug.ac.in

| angles (in deg | gree) for the Ful | ly Optimized Stru     | ictures of I and Z a | at CAM-B3L Y P/6-3 | G(a) level     |
|----------------|-------------------|-----------------------|----------------------|--------------------|----------------|
| parame         | ter               | <b>1</b> <sup>a</sup> | 1 <sup>b</sup>       | 2 <sup>a</sup>     | 2 <sup>b</sup> |
| B1 C           | 22                | 1.595                 | 1.582                | 1.591              | 1.577          |
| B1 C           | 10                | 1.574                 | 1.571                | 1.591              | 1.574          |
| B1 C           | 18                | 1.574                 | 1.572                | 1.566              | 1.574          |
| P26 C          | 27                | 1.782                 | 1.764                | 1.784              | 1.771          |
| P30 C          | 215               |                       |                      | 1.784              | 1.769          |
| C2 B1          | C10               | 119.1                 | 119.1                | 118.1              | 122.7          |
| C10 B1         | C18               | 121.6                 | 121.5                | 120.9              | 118.8          |
| C2 B1          | C18               | 119.1                 | 119.3                | 120.9              | 118.4          |
| C7 P26         | H29               | 110.1                 | 110.6                | 109.9              | 110.8          |
| C7 P26         | H28               | 112.3                 | 112.6                | 112.6              | 112.0          |
| C7 P26         | H27               | 113.4                 | 115.5                | 113.1              | 114.9          |
| C4 C2          | B1                | 120.5                 | 121.2                | 119.6              | 121.6          |
| C3 C2          | B1                | 120.4                 | 121.3                | 121.2              | 120.7          |
|                |                   |                       |                      |                    |                |

Table S1: Calculated Important Geometrical Parameters i.e, Bond lengths (in Å) and Bond angles (in degree) for the Fully Optimized Structures of **1** and **2** at CAM-B3LYP/6-31G(d) level

| C10 | B1   | 121.7   | 122.4  | 121.2  | 120.8  |
|-----|--|---|--|--|--|
| C10 | B1   | 120.4   | 120.8  | 119.6  | 121.6  |
| C18 | B1   | 120.4   | 120.8  | 121.0  | 121.4  |
| C18 | B1   | 121.7   | 122.3  | 121.1  | 121.7  |
| C4  | C2   |   |  | 122.7  | 121.5  |
| C3  | C2   |   |  | 122.6  | 122.7  |
| C4  | C2   | 122.4   | 122.1  |  |  |
| C3  | C2   | 122.6   | 122.1  |  |  |
| C11 | C10  |   |  | 122.5  | 122.6  |
| C12 | C10  |   |  | 122.8  | 121.5  |
| C12 | C10  | 122.8   | 120.1  |  |  |
| C11 | C10  | 122.7   | 121.5  |  |  |
| C20 | C18  |   |  | 123.0  | 120.1  |
| C19 | C18  |   |  | 123.0  | 119.9  |
| C20 | C18  | 122.6   | 121.6  |  |  |
| C19 | C18  | 122.8   | 120.1  |  |  |
| C7  | P26  | 119.5   | 119.8  | 119.5  | 119.9  |
| C7  | P26  | 120.0   | 120.4  | 120.0  | 120.5  |
| C15 | P30  | 119.9   | 120.4  |  |  |
| C15 | P30  | 119.6   | 119.8  |  |  |
|     | C10<br>C10<br>C18<br>C18<br>C4<br>C3<br>C4<br>C3<br>C11<br>C12<br>C12<br>C12<br>C12<br>C12<br>C12<br>C19<br>C20<br>C19<br>C7<br>C7<br>C7<br>C15<br>C15 | C10B1C10B1C18B1C18B1C4C2C3C2C4C2C3C2C11C10C12C10C12C10C11C10C12C10C11C10C12C10C11C10C12C10C11C10C11C10C12C10C11C10C12C110C13P26C15P30C15P30 | C10B1121.7C10B1120.4C18B1121.7C4C2C3C2C4C2122.4C3C2122.6C11C10C12C10122.8C11C10122.7C20C18C19C18122.6C19C18122.8C7P26119.5C7P26120.0C15P30119.9C15P30119.6 | C10B1121.7122.4C10B1120.4120.8C18B1121.7122.3C4C2C3C2C4C2122.4122.1C3C2122.6122.1C1C10C12C10122.8120.1C11C10122.7121.5C20C18C19C18122.6121.6C19C18122.8120.1C7P26119.5119.8C7P26120.0120.4C15P30119.9120.4 | C10       B1       121.7       122.4       121.2         C10       B1       120.4       120.8       119.6         C18       B1       120.4       120.8       121.0         C18       B1       121.7       122.3       121.1         C4       C2         122.7         C3       C2         122.6         C4       C2       122.4       122.1          C3       C2       122.6       122.1          C3       C2       122.6       122.1          C11       C10        122.5       122.1          C12       C10        122.8       120.1          C11       C10       122.7       121.5        123.0         C12       C10       122.7       121.5        123.0         C12       C10       122.7       121.5        123.0         C19       C18       122.6       121.6        123.0         C19       C18       122.8       120.1        12 |

Table S2: Calculated Important Geometrical Parameters i.e, Bond lengths (in Å) and Bond angles (in degree) for the Fully Optimized Structures of **3** at CAM-B3LYP/6-31G(d) level; the Corresponding X-ray data<sup>1</sup>(in parentheses)

| concepting in ray and | a (in parentileses)   |                |
|-----------------------|-----------------------|----------------|
| parameter             | <b>3</b> <sup>a</sup> | 3 <sup>b</sup> |
| B1 C2                 | 1.585 (1.584)         | 1.605          |
| B1 C10                | 1.585                 | 1.560          |
| B1 C18                | 1.585                 | 1.560          |
| P26 C7                | 1.787 (1.792)         | 1.780          |
| P30 C15               | 1.787                 | 1.782          |
| P58 C23               | 1.787                 | 1.782          |
|                       |                       |                |

| C2  | B1  | C10 | 120.0 (120.0) | 118.8 |
|-----|-----|-----|---------------|-------|
| C10 | B1  | C18 | 119.9         | 122.3 |
| C2  | B1  | C18 | 119.9         | 118.9 |
| C7  | P26 | H29 | 110.0 (111.0) | 110.1 |
| C7  | P26 | H28 | 112.0         | 112.4 |
| C7  | P26 | H27 | 113.0         | 113.6 |
| C5  | C7  | P26 | 119.5         | 119.6 |
| C6  | C7  | P26 | 119.9         | 120.1 |
| C13 | C15 | P30 | 120.0         | 120.2 |
| C14 | C15 | P30 | 119.4         | 119.6 |
| C22 | C23 | P58 | 119.9         | 120.2 |
| C21 | C23 | P58 | 119.5         | 119.6 |
| C4  | C2  | B1  | 120.4         | 120.5 |
| C3  | C2  | B1  | 120.4         | 120.5 |
| C11 | C10 | B1  | 120.4         | 123.3 |
| C12 | C10 | B1  | 120.4         | 119.5 |
| C19 | C18 | B1  | 120.4         | 119.5 |
| C20 | C18 | B1  | 120.4         | 123.3 |
| C38 | C4  | C2  | 122.9         | 122.1 |
| C34 | C3  | C2  | 122.9         | 122.2 |
| C42 | C11 | C10 | 122.8         | 122.3 |
| C46 | C12 | C10 | 122.9         | 121.0 |
| C50 | C19 | C18 | 122.9         | 121.0 |
| C54 | C20 | C18 | 122.8         | 122.3 |
|     |     |     |               |       |

Table S3: Calculated Important Geometrical Parameters i.e, Bond lengths (in Å) and Bond angles (in degree) for the Fully Optimized Structures of 1F and 2F at CAM-B3LYP/6-31G(d) Level

| Dever |       |                 |                 |                 |                 |
|-------|-------|-----------------|-----------------|-----------------|-----------------|
| para  | meter | 1F <sup>a</sup> | 1F <sup>b</sup> | 2F <sup>a</sup> | 2F <sup>b</sup> |
| B1    | C2    | 1.678           | 1.681           | 1.660           | 1.657           |
| B1    | C10   | 1.664           | 1.671           | 1.672           | 1.665           |

| B1 C18   | 3   | 1.665 | 1.667 | 1.674 | 1.676 |
|----------|-----|-------|-------|-------|-------|
| P26 C7   | ,   | 1.771 | 1.764 |       |       |
| P26 C1:  | 5   |       |       | 1.772 | 1.774 |
| B1 F62   | ,   | 1.460 | 1.461 | 1.454 | 1.454 |
| P38 C23  | 3   |       |       | 1.773 | 1.775 |
| C2 B1 C  | 210 | 113.8 | 114.9 | 114.6 | 115.6 |
| C10 B1 0 | C18 | 115.3 | 117.4 | 113.9 | 114.9 |
| C2 B1 C  | 218 | 114.1 | 115.6 | 114.7 | 112.8 |
| C7 P26 H | H29 | 110.3 | 110.8 |       |       |
| C7 P26 H | H28 | 112.8 | 113.9 |       |       |
| C7 P26 H | H27 | 114.6 | 115.5 |       |       |
| C15 P26  | H27 |       |       | 111.4 | 111.2 |
| C15 P26  | H28 |       |       | 114.8 | 114.6 |
| C15 P26  | H29 |       |       | 111.3 | 111.3 |
| C23 P38  | H31 |       |       | 114.5 | 114.3 |
| C23 P38  | H32 |       |       | 112.6 | 112.4 |
| C23 P38  | H33 |       |       | 110.4 | 110.4 |
| C4 C2 I  | B1  | 125.6 | 124.9 | 126.2 | 125.8 |
| C3 C2 I  | B1  | 117.5 | 118.3 | 117.8 | 118.1 |
| C11 C10  | B1  | 126.3 | 127.0 | 117.2 | 116.9 |
| C12 C10  | B1  | 117.8 | 118.2 | 125.8 | 125.9 |
| C19 C18  | B1  | 126.0 | 126.4 | 117.7 | 118.3 |
| C20 C18  | B1  | 118.1 | 119.7 | 125.3 | 126.8 |
| C34 C4   | C2  | 123.5 | 124.3 |       |       |
| C30 C3   | C2  | 123.2 | 124.0 |       |       |
| C42 C4   | C2  |       |       | 123.5 | 123.6 |
| C46 C3   | C2  |       |       | 123.1 | 123.4 |
| C34 C12  | C10 |       |       | 123.6 | 123.7 |
| C42 C12  | C10 | 122.8 | 123.4 |       |       |
| C38 C11  | C10 | 123.4 | 124.1 | 123.2 | 123.1 |
| C54 C19  | C18 |       |       | 123.2 | 123.7 |

| C58 | C20 | C18 |       |       | 123.8 | 124.6 |
|-----|-----|-----|-------|-------|-------|-------|
| C50 | C20 | C18 | 123.0 | 123.8 |       |       |
| C46 | C19 | C18 | 123.5 | 124.2 |       |       |
| C5  | C7  | P26 | 119.8 | 120.3 |       |       |
| C6  | C7  | P26 | 120.6 | 121.1 |       |       |
| C13 | C15 | P26 |       |       | 120.2 | 120.1 |
| C14 | C15 | P26 |       |       | 120.2 | 120.2 |
| C21 | C23 | P30 |       |       | 120.6 | 120.5 |
| C22 | C23 | P30 |       |       | 119.8 | 119.7 |
| C2  | B1  | F62 | 102.7 | 103.3 | 104.8 | 106.2 |
| C10 | B1  | F62 | 104.5 | 105.1 | 103.5 | 103.7 |
| C18 | B1  | F62 | 104.2 | 104.9 | 103.2 | 101.5 |
|     |     |     |       |       |       |       |

Table S4: Calculated Important Geometrical Parameters i.e, Bond lengths (in Å) and Bond angles (in degree) for the Fully Optimized Structures of **3F** at CAM-B3LYP/6-31G(d) level

| parameter  | 3F <sup>a</sup> | 3F <sup>b</sup> |
|------------|-----------------|-----------------|
| B1 C2      | 1.669           | 1.670           |
| B1 C10     | 1.669           | 1.663           |
| B1 C18     | 1.669           | 1.666           |
| P26 C7     | 1.774           | 1.776           |
| P30 C15    | 1.775           | 1.776           |
| P58 C23    | 1.775           | 1.776           |
| B1 F62     | 1.449           | 1.448           |
| C2 B1 C10  | 114.6           | 115.5           |
| C10 B1 C18 | 114.5           | 115.4           |
| C2 B1 C18  | 114.4           | 112.7           |
| C7 P26 H29 | 111.1           | 111.0           |
| C7 P26 H28 | 111.6           | 114.3           |
| C7 P26 H27 | 114.5           | 111.6           |

| C5  | C7  | P26 | 120.1 | 120.2 |
|-----|-----|-----|-------|-------|
| C6  | C7  | P26 | 120.3 | 120.1 |
| C13 | C15 | P30 | 120.3 | 120.2 |
| C14 | C15 | P30 | 120.0 | 120.0 |
| C22 | C23 | P58 | 120.2 | 120.3 |
| C21 | C23 | P58 | 120.1 | 119.9 |
| C4  | C2  | B1  | 125.6 | 127.2 |
| C3  | C2  | B1  | 117.3 | 117.8 |
| C11 | C10 | B1  | 125.6 | 125.7 |
| C12 | C10 | B1  | 117.3 | 117.0 |
| C19 | C18 | B1  | 125.5 | 125.1 |
| C20 | C18 | B1  | 117.3 | 117.6 |
| C38 | C4  | C2  | 123.7 | 124.7 |
| C34 | C3  | C2  | 123.4 | 123.7 |
| C42 | C11 | C10 | 123.7 | 123.7 |
| C46 | C12 | C10 | 123.4 | 123.3 |
| C50 | C19 | C18 | 123.7 | 123.7 |
| C54 | C20 | C18 | 123.4 | 123.7 |
| C2  | B1  | F62 | 103.7 | 102.0 |
| C10 | B1  | F62 | 103.7 | 104.0 |
| C18 | B1  | F62 | 103.8 | 105.1 |

| Table S5: Calculated Important Geometrical Parameters i.e, Bond lengths (in Å) and Bond |
|---|
| angles (in degree) for the Fully Optimized Structures of 1CN and 2CN at CAM-B3LYP/6-    |
| 31G(d) level  |

| 510(4)10 |        |                  |                  |                  |                  |
|----------|--------|------------------|------------------|------------------|------------------|
| para     | imeter | 1CN <sup>a</sup> | 1CN <sup>b</sup> | 2CN <sup>a</sup> | 2CN <sup>b</sup> |
| B1       | C2     | 1.681            | 1.670            | 1.669            | 1.665            |
| B1       | C10    | 1.672            | 1.658            | 1.677            | 1.671            |
| B1       | C18    | 1.673            | 1.654            | 1.679            | 1.678            |
| P26      | C7     | 1.773            | 1.717            |                  |                  |
|          |        |                  |                  |                  |                  |

| P26  | 6 C1  | 5   |       |       | 1.777 | 1.776 |
|------|-------|-----|-------|-------|-------|-------|
| B1   | C62   | 2   | 1.625 | 1.673 | 1.622 | 1.622 |
| P30  | ) C23 | 3   |       |       | 1.775 | 1.774 |
| C2   | B1 C  | C10 | 114.5 | 118.7 | 114.9 | 115.9 |
| C10  | B1 (  | C18 | 115.1 | 115.5 | 114.3 | 115.2 |
| C2   | B1 C  | C18 | 114.3 | 106.4 | 114.7 | 112.7 |
| C7 I | P26 I | H29 | 111.1 | 110.2 |       |       |
| C7 I | P26 I | H28 | 111.8 | 110.0 |       |       |
| C7 I | P26 I | H27 | 114.5 | 113.7 |       |       |
| C15  | P26   | H27 |       |       | 111.7 | 111.8 |
| C15  | P26   | H28 |       |       | 114.4 | 114.3 |
| C15  | P26   | H29 |       |       | 110.9 | 110.8 |
| C23  | P30   | H31 |       |       | 114.3 | 114.3 |
| C23  | P30   | H32 |       |       | 112.3 | 111.7 |
| C23  | P30   | H33 |       |       | 110.6 | 110.8 |
| C4   | C2 1  | B1  | 123.8 | 126.6 | 124.4 | 124.0 |
| C3   | C2 1  | B1  | 119.8 | 117.5 | 119.9 | 120.1 |
| C11  | C10   | B1  | 124.5 | 124.1 | 119.5 | 118.9 |
| C12  | C10   | B1  | 119.8 | 119.9 | 124.0 | 124.3 |
| C19  | C18   | B1  | 124.1 | 122.7 | 119.8 | 121.2 |
| C20  | C18   | B1  | 120.3 | 119.5 | 123.6 | 124.8 |
| C42  | C4    | C2  |       |       | 124.1 | 124.1 |
| C46  | C3    | C2  |       |       | 123.9 | 124.3 |
| C34  | C4    | C2  | 124.1 | 123.6 |       |       |
| C30  | C3    | C2  | 123.9 | 123.2 |       |       |
| C42  | C12   | C10 | 123.7 | 123.7 |       |       |
| C38  | C11   | C10 | 124.0 | 124.1 | 124.0 | 123.9 |
| C34  | C12   | C10 |       |       | 124.2 | 124.3 |
| C54  | C19   | C18 |       |       | 124.1 | 124.5 |
| C58  | C20   | C18 |       |       | 124.4 | 124.9 |
| C50  | C20   | C18 | 123.9 | 123.6 |       |       |

| C46 | C19 | C18 | 124.1 | 123.9 |       |       |
|-----|-----|-----|-------|-------|-------|-------|
| C5  | C7  | P26 | 120.3 | 121.7 |       |       |
| C6  | C7  | P26 | 120.5 | 121.3 |       |       |
| C13 | C15 | P26 |       |       | 120.1 | 120.0 |
| C14 | C15 | P26 |       |       | 120.5 | 120.5 |
| C21 | C23 | P30 |       |       | 120.6 | 121.5 |
| C22 | C23 | P30 |       |       | 120.0 | 120.8 |
| C2  | B1  | C62 | 102.8 | 105.1 | 104.3 | 106.2 |
| C10 | B1  | C62 | 103.9 | 105.9 | 103.1 | 102.9 |
| C18 | B1  | C62 | 103.9 | 103.6 | 103.3 | 101.7 |
|     |     |     |       |       |       |       |

Table S6: Calculated Important Geometrical Parameters i.e, Bond lengths (in Å) and Bond angles (in degree) for the Fully Optimized Structures of **3**CN at CAM-B3LYP/6-31G(d) level

| parameter  | 3CN <sup>a</sup> | 3CN <sup>b</sup> |
|------------|------------------|------------------|
| B1 C2      | 1.675            | 1.672            |
| B1 C10     | 1.675            | 1.654            |
| B1 C18     | 1.674            | 1.677            |
| P26 C7     | 1.776            | 1.777            |
| P30 C15    | 1.776            | 1.729            |
| P58 C23    | 1.776            | 1.777            |
| B1 C62     | 1.619            | 1.621            |
| C2 B1 C10  | 114.5            | 111.4            |
| C10 B1 C18 | 114.7            | 116.5            |
| C2 B1 C18  | 114.5            | 115.3            |
| C7 P26 H29 | 111.6            | 111.9            |
| C7 P26 H28 | 111.1            | 110.7            |
| C7 P26 H27 | 114.2            | 114.2            |
| C5 C7 P26  | 120.3            | 120.5            |
| C6 C7 P26  | 120.3            | 120.1            |
|            |                  |                  |

| C13 C15 | P30 | 120.0 | 124.0 |
|---------|-----|-------|-------|
| C14 C15 | P30 | 120.6 | 124.1 |
| C22 C23 | P58 | 120.2 | 120.3 |
| C21 C23 | P58 | 120.3 | 120.2 |
| C4 C2   | B1  | 123.9 | 123.8 |
| C3 C2   | B1  | 119.5 | 119.5 |
| C11 C10 | B1  | 123.8 | 126.1 |
| C12 C10 | B1  | 119.5 | 122.3 |
| C19 C18 | B1  | 123.8 | 124.1 |
| C20 C18 | B1  | 119.5 | 119.1 |
| C38 C4  | C2  | 124.3 | 124.4 |
| C34 C3  | C2  | 124.3 | 124.2 |
| C42 C11 | C10 | 124.3 | 124.3 |
| C46 C12 | C10 | 124.2 | 123.7 |
| C50 C19 | C18 | 124.3 | 124.4 |
| C54 C20 | C18 | 124.2 | 124.0 |
| C2 B1   | C62 | 103.5 | 106.1 |
| C10 B1  | C62 | 103.6 | 103.1 |
| C18 B1  | C62 | 103.6 | 102.5 |

| Table S7: The NPA Charge Distribution on Some Crucial Atoms of 1-3,  | 1CN-3CN and 1F- |
|--|-----------------|
| <b>3F</b> in $S_0$ Calculated at CAM-B3LYP/6-31G(d) Level of Theory. |                 |

| Molecule | NPA charge distribution (Atom involved) |                |                 |                 |                |        |
|----------|---|----------------|-----------------|-----------------|----------------|--------|
| 1        | 0.933<br>(B1)                           | -0.336<br>(C2) | -0.426<br>(C10) | -0.426<br>(C18) | 0.861<br>(P26) |        |
| 1CN      | 0.274                                   | -0.176         | -0.252          | -0.255          | 0.865          | 0.169  |
|          | (B1)                                    | (C2)           | (C10)           | (C18)           | (P26)          | (C62)  |
| 1F       | 0.757                                   | -0.216         | -0.298          | -0.300          | 0.866          | -0.556 |
|          | (B1)                                    | (C2)           | (C10)           | (C18)           | (P26)          | (F62)  |

| 2          | 0.941<br>(B1) | -0.350<br>(C2) | -0.350<br>(C10) | -0.445<br>(C18) | 0.861<br>(P26) |        |
|------------|---------------|----------------|-----------------|-----------------|----------------|--------|
| 2CN        | 0.272         | -0.260         | -0.183          | -0.186          | 0.865          | 0.162  |
|            | (B1)          | (C2)           | (C10)           | (C18)           | (P26)          | (C62)  |
| <b>2</b> F | 0.756         | -0.308         | -0.225          | -0.227          | 0.865          | -0.552 |
|            | (B1)          | (C2)           | (C10)           | (C18)           | (P26)          | (F62)  |
| 3          | 0.965<br>(B1) | -0.371<br>(C2) | -0.372<br>(C10) | -0.371<br>(C18) | 0.859<br>(P26) |        |
| 3CN        | 0.271         | -0.193         | -0.193          | -0.193          | 0.864          | 0.155  |
|            | (B1)          | (C2)           | (C10)           | (C18)           | (P26)          | (C62)  |
| 3F         | 0.756         | -0.236         | -0.236          | -0.236          | 0.864          | -0.548 |
|            | (B1)          | (C2)           | (C10)           | (C18)           | (P26)          | (F62)  |

Table S8: Calculated free energy changes ( $\Delta G$ ) for various Addition Products using CAM-B3LYP/6-31G(d) Level of Theory with Basis Set Superposition Error (BSSE) Corrections.

| Molecule             | ΔG (Kcal/mol) |
|----------------------|---------------|
| 1CN                  | -9.56         |
| 1 <b>F</b>           | -59.99        |
| 1Br                  | 21.73         |
| 1Cl                  | 28.22         |
| 1CH <sub>3</sub> COO | 4.08          |
| 1NO <sub>3</sub>     | 18.96         |
| 1HSO <sub>4</sub>    | 26.89         |
| 2CN                  | -17.43        |
| <b>2</b> F           | -69.52        |
| 2Br                  | 12.90         |
| <b>2</b> Cl          | 19.60         |
| 2CH <sub>3</sub> COO | 3.01          |
| 2NO <sub>3</sub>     | 10.93         |
| 2HSO <sub>4</sub>    | 19.61         |
| 3CN                  | -23.19        |

| <b>3</b> F              | -75.14 |
|-------------------------|--------|
| 3Br                     | 8.09   |
| <b>3Cl</b>              | 13.50  |
| 3CH <sub>3</sub> COO    | 10.55  |
| <b>3NO</b> <sub>3</sub> | 5.63   |
| 3HSO <sub>4</sub>       | 15.1   |

Table S9: Hybrids of **1-3**, **1CN-3CN** and **1F-3F** in Ground State Calculated by Employing the CAM-B3LYP/6-31G(d) Level of Theory.

| Molecule     | Lewis-type<br>NBOs          | Hybrid <sup>a</sup>                  | AO (%) <sup>b</sup>          |
|--------------|-----------------------------|--------------------------------------|------------------------------|
|              | $\sigma\left(B1-C2\right)$  | $sp^{2.11}d^0$                       | s(32.12%) p(67.78%) d(0.10%) |
| 1            | $\sigma\left(B1-C10\right)$ | sp <sup>1.95</sup> d <sup>0</sup>    | s(33.91%) p(66.00%) d(0.09%) |
|              | $\sigma\left(B1-C18\right)$ | $sp^{1.95}d^{0}$                     | s(33.92%) p(65.99%) d(0.09%) |
|              | σ (B1 – C2)                 | sp <sup>2.95</sup> d <sup>0</sup>    | s(25.26%) p(74.64%) d(0.10%) |
| 1 <i>C</i> N | $\sigma\left(B1-C10\right)$ | $sp^{2.78}d^{0}$                     | s(26.46%) p(73.45%) d(0.09%) |
| ICN          | $\sigma\left(B1-C18\right)$ | $sp^{2.77}d^{0}$                     | s(26.51%) p(73.40%) d(0.09%) |
|              | $\sigma\left(B1-C62\right)$ | sp <sup>3.58</sup> d <sup>0.01</sup> | s(21.79%) p(78.09%) d(0.12%) |
|              | $\sigma \left( B1-C2 ight)$ | $sp^{2.67}d^{0}$                     | s(27.18%) p(72.70%) d(0.12%) |
| 16           | $\sigma\left(B1-C10\right)$ | $sp^{2.51}d^{0}$                     | s(28.46%) p(71.43%) d(0.11%) |
| IF           | $\sigma\left(B1-C18\right)$ | $sp^{2.49}d^{0}$                     | s(28.62%) p(71.27%) d(0.11%) |
|              | $\sigma\left(B1-F62\right)$ | sp <sup>3.43</sup> d <sup>0.01</sup> | s(21.80%) p(78.10%) d(0.10%) |
|              | $\sigma \left( B1-C2 ight)$ | sp <sup>2.06</sup> d <sup>0</sup>    | s(32.67%) p(67.23%) d(0.10%) |
| 2            | $\sigma\left(B1-C10\right)$ | $sp^{2.06}d^{0}$                     | s(32.67%) p(67.23%) d(0.10%) |
|              | $\sigma\left(B1-C18\right)$ | $sp^{1.89}d^{0}$                     | s(34.61%) p(65.31%) d(0.09%) |

|                   | $\sigma (B1 - C2)$          | $sp^{2.72}d^{0}$                     | s(26.83%) p(73.08%) d(0.10%) |
|-------------------|-----------------------------|--------------------------------------|------------------------------|
| 2CN               | $\sigma\left(B1-C10\right)$ | $sp^{2.90}d^{0}$                     | s(25.61%) p(74.30%) d(0.09%) |
| ZUN               | $\sigma\left(B1-C18\right)$ | $sp^{2.89}d^{0}$                     | s(25.65%) p(74.26%) d(0.09%) |
|                   | $\sigma\left(B1-C62\right)$ | sp <sup>3.55</sup> d <sup>0.01</sup> | s(21.94%) p(77.95%) d(0.12%) |
|                   | σ (B1 – C2)                 | $sp^{2.47}d^{0}$                     | s(28.80%) p(71.10%) d(0.10%) |
| ЭF                | $\sigma\left(B1-C10\right)$ | $sp^{2.63}d^{0}$                     | s(27.55%) p(72.34%) d(0.11%) |
| 21                | $\sigma\left(B1-C18\right)$ | $sp^{2.61}d^{0}$                     | s(27.64%) p(72.24%) d(0.11%) |
|                   | $\sigma\left(B1-F62\right)$ | sp <sup>2.95</sup> d <sup>0</sup>    | s(27.05%) p(72.86%) d(0.10%) |
|                   | σ (B1 – C2)                 | $sp^{2.00}d^{0}$                     | s(33.32%) p(66.59%) d(0.10%) |
| 3                 | $\sigma\left(B1-C10\right)$ | $sp^{2.00}d^{0}$                     | s(33.33%) p(66.58%) d(0.10%) |
| <b>3</b> σ(<br>σ( | σ (B1 – C18)                | $sp^{2.00}d^{0}$                     | s(33.31%) p(66.60%) d(0.10%) |
|                   | σ (B1 – C2)                 | $sp^{2.85}d^{0}$                     | s(25.96%) p(73.95%) d(0.09%) |
| 3CN               | $\sigma\left(B1-C10\right)$ | $sp^{2.84}d^{0}$                     | s(25.99%) p(73.92%) d(0.09%) |
| JUN               | $\sigma\left(B1-C18\right)$ | $sp^{2.84}d^{0}$                     | s(25.99%) p(73.92%) d(0.09%) |
|                   | $\sigma\left(B1-C62\right)$ | $sp^{3.52}d^{0.01}$                  | s(22.09%) p(77.80%) d(0.11%) |
|                   | $\sigma\left(B1-C2\right)$  | $sp^{2.58}d^{0}$                     | s(27.90%) p(71.99%) d(0.11%) |
| <b>2</b> E        | $\sigma\left(B1-C10\right)$ | $sp^{2.58}d^{0}$                     | s(27.92%) p(71.97%) d(0.11%) |
| ЭГ                | $\sigma\left(B1-C18\right)$ | sp <sup>2.58</sup> d <sup>0</sup>    | s(27.91%) p(71.98%) d(0.11%) |
|                   | $\sigma\left(B1-F62\right)$ | $sp^{2.87}d^{0}$                     | s(27.05%) p(72.86%) d(0.10%) |

<sup>a</sup> Hybrid on A atom in the A-B Bond or otherwise as indicated. <sup>b</sup> Percentage Contribution of Atomic Orbitals in NBO Hybrid.

Table S10: Calculated Electronic Excitation Energies and Corresponding Oscillator Strengths of Singlet Excited States of 1-3, 1F-3F and 1CN-3CN at DFT/CAM-B3LYP/6-31G(d) Level of Theory.

| molecule   | electronic<br>transition <sup>a</sup>                | energy<br>(nm/eV) | $f^{\mathrm{b}}$ | contrib. <sup>c</sup>     | CId   |
|------------|--|-------------------|------------------|---------------------------|-------|
|            | $S_0 \rightarrow S_1$                                | 377(3,85)         | 0 1745           | HOMO→LUMO                 | 0.658 |
|            | $S_0 \rightarrow S_2$                                | 302(4.10)         | 0.1745           | HOMO-1 $\rightarrow$ LUMO | 0.030 |
|            | $S_0 \rightarrow S_3$                                | 284(4.10)         | 0.0110           | HOMO-1 →LUMO              | 0.638 |
|            | $S_0 \rightarrow S_4$                                | 279 (4.43)        | 0.0140           | HOMO-3→LUMO               | 0.629 |
|            | $S_0 \rightarrow S_5$                                | 264 (4 68)        | 0.0018           | HOMO-4→LUMO               | 0.640 |
|            | $S_0 \rightarrow S_6$                                | 255 (4 84)        | 0.0071           | HOMO-5→LUMO               | 0.637 |
|            | $S_0 \rightarrow S_7$                                | 232(535)          | 0.0196           | HOMO→LUMO+1               | 0.596 |
| 1          | $S_0 \rightarrow S_8$                                | 225 (5.51)        | 0.0033           | HOMO-1→LUMO+1             | 0.334 |
|            | $S_0 \rightarrow S_0$                                | 224 (5.52)        | 0.0009           | HOMO-2→LUMO+1             | 0.323 |
|            | $S_0 \rightarrow S_{10}$                             | 220 (5.63)        | 0.0268           | HOMO-7→LUMO               | 0.399 |
|            | $S_0 \rightarrow S_{11}$                             | 216 (5.72)        | 0.0211           | HOMO-6→LUMO               | 0.571 |
|            | $S_0 \rightarrow S_{10}$                             | 213 (5.81)        | 0.0077           | HOMO-1→LUMO+1             | 0.434 |
|            | $S_0 \rightarrow S_{12}$                             | 211 (5.87)        | 0.0086           | HOMO-4→LUMO+1             | 0.534 |
|            | $S_0 \rightarrow S_{13}$                             | 205(6.05)         | 0.0045           | HOMO-5→LUMO+1             | 0.413 |
|            | $S_0 \rightarrow S_{14}$<br>$S_0 \rightarrow S_{15}$ | 201 (6.15)        | 0.0124           | HOMO-2→LUMO+1             | 0.504 |
|            | $S_0 \rightarrow S_1$                                | 0.57 (1.00)       | 0.0021           |                           | 0.500 |
|            | $S_0 \rightarrow S_2$                                | 257 (4.80)        | 0.0021           | HOMO→LUMO                 | 0.592 |
|            | $S_0 \rightarrow S_3$                                | 246 (5.02)        | 0.0082           | HOMO-5→LUMO               | 0.601 |
|            | 0 5  | 245 (5.05)        | 0.0126           | HOMO-1→LUMO               | 0.485 |
|            | $S_0 \rightarrow S_A$                                | 005 (5.07)        | 0.0001           | HOMO→LUMO                 | 0.104 |
|            | $S_0 \rightarrow S_r$                                | 235 (5.27)        | 0.0081           | HOMO→LUMO+7               | 0.292 |
|            | $S_0 \rightarrow S_c$                                | 234 (5.29)        | 0.0029           | HOMO→LUMO+6               | 0.346 |
|            | $S \rightarrow S$                                    | 230 (5.37)        | 0.0082           | HOMO-1→LUMO               | 0.458 |
| 1 <b>F</b> | $S_0 > S_7$  | 217 (5.70)        | 0.0061           | HOMO-2→LUMO               | 0.517 |
|            | 3 <sub>0</sub> →3 <sub>8</sub>                       | 216 (5.75)        | 0.0014           | HOMO-3→LUMO               | 0.307 |
|            | $s_0 \rightarrow s_9$                                | 215 (5.78)        | 0.0041           | HOMO-3→LUMO               | 0.418 |
|            | $S_0 \rightarrow S_{10}$                             | 214 (5.80)        | 0.0016           | HOMO→LUMO+I               | 0.4/4 |
|            | $S_0 \rightarrow S_{11}$                             | 211 (5.87)        | 0.0050           | HOMO-6→LUMO               | 0.465 |
|            | $S_0 \rightarrow S_{12}$                             | 209 (5.91)        | 0.0035           | HOMO $\rightarrow$ LUMO+4 | 0.246 |
|            | $S_0 \rightarrow S_{13}$                             | 204 (6.06)        | 0.0042           | HUMU-/→LUMU               | 0.301 |
|            | $S_0 \rightarrow S_{14}$                             | 202 (6.11)        | 0.0010           | HOMO- $/\rightarrow$ LUMO | 0.452 |
|            | $S_0 \rightarrow S_{15}$                             | 200 (6.18)        | 0.0021           | HUMU-4→LUMU+I             | 0.236 |

|    | $S_{a} \rightarrow S_{a}$                            |            |        |               |       |
|----|--|------------|--------|---------------|-------|
|    | $S_0 \rightarrow S_1$                                | 251 (4.93) | 0.0040 | HOMO-5→LUMO   | 0.514 |
|    | $S_0 S_2$  | 246 (5.03) | 0.0019 | HOMO-1→LUMO   | 0.523 |
|    | $3_0 \rightarrow 3_3$                                | 240 (5.15) | 0.0046 | HOMO→LUMO     | 0.515 |
|    | $S_0 \rightarrow S_4$                                | 238 (5.20) | 0.0143 | HOMO-4→LUMO   | 0.550 |
|    |  |            |        | HOMO→LUMO     | 0.229 |
|    | $S_0 \rightarrow S_5$                                | 236 (5.24) | 0.0013 | HOMO→LUMO+7   | 0.267 |
|    | $S_0 \rightarrow S_6$                                | 235 (5.26) | 0.0029 | HOMO→LUMO     | 0.357 |
|    | $S_0 \rightarrow S_7$                                | 219 (5.65) | 0.0014 | HOMO-2→LUMO   | 0.591 |
| CN | $S_0 \rightarrow S_8$                                | 216 (5.73) | 0.0023 | HOMO→LUMO+3   | 0.376 |
|    | $S_0 \rightarrow S_9$                                | 214 (5.78) | 0.0021 | HOMO-3→LUMO   | 0.597 |
|    | $S_0 \rightarrow S_{10}$                             | 211 (5.84) | 0.0013 | HOMO-1→LUMO+3 | 0.314 |
|    | $S_0 \rightarrow S_{11}$                             | 208 (5.94) | 0.0005 | HOMO-1→LUMO+1 | 0.511 |
|    | $S_0 \rightarrow S_{12}$                             | 201 (6.14) | 0.0021 | HOMO-4→LUMO+1 | 0.379 |
|    | $S_0 \rightarrow S_{12}$                             | 200 (6.18) | 0.0022 | HOMO-7→LUMO   | 0.441 |
|    | $S_0 \rightarrow S_1$                                | 198 (6.23) | 0.0013 | HOMO→LUMO+1   | 0.419 |
|    | $S_0 \rightarrow S_{14}$                             | 197 (6.27) | 0.0034 | HOMO-5→LUMO   | 0.298 |
|    | $\frac{S_0}{S_{15}}$                                 |            |        |               |       |
|    | $S_0 \rightarrow S_1$                                | 324 (3.82) | 0.1955 | HOMO→LUMO     | 0.664 |
|    | $S_0 \rightarrow S_2$                                | 300 (4.13) | 0.0187 | HOMO-1→LUMO   | 0.622 |
|    | $S_0 \rightarrow S_3$                                | 287 (4.30) | 0.0200 | HOMO-3→LUMO   | 0.464 |
|    | $S_0 \rightarrow S_4$                                | 272 (4.55) | 0.0018 | HOMO-2→LUMO   | 0.553 |
|    | $S_0 \rightarrow S_5$                                | 270 (4.58) | 0.0071 | HOMO-4→LUMO   | 0.522 |
|    | $S_0 \rightarrow S_6$                                | 253 (4.88) | 0.0195 | HOMO-5→LUMO   | 0.667 |
|    | $S_0 \rightarrow S_7$                                | 233 (5.31) | 0.0083 | HOMO→LUMO+1   | 0.603 |
| 2  | $S_0 \rightarrow S_8$                                | 224 (5.53) | 0.0026 | HOMO-6→LUMO   | 0.374 |
|    | $S_0 \rightarrow S_9$                                | 223 (5.55) | 0.0077 | HOMO→LUMO+7   | 0.379 |
|    | $S_0 \rightarrow S_{10}$                             | 221 (5.60) | 0.0104 | HOMO-4→LUMO+1 | 0.370 |
|    | $S_0 \rightarrow S_{11}$                             | 220 (5.62) | 0.0014 | HOMO-2→LUMO+1 | 0.437 |
|    | $S_0 \rightarrow S_{12}$                             | 217 (5.70) | 0.0205 | HOMO-7→LUMO   | 0.414 |
|    | $S_0 \rightarrow S_{12}$                             | 215 (5.76) | 0.0053 | HOMO-1→LUMO+1 | 0.624 |
|    | $S_0 \rightarrow S_1$                                | 213 (5.81) | 0.0116 | HOMO→LUMO+2   | 0.569 |
|    | $S_0 \rightarrow S_{17}$                             | 211 (5.86) | 0.0051 | HOMO-4→LUMO+1 | 0.366 |
|    | $\frac{S_0 \rightarrow S_{15}}{S_1 \rightarrow S_1}$ |            |        |               |       |
|    | $S_0 \rightarrow S_1$                                | 251 (4.92) | 0.0066 | HOMO→LUMO     | 0.525 |
|    | $3_0 \rightarrow 3_2$                                | 249 (4.97) | 0.0012 | HOMO→LUMO+1   | 0.329 |
|    | $S_0 \rightarrow S_3$                                | 246 (5.02) | 0.0035 | HOMO-5→LUMO   | 0.396 |
| 2F | $S_0 \rightarrow S_4$                                | 244 (5.07) | 0.0068 | HOMO→LUMO+1   | 0.392 |
|    | $S_0 \rightarrow S_5$                                | 240 (5.14) | 0.0149 | HOMO-2→LUMO+1 | 0.552 |
|    | <b>-</b> -   |            | 0.007- | HOMO-1→LUMO+1 | 0.142 |
|    | $S_0 \rightarrow S_6$                                | 236 (5.25) | 0.0025 | HOMO-2→LUMO   | 0.504 |

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|     | $S_0 \rightarrow S_7$                             | 233 (5.30)               | 0.0049           | HOMO→LUMO+9                         | 0.480 |
|-----|---|--------------------------|------------------|-------------------------------------|-------|
|     | $S_0 \rightarrow S_8$                             | 221 (5.60)               | 0.0018           | HOMO-3→LUMO                         | 0.404 |
|     | $S_0 \rightarrow S_9$                             | 218 (5.67)               | 0.0031           | HOMO-3→LUMO+1                       | 0.393 |
|     | $S_0 \rightarrow S_{10}$                          | 216 (5.72)               | 0.0015           | HOMO-1→LUMO                         | 0.551 |
|     | $S_0 \rightarrow S_{11}$                          | 213 (5.80)               | 0.0005           | HOMO-1→LUMO+1                       | 0.647 |
|     | $S_0 \rightarrow S_{12}$                          | 212 (5.83)               | 0.0007           | HOMO→LUMO+6                         | 0.475 |
|     | $S_0 \rightarrow S_{12}$                          | 207 (5.98)               | 0.0022           | HOMO→LUMO+3                         | 0.438 |
|     | $S_0 \times S_{13}$                               | 205 (6.02)               | 0.0030           | HOMO→LUMO+2                         | 0.435 |
|     | $3_0 \rightarrow 3_{14}$                          | 201 (6.16)               | 0.0014           | HOMO-7→LUMO                         | 0.335 |
|     | $3_0 \rightarrow 3_{15}$                          |                          |                  |                                     |       |
|     | $S_0 \rightarrow S_1$                             | 250 (4.94)               | 0.0046           | HOMO-4→LUMO                         | 0.405 |
|     | $S_0 \rightarrow S_2$                             | 251 (4 95)               | 0.0034           | HOMO-5→LUMO                         | 0 329 |
|     | $S_0 \rightarrow S_3$                             | 245 (5.04)               | 0.0017           | HOMO→LUMO                           | 0.524 |
|     | $S_0 \rightarrow S_4$                             | 239 (5.18)               | 0.0159           | HOMO-2 $\rightarrow$ LUMO+1         | 0.431 |
|     |   | 259 (5.10)               | 0.0109           | HOMO- $3 \rightarrow LUMO$          | 0.392 |
|     | $S_0 \rightarrow S_5$                             | 236 (5 24)               | 0.0019           | HOMO $\rightarrow$ LUMO+1           | 0.408 |
|     | $S_0 \rightarrow S_6$                             | 235 (5.21)               | 0.0013           | HOMO→LUMO+7                         | 0.403 |
|     | $S_0 \rightarrow S_7$                             | 233 (5.23)               | 0.0048           | HOMO→LUMO+1                         | 0.384 |
| 2CN | $S_0 \rightarrow S_0$                             | 220 (5.62)               | 0.0010           | HOMO-1→LUMO                         | 0.627 |
|     | $S_0 \rightarrow S_0$                             | 217 (5.69)               | 0.0010           | HOMO-3 $\rightarrow$ LUMO+1         | 0.337 |
|     | S <sub>0</sub> →S <sub>10</sub>                   | 217 (5.05)               | 0.0046           | HOMO $\rightarrow$ LUMO+6           | 0.337 |
|     | $S_0 \rightarrow S_{10}$                          | 212 (5.82)               | 0.0030           | HOMO-1 $\rightarrow$ LUMO+1         | 0.544 |
|     | $S_0 / S_{11}$                                    | 209 (5.90)               | 0.0030           | HOMO-2 $\rightarrow$ LUMO+1         | 0.316 |
|     | $3_0 \rightarrow 3_{12}$                          | 205 (6.03)               | 0.0060           | HOMO $\rightarrow$ LUMO+3           | 0.447 |
|     | $S_0 \rightarrow S_{13}$                          | 203 (0.05)               | 0.0000           | HOMO- $2 \rightarrow UUMO+2$        | 0.117 |
|     | $S_0 \rightarrow S_{14}$                          | 201 (0.10)               | 0.0025           | HOMO $2^{\circ}$ / LOMO $^{\circ}2$ | 0.383 |
|     | $S_0 \rightarrow S_{15}$                          | 200 (0.17)               | 0.0050           |                                     | 0.505 |
|     | $S_0 \rightarrow S_1$                             | 302 (4.10)               | 0.1433           | HOMO-4→LUMO                         | 0.485 |
|     | $S_0 \rightarrow S_2$                             | 301 (4.11)               | 0.0015           | HOMO-3→LUMO                         | 0.529 |
|     | $S_0 \rightarrow S_3$                             | 283 (4.37)               | 0.0082           | HOMO-1→LUMO                         | 0.467 |
|     | $S_0 \rightarrow S_4$                             | 282 (4.40)               | 0.0080           | HOMO-2→LUMO                         | 0.463 |
|     | $S_0 \rightarrow S_{r}$                           | 281(4.41)                | 0.0010           | HOMO-4→LUMO                         | 0.453 |
|     | $S_0 \rightarrow S_1$                             | 255 (4.84)               | 0.0000           | HOMO-5→LUMO                         | 0.682 |
| 3   | 5 <sub>0</sub> ,5 <sub>6</sub>                    | 227 (5.46)               | 0.0076           | HOMO-2→LUMO+1                       | 0.425 |
|     | $S_0 \rightarrow S_7$                             | 226 (5.47)               | 0.0055           | HOMO→LUMO+2                         | 0.343 |
|     | ა <sub>0</sub> →ა <sub>8</sub>                    | 225 (5.49)               | 0.0026           | HOMO-2→LUMO+2                       | 0.317 |
|     | $S_0 \rightarrow S_9$                             | 223 (5.55)               | 0.0031           | HOMO-6→LUMO                         | 0.394 |
|     |   | · · · ·                  | 0.0007           |                                     | 0 308 |
|     | $S_0 \rightarrow S_{10}$                          | 222 (5.57)               | 0.0027           | ΠUMU-/→LUMU                         | 0.590 |
|     | $S_0 \rightarrow S_{10}$ $S_0 \rightarrow S_{11}$ | 222 (5.57)<br>213 (5.81) | 0.0027<br>0.0006 | HOMO-7→LUMO<br>HOMO-3→LUMO+1        | 0.398 |

| $S_0 \rightarrow S_{13}$ | 210 (5.89) | 0.0087 | HOMO-6→LUMO   | 0.415 |
|--------------------------|------------|--------|---------------|-------|
| $S_0 \rightarrow S_{14}$ | 209 (5.93) | 0.0015 | HOMO-3→LUMO+2 | 0.432 |
| $S_0 \rightarrow S_{15}$ |            |        |               |       |

|         | $S_0 \rightarrow S_1$    | 248 (4.99) | 0.0051 | HOMO-2→LUMO   | 0.364 |
|---------|--------------------------|------------|--------|---------------|-------|
|         | $S_0 \rightarrow S_2$    | 248 (5.00) | 0.0041 | HOMO-2→LUMO+1 | 0.353 |
|         | $S_0 \rightarrow S_3$    | 247 (5.01) | 0.0058 | HOMO-1→LUMO+2 | 0.364 |
|         | $S_0 \rightarrow S_4$    | 240 (5.18) | 0.0157 | HOMO→LUMO+1   | 0.360 |
|         |                          | ()         |        | HOMO-1→LUMO+1 | 0.349 |
|         | $S_0 \rightarrow S_5$    | 239 (5.19) | 0.0055 | HOMO→LUMO     | 0.366 |
|         | $S_0 \rightarrow S_6$    | 233 (5.31) | 0.0020 | HOMO→LUMO     | 0.373 |
|         | $S_0 \rightarrow S_7$    | 230 (5.39) | 0.0016 | HOMO-1→LUMO+2 | 0.438 |
| 3F      | $S_0 \rightarrow S_8$    | 229 (5.40) | 0.0002 | HOMO→LUMO+2   | 0.463 |
|         | $S_0 \rightarrow S_9$    | 226 (5.46) | 0.0037 | HOMO→LUMO+1   | 0.417 |
|         | $S_0 \rightarrow S_{10}$ | 203 (6.12) | 0.0042 | HOMO-5→LUMO+2 | 0.395 |
|         | $S_0 \rightarrow S_{11}$ | 202 (6.13) | 0.0027 | HOMO-5→LUMO   | 0.501 |
|         | $S_0 \rightarrow S_{12}$ | 201 (6.14) | 0.0008 | HOMO-5→LUMO+1 | 0.477 |
|         | $S_0 \rightarrow S_{12}$ | 198 (6.28) | 0.0034 | HOMO→LUMO+4   | 0.292 |
|         | $S_0 \rightarrow S_{13}$ | 197 (6.29) | 0.0028 | HOMO→LUMO+4   | 0.349 |
|         | $S_0 \rightarrow S_{14}$ | 196 (6.30) | 0.0017 | HOMO-1→LUMO+3 | 0.299 |
|         | <u> </u>                 |            |        |               |       |
|         | $S_0 \rightarrow S_1$    | 251 (4.94) | 0.0038 | HOMO→LUMO+1   | 0.372 |
|         | $S_0 \rightarrow S_2$    | 250 (4.95) | 0.0046 | HOMO-2→LUMO   | 0.274 |
|         | $S_0 \rightarrow S_3$    | 249 (4.97) | 0.0043 | HOMO-5→LUMO   | 0.325 |
|         | $S_0 \rightarrow S_4$    | 238 (5.21) | 0.0160 | HOMO-3→LUMO+1 | 0.334 |
|         |                          |            |        | HOMO-5→LUMO+1 | 0.116 |
|         | $S_0 \rightarrow S_5$    | 237(5.22)  | 0.0060 | HOMO-3→LUMO+1 | 0.350 |
|         | $S_0 \rightarrow S_6$    | 228 (5.43) | 0.0092 | HOMO-1→LUMO   | 0.326 |
| 3CN     | $S_0 \rightarrow S_7$    | 221 (5.60) | 0.0024 | HOMO-1→LUMO+1 | 0.311 |
| • • • • | $S_0 \rightarrow S_8$    | 217 (5.71) | 0.0017 | HOMO-2→LUMO+2 | 0.290 |
|         | $S_0 \rightarrow S_0$    | 216 (5.72) | 0.0016 | HOMO-1→LUMO+2 | 0.325 |
|         | $S_0 \rightarrow S_{10}$ | 204 (6.07) | 0.0013 | HOMO-3→LUMO+1 | 0.452 |
|         | $S_0 \rightarrow S_{10}$ | 203 (6.08) | 0.0011 | HOMO-3→LUMO   | 0.454 |
|         | $S_0 \rightarrow S_{11}$ | 201 (6.15) | 0.0026 | HOMO-3→LUMO+2 | 0.433 |
|         | $S_0 - S_{12}$           | 200 (6.18) | 0.0009 | HOMO→LUMO     | 0.332 |
|         | $s_0 \rightarrow s_{13}$ | 199 (6.22) | 0.0027 | HOMO→LUMO+1   | 0.337 |
|         | $S_0 \rightarrow S_{14}$ | 198 (6.26) | 0.0024 | HOMO-2→LUMO+3 | 0.313 |

<sup>a</sup>Only the Selected Low-lying Excited States are Presented. <sup>b</sup>Oscillator Strength. <sup>c</sup>Only the Main Configurations are Presented. <sup>d</sup> The CI Coefficients are in Absolute Values.

Table S11: Calculated Electronic Excitation Energies and Corresponding Oscillator Strengths of the Low-Lying Singlet Excited States of **1-2**, **1CN-2CN** and **1F-2F** by Employing Different Functionals.

| functional | molecule | electronic<br>transition <sup>a</sup> | energy<br>(nm/eV) | $f^{\mathrm{b}}$ | contrib. <sup>c</sup> | CId   |
|------------|----------|---------------------------------------|-------------------|------------------|-----------------------|-------|
|            |          | $S_0 \rightarrow S_1$                 | 328 (3.77)        | 0.1572           | HOMO→LUMO             | 0.665 |
|            |          | $S_0 \rightarrow S_2$                 | 308 (4.01)        | 0.0197           | HOMO-1→LUMO           | 0.591 |
| MOGON      | 1        | $S_0 \rightarrow S_3$                 | 288 (4.29)        | 0.0059           | HOMO-2→LUMO           | 0.621 |
| M06-2X     | 1        | $S_0 \rightarrow S_4$                 | 281 (4.41)        | 0.0098           | HOMO-3→LUMO           | 0.649 |
|            |          | $S_0 \rightarrow S_5$                 | 263 (4.69)        | 0.0638           | HOMO-4→LUMO           | 0.647 |
|            |          | $S_0 \rightarrow S_6$                 | 260 (4.76)        | 0.0309           | HOMO-5→LUMO           | 0.623 |
|            | 45       | $S_0 \rightarrow S_1$                 | 266 (4.65)        | 0.0069           | HOMO→LUMO             | 0.589 |
|            |          | $S_0 \rightarrow S_2$                 | 247 (5.00)        | 0.0017           | HOMO-1→LUMO           | 0.566 |
| MOC ON     |          | $S_0 \rightarrow S_3$                 | 244 (5.06)        | 0.0329           | HOMO-5→LUMO           | 0.592 |
| M06-2X     | 11       | $S_0 \rightarrow S_4$                 | 234 (5.29)        | 0.0042           | HOMO-4→LUMO           | 0.403 |
|            |          | $S_0 \rightarrow S_5$                 | 232 (5.32)        | 0.0024           | HOMO-2→LUMO+3         | 0.319 |
|            |          | $S_0 \rightarrow S_6$                 | 231 (5.35)        | 0.0013           | HOMO-4→LUMO           | 0.348 |
|            | 1CN      | $S_0 \rightarrow S_1$                 | 254 (4.87)        | 0.0050           | HOMO-1→LUMO           | 0.603 |
| MOGOV      |          | $S_0 \rightarrow S_2$                 | 247 (5.01)        | 0.0021           | HOMO-5→LUMO           | 0.546 |
| WI00-2A    |          | $S_0 \rightarrow S_3$                 | 244 (5.07)        | 0.0017           | HOMO→LUMO             | 0.623 |
|            |          | $S_0 \rightarrow S_4$                 | 236 (5.23)        | 0.0135           | HOMO-4→LUMO           | 0.608 |

|         |              | $S_0 \rightarrow S_5$ | 235 (5.26) | 0.0023 | HOMO→LUMO+6   | 0.325 |
|---------|--------------|-----------------------|------------|--------|---------------|-------|
|         |              | $S_0 \rightarrow S_6$ | 235 (5.27) | 0.0021 | HOMO-1→LUMO+5 | 0.351 |
|         |              | $S_0 \rightarrow S_1$ | 380 (3.25) | 0.1207 | HOMO→LUMO     | 0.701 |
|         |              | $S_0 \rightarrow S_2$ | 355 (3.48) | 0.0603 | HOMO-2→LUMO   | 0.690 |
| D2DU/01 | 4            | $S_0 \rightarrow S_3$ | 352 (3.51) | 0.0204 | HOMO-1→LUMO   | 0.696 |
| B3PW91  | 1            | $S_0 \rightarrow S_4$ | 342 (3.62) | 0.0596 | HOMO-3→LUMO   | 0.699 |
|         |              | $S_0 \rightarrow S_5$ | 296 (4.18) | 0.0374 | HOMO-4→LUMO   | 0.691 |
|         |              | $S_0 \rightarrow S_6$ | 291 (4.25) | 0.0713 | HOMO-5→LUMO   | 0.655 |
|         |              | $S_0 \rightarrow S_1$ | 333 (3.72) | 0.0046 | HOMO→LUMO     | 0.697 |
|         |              | $S_0 \rightarrow S_2$ | 321 (3.85) | 0.0016 | HOMO-1→LUMO   | 0.703 |
| D2DU/01 | 115          | $S_0 \rightarrow S_3$ | 296 (4.17) | 0.0143 | HOMO-2→LUMO   | 0.703 |
| B3PW91  | IF           | $S_0 \rightarrow S_4$ | 290 (4.26) | 0.0001 | HOMO-3→LUMO   | 0.703 |
|         |              | $S_0 \rightarrow S_5$ | 277 (4.47) | 0.0022 | HOMO-4→LUMO   | 0.688 |
|         |              | $S_0 \rightarrow S_6$ | 265 (4.66) | 0.0012 | HOMO→LUMO+1   | 0.671 |
|         |              | $S_0 \rightarrow S_1$ | 321 (3.85) | 0.0075 | HOMO-1→LUMO   | 0.647 |
|         |              | $S_0 \rightarrow S_2$ | 320 (3.86) | 0.0050 | HOMO→LUMO     | 0.653 |
| D2DW01  | 1 <b>C</b> N | $S_0 \rightarrow S_3$ | 300 (4.12) | 0.0035 | HOMO-2→LUMO   | 0.699 |
| B3PW91  | ICN          | $S_0 \rightarrow S_4$ | 291 (4.25) | 0.0126 | HOMO-3→LUMO   | 0.703 |
|         |              | $S_0 \rightarrow S_5$ | 264 (4.69) | 0.0044 | HOMO-4→LUMO   | 0.636 |
|         |              | $S_0 \rightarrow S_6$ | 263 (4.71) | 0.0080 | HOMO-5→LUMO   | 0.579 |
|         |              | $S_0 \rightarrow S_1$ | 442 (2.80) | 0.1563 | HOMO→LUMO     | 0.699 |
|         |              | $S_0 \rightarrow S_2$ | 423 (2.92) | 0.0100 | HOMO-2→LUMO   | 0.699 |
| ИСТИ    | 1            | $S_0 \rightarrow S_3$ | 422 (2.93) | 0.0071 | HOMO-1→LUMO   | 0.647 |
| пстп    | 1            | $S_0 \rightarrow S_4$ | 409 (3.02) | 0.0542 | HOMO-3→LUMO   | 0.647 |
|         |              | $S_0 \rightarrow S_5$ | 335 (3.69) | 0.0057 | HOMO→LUMO+1   | 0.683 |
|         |              | $S_0 \rightarrow S_6$ | 327 (3.79) | 0.0344 | HOMO-1→LUMO+1 | 0.524 |

|      |              | $S_0 \rightarrow S_1$ | 429 (2.88) | 0.0032 | HOMO→LUMO     | 0.704 |
|------|--------------|-----------------------|------------|--------|---------------|-------|
|      |              | $S_0 \rightarrow S_2$ | 421 (2.93) | 0.0083 | HOMO-1→LUMO   | 0.702 |
| UCTU | 11           | $S_0 \rightarrow S_3$ | 389 (3.18) | 0.0187 | HOMO-2→LUMO   | 0.706 |
| пстп | 11           | $S_0 \rightarrow S_4$ | 381 (3.24) | 0.0001 | HOMO-3→LUMO   | 0.705 |
|      |              | $S_0 \rightarrow S_5$ | 358 (3.46) | 0.0018 | HOMO-4→LUMO   | 0.694 |
|      |              | $S_0 \rightarrow S_6$ | 329 (3.76) | 0.0068 | HOMO-5→LUMO   | 0.692 |
|      |              | $S_0 \rightarrow S_1$ | 417 (2.97) | 0.0020 | HOMO→LUMO     | 0.706 |
|      |              | $S_0 \rightarrow S_2$ | 412 (3.00) | 0.0076 | HOMO-1→LUMO   | 0.706 |
| UCTU | 1 <i>C</i> N | $S_0 \rightarrow S_3$ | 392 (3.15) | 0.0023 | HOMO-2→LUMO   | 0.706 |
| HCIH | ICN          | $S_0 \rightarrow S_4$ | 382 (3.24) | 0.0181 | HOMO-3→LUMO   | 0.706 |
|      |              | $S_0 \rightarrow S_5$ | 323 (3.83) | 0.0012 | HOMO→LUMO+1   | 0.706 |
|      |              | $S_0 \rightarrow S_6$ | 321 (3.85) | 0.0014 | HOMO-1→LUMO+1 | 0.706 |
|      |              | $S_0 \rightarrow S_1$ | 474 (2.61) | 0.1687 | HOMO→LUMO     | 0.686 |
|      |              | $S_0 \rightarrow S_2$ | 448 (2.76) | 0.0381 | HOMO-1→LUMO   | 0.687 |
|      | 1            | $S_0 \rightarrow S_3$ | 436 (2.84) | 0.0245 | HOMO-2→LUMO   | 0.646 |
| LSDA | 1            | $S_0 \rightarrow S_4$ | 415 (2.98) | 0.0703 | HOMO-3→LUMO   | 0.645 |
|      |              | $S_0 \rightarrow S_5$ | 354 (3.49) | 0.0518 | HOMO→LUMO+1   | 0.638 |
|      |              | $S_0 \rightarrow S_6$ | 349 (3.54) | 0.0313 | HOMO-4→LUMO   | 0.583 |
|      |              | $S_0 \rightarrow S_1$ | 446 (2.77) | 0.0016 | HOMO→LUMO     | 0.704 |
|      |              | $S_0 \rightarrow S_2$ | 431 (2.87) | 0.0015 | HOMO-1→LUMO   | 0.701 |
|      | 10           | $S_0 \rightarrow S_3$ | 397 (3.11) | 0.0192 | HOMO-2→LUMO   | 0.705 |
| LSDA | 11           | $S_0 \rightarrow S_4$ | 379 (3.27) | 0.0011 | HOMO-3→LUMO   | 0.705 |
|      |              | $S_0 \rightarrow S_5$ | 357 (3.46) | 0.0020 | HOMO-4→LUMO   | 0.687 |
|      |              | $S_0 \rightarrow S_6$ | 338 (3.65) | 0.0003 | HOMO→LUMO+1   | 0.704 |

|          |     | $S_0 \rightarrow S_1$ | 427 (2.89) | 0.0034 | HOMO→LUMO     | 0.701 |
|----------|-----|-----------------------|------------|--------|---------------|-------|
|          |     | $S_0 \rightarrow S_2$ | 422 (2.93) | 0.0038 | HOMO-1→LUMO   | 0.701 |
|          | 101 | $S_0 \rightarrow S_3$ | 395 (3.13) | 0.0043 | HOMO-2→LUMO   | 0.704 |
| LSDA     | ICN | $S_0 \rightarrow S_4$ | 375 (3.30) | 0.0139 | HOMO-3→LUMO   | 0.702 |
|          |     | $S_0 \rightarrow S_5$ | 331 (3.74) | 0.0015 | HOMO→LUMO+1   | 0.704 |
|          |     | $S_0 \rightarrow S_6$ | 328 (3.77) | 0.0005 | HOMO-1→LUMO+1 | 0.704 |
|          |     | $S_0 \rightarrow S_1$ | 329 (3.76) | 0.1856 | HOMO→LUMO     | 0.666 |
|          |     | $S_0 \rightarrow S_2$ | 304 (4.07) | 0.0235 | HOMO-1→LUMO   | 0.580 |
| MOC ON   | 2   | $S_0 \rightarrow S_3$ | 293 (4.22) | 0.0440 | HOMO-2→LUMO   | 0.486 |
| M06-2X   | 2   | $S_0 \rightarrow S_4$ | 271 (4.56) | 0.0532 | HOMO-3→LUMO   | 0.625 |
|          |     | $S_0 \rightarrow S_5$ | 270 (4.58) | 0.0042 | HOMO-4→LUMO   | 0.547 |
|          |     | $S_0 \rightarrow S_6$ | 256 (4.82) | 0.0111 | HOMO-5→LUMO   | 0.669 |
|          |     | $S_0 \rightarrow S_1$ | 258 (4.79) | 0.0087 | HOMO→LUMO     | 0.526 |
|          |     | $S_0 \rightarrow S_2$ | 254 (4.87) | 0.0029 | HOMO→LUMO+1   | 0.481 |
| N/06 037 |     | $S_0 \rightarrow S_3$ | 245 (5.06) | 0.0033 | HOMO-4→LUMO+1 | 0.338 |
| M06-2X   | 21  | $S_0 \rightarrow S_4$ | 244 (5.07) | 0.0045 | HOMO-4→LUMO   | 0.334 |
|          |     | $S_0 \rightarrow S_5$ | 241 (5.14) | 0.0143 | HOMO-2→LUMO+1 | 0.552 |
|          |     | $S_0 \rightarrow S_6$ | 236 (5.25) | 0.0026 | HOMO-2→LUMO   | 0.521 |
|          |     | $S_0 \rightarrow S_1$ | 253 (4.91) | 0.0075 | HOMO→LUMO     | 0.584 |
|          |     | $S_0 \rightarrow S_2$ | 248 (4.98) | 0.0018 | HOMO-4→LUMO   | 0.391 |
| MOC ON   |     | $S_0 \rightarrow S_3$ | 247 (5.02) | 0.0014 | HOMO-5→LUMO   | 0.420 |
| M06-2X   | 2CN | $S_0 \rightarrow S_4$ | 241 (5.14) | 0.0143 | HOMO→LUMO+1   | 0.503 |
|          |     | $S_0 \rightarrow S_5$ | 236 (5.24) | 0.0061 | HOMO-3→LUMO   | 0.431 |
|          |     | $S_0 \rightarrow S_6$ | 235 (5.27) | 0.0032 | HOMO→LUMO+7   | 0.473 |

|         |            | $S_0 \rightarrow S_1$ | 380 (3.25) | 0.1527 | HOMO→LUMO     | 0.699 |
|---------|------------|-----------------------|------------|--------|---------------|-------|
|         |            | $S_0 \rightarrow S_2$ | 373 (3.32) | 0.0074 | HOMO-1→LUMO   | 0.702 |
| DADUIA1 | •          | $S_0 \rightarrow S_3$ | 327 (3.78) | 0.0306 | HOMO-3→LUMO   | 0.466 |
| B3PW91  | 2          | $S_0 \rightarrow S_4$ | 316 (3.92) | 0.0230 | HOMO-2→LUMO   | 0.538 |
|         |            | $S_0 \rightarrow S_5$ | 312 (3.96) | 0.0464 | HOMO-4→LUMO   | 0.624 |
|         |            | $S_0 \rightarrow S_6$ | 294 (4.20) | 0.0277 | HOMO→LUMO+1   | 0.703 |
|         |            | $S_0 \rightarrow S_1$ | 324 (3.81) | 0.0052 | HOMO→LUMO     | 0.695 |
|         |            | $S_0 \rightarrow S_2$ | 319 (3.87) | 0.0032 | HOMO→LUMO+1   | 0.695 |
|         | <b>3</b> E | $S_0 \rightarrow S_3$ | 296 (4.18) | 0.0004 | HOMO-1→LUMO   | 0.704 |
| B3PW91  | 2 <b>F</b> | $S_0 \rightarrow S_4$ | 292 (4.23) | 0.0010 | HOMO-1→LUMO+1 | 0.700 |
|         |            | $S_0 \rightarrow S_5$ | 281 (4.40) | 0.0112 | HOMO-2→LUMO+1 | 0.590 |
|         |            | $S_0 \rightarrow S_6$ | 280 (4.41) | 0.0079 | HOMO-2→LUMO   | 0.585 |
|         |            | $S_0 \rightarrow S_1$ | 324 (3.81) | 0.0052 | HOMO→LUMO     | 0.696 |
|         |            | $S_0 \rightarrow S_2$ | 319 (3.87) | 0.0032 | HOMO→LUMO+1   | 0.695 |
|         |            | $S_0 \rightarrow S_3$ | 296 (4.18) | 0.0004 | HOMO-1→LUMO   | 0.704 |
| B3PW91  | 2CN        | $S_0 \rightarrow S_4$ | 292 (4.23) | 0.0152 | HOMO→LUMO+1   | 0.700 |
|         |            | $S_0 \rightarrow S_5$ | 281 (4.40) | 0.0011 | HOMO-2→LUMO+1 | 0.590 |
|         |            | $S_0 \rightarrow S_6$ | 280 (4.41) | 0.0070 | HOMO-2→LUMO   | 0.585 |
|         |            | $S_0 \rightarrow S_1$ | 452 (2.74) | 0.1372 | HOMO→LUMO     | 0.698 |
|         |            | $S_0 \rightarrow S_2$ | 445 (2.78) | 0.0183 | HOMO-→LUMO    | 0.695 |
| UCTU    | 2          | $S_0 \rightarrow S_3$ | 370 (3.34) | 0.0035 | HOMO→LUMO+1   | 0.696 |
| HUTH    | 2          | $S_0 \rightarrow S_4$ | 368 (3.37) | 0.0002 | HOMO-1→LUMO+1 | 0.701 |
|         |            | $S_0 \rightarrow S_5$ | 362 (3.42) | 0.0203 | HOMO-2→LUMO   | 0.631 |
|         |            | $S_0 \rightarrow S_6$ | 360 (3.44) | 0.0376 | HOMO-3→LUMO   | 0.634 |

|      |     | $S_0 \rightarrow S_1$ | 417 (2.96) | 0.0028 | HOMO→LUMO     | 0.705 |
|------|-----|-----------------------|------------|--------|---------------|-------|
|      |     | $S_0 \rightarrow S_2$ | 412 (3.00) | 0.0014 | HOMO→LUMO+1   | 0.704 |
| UCTU | ЭГ  | $S_0 \rightarrow S_3$ | 387 (3.20) | 0.0000 | HOMO-1→LUMO   | 0.705 |
| пстп | 2Γ  | $S_0 \rightarrow S_4$ | 382 (3.24) | 0.0011 | HOMO-1→LUMO+1 | 0.706 |
|      |     | $S_0 \rightarrow S_5$ | 354 (3.49) | 0.0563 | HOMO-2→LUMO   | 0.539 |
|      |     | $S_0 \rightarrow S_6$ | 352 (3.52) | 0.0046 | HOMO-2→LUMO+1 | 0.542 |
|      |     | $S_0 \rightarrow S_1$ | 415 (2.98) | 0.0015 | HOMO→LUMO     | 0.706 |
|      |     | $S_0 \rightarrow S_2$ | 397 (3.12) | 0.0109 | HOMO→LUMO+1   | 0.703 |
| UCTU |     | $S_0 \rightarrow S_3$ | 393 (3.15) | 0.0013 | HOMO-1→LUMO   | 0.704 |
| нстн | 2CN | $S_0 \rightarrow S_4$ | 377 (3.28) | 0.0143 | HOMO-1→LUMO+1 | 0.706 |
|      |     | $S_0 \rightarrow S_5$ | 328 (3.77) | 0.0012 | HOMO-2→LUMO   | 0.564 |
|      |     | $S_0 \rightarrow S_6$ | 319 (3.88) | 0.0036 | HOMO-2→LUMO+1 | 0.409 |
|      |     | $S_0 \rightarrow S_1$ | 450 (2.75) | 0.1575 | HOMO→LUMO     | 0.697 |
|      |     | $S_0 \rightarrow S_2$ | 424 (2.92) | 0.0140 | HOMO-1→LUMO   | 0.682 |
|      | 2   | $S_0 \rightarrow S_3$ | 389 (3.18) | 0.0282 | HOMO-2→LUMO   | 0.694 |
| LSDA | 2   | $S_0 \rightarrow S_4$ | 384 (3.22) | 0.0080 | HOMO-3→LUMO   | 0.684 |
|      |     | $S_0 \rightarrow S_5$ | 346 (3.40) | 0.0046 | HOMO→LUMO+1   | 0.690 |
|      |     | $S_0 \rightarrow S_6$ | 361 (3.43) | 0.0084 | HOMO-4→LUMO   | 0.581 |
|      |     | $S_0 \rightarrow S_1$ | 427 (2.90) | 0.0044 | HOMO→LUMO     | 0.670 |
|      |     | $S_0 \rightarrow S_2$ | 425 (2.91) | 0.0008 | HOMO→LUMO+1   | 0.669 |
|      | ЭГ  | $S_0 \rightarrow S_3$ | 388 (3.19) | 0.0001 | HOMO-1→LUMO   | 0.694 |
| LSDA | 2Γ  | $S_0 \rightarrow S_4$ | 387 (3.20) | 0.0051 | HOMO-1→LUMO+1 | 0.698 |
|      |     | $S_0 \rightarrow S_5$ | 364 (3.40) | 0.0574 | HOMO-2→LUMO+1 | 0.540 |
|      |     | $S_0 \rightarrow S_6$ | 357 (3.46) | 0.0042 | HOMO-2→LUMO   | 0.530 |

|      |      | $S_0 \rightarrow S_1$ | 424(2.92)  | 0.0010 | HOMO→LUMO     | 0.706 |
|------|------|-----------------------|------------|--------|---------------|-------|
|      |      | $S_0 \rightarrow S_2$ | 403 (3.07) | 0.0021 | HOMO→LUMO+1   | 0.702 |
| ISDA | 2CN  | $S_0 \rightarrow S_3$ | 394 (3.14) | 0.0022 | HOMO-1→LUMO   | 0.700 |
| LSDA | 2011 | $S_0 \rightarrow S_4$ | 377 (3.28) | 0.0129 | HOMO-1→LUMO+1 | 0.704 |
|      |      | $S_0 \rightarrow S_5$ | 337 (3.67) | 0.0054 | HOMO-2→LUMO   | 0.572 |
|      |      | $S_0 \rightarrow S_6$ | 327 (3.78) | 0.0012 | HOMO→LUMO+2   | 0.681 |

<sup>a</sup> Only the Selected Low-lying Excited States are Presented. <sup>b</sup> Oscillator sSrength. <sup>c</sup> Only the Main Configurations are Presented. <sup>d</sup> The CI Coefficients are in Absolute Values.

Table S12: Calculated Electronic De-Excitation Energies and Corresponding Oscillator Strengths of the Higher Singlet Excited States of **1F-3F** and **1CN-3CN** at DFT/CAM-B3LYP/631G(d) Level of Theory.

| molecule | electronic<br>de-<br>excitation <sup>a</sup> | energy<br>(eV) | $f^{b}$            | contrib. <sup>c</sup>      | CId            |
|----------|--|----------------|--------------------|----------------------------|----------------|
| 1F       | $S_1 \leftarrow S_2 \\ S_2 \leftarrow S_3$   | 0.74<br>0.70   | $0.0003 \\ 0.0002$ | HOMO←LUMO<br>HOMO – 1←LUMO | 0.631<br>0.565 |
| 1CN      | $S_1 \leftarrow S_2$                         | 0.49           | 0.0002             | HOMO-1←LUMO                | 0.447          |
|          | $S_2 \leftarrow S_3$                         | 0.41           | 0.0001             | HOMO-5←LUMO                | 0.594          |
|          | $S_3 \leftarrow S_4$                         | 0.30           | 0.0002             | HOMO←LUMO                  | 0.350          |
| 2F       | $S_1 \leftarrow S_2$                         | 0.42           | 0.0003             | HOMO←LUMO                  | 0.568          |
|          | $S_2 \leftarrow S_3$                         | 0.31           | 0.0001             | HOMO-1←LUMO                | 0.383          |
|          | $S_3 \leftarrow S_4$                         | 0.23           | 0.0002             | HOMO-1←LUMO                | 0.409          |
|          | $S_4 \leftarrow S_5$                         | 0.19           | 0.0003             | HOMO←LUMO+1                | 0.477          |
| 2CN      | $S_1 \leftarrow S_2$                         | 0.48           | 0.0003             | HOMO-2←LUMO                | 0.631          |
|          | $S_2 \leftarrow S_3$                         | 0.39           | 0.0001             | HOMO-4←LUMO                | 0.509          |
|          | $S_3 \leftarrow S_4$                         | 0.33           | 0.0002             | HOMO←LUMO                  | 0.677          |

| 3F  | $S_1 \leftarrow S_2$<br>$S_2 \leftarrow S_3$<br>$S_3 \leftarrow S_4$ | 0.09<br>0.07<br>0.04 | $\begin{array}{c} 0.0002 \\ 0.0004 \\ 0.0002 \end{array}$ | HOMO←LUMO<br>HOMO-5←LUMO<br>HOMO-1←LUMO | 0.657<br>0.421<br>0.602 |
|-----|--|----------------------|---|---|-------------------------|
| 3CN | $S_1 \leftarrow S_2$   | 0.76                 | 0.0003  | HOMO←LUMO                               | 0.693                   |
|     | $S_2 \leftarrow S_3$   | 0.51                 | 0.0002  | HOMO-1←LUMO                             | 0.640                   |
|     | $S_3 \leftarrow S_4$   | 0.33                 | 0.0004  | HOMO-4←LUMO                             | 0.404                   |

<sup>a</sup> Only the Selected Low-lying Excited States are Presented. <sup>b</sup> Oscillator sSrength. <sup>c</sup> Only the Main Configurations are Presented. <sup>d</sup> The CI Coefficients are in Absolute Values.





Figure S1: Ground state (S<sub>0</sub>) optimized structures of **1F-3F** and **1CN-3CN** calculated at CAM-B3LYP/6-31G(d) level with the CPCM solvation model. Hydrogen atoms are omitted for clarity. In **1**, **2** and **3**, the cyanide and the fluoride ions are added at boron atoms with numbering 1. The numbering of atoms of added cyanide is C (62), N (63) and added fluoride is F (62). Geometry at boron centers in **1F-3F** and **1CN-3CN** is tetrahedral.





Figure S2: Potential energy curves of corresponding  $S_0$  states of (I) **1F**, (III) **2F** and (V) **3F**; and corresponding  $S_1$  states of (II) **1F**, (IV) **2F** and (VI) **3F** calculated at the CAM-B3LYP/6-31G(d) level with the CPCM solvation model as functions of the angles mentioned.



Figure S3: Calculated FMO energies for (I) **1** in ground state and excited state (**1\_EXC**) (II) **1F** in ground state and excited state (**1F\_EXC**) and (III) **1CN** in ground state and excited state (**1CN\_EXC**) at CAM-B3LYP/6-31G(d) level using CPCM solvation model.



Figure S4: Calculated FMO energies for (IV) **2** in ground state and excited state (**2\_EXC**) (V) **2F** in ground state and excited state (**2F\_EXC**) and (VI) **2CN** in ground state and excited state (**2CN\_EXC**) at CAM-B3LYP/6-31G(d) level using CPCM solvation model.



Figure S5: Calculated FMO energies for (VII) **3** in ground state and excited state (**3\_EXC**) (VIII) **3F** in ground state and excited state (**3F\_EXC**) and (IX) **3CN** in ground state and excited state (**3CN\_EXC**) at CAM-B3LYP/6-31G(d) level using CPCM solvation model.





Figure S6: Excited state (S<sub>1</sub>) optimized structures of 1, 1F, 1CN, 2, 2F, 2CN, 3, 3F and 3CN calculated at CAM-B3LYP/6-31G(d) level with the CPCM solvation model. Hydrogen atoms are omitted for clarity. In 1, 2 and 3, the cyanide and the fluoride ions are added at boron atoms with numbering 1. The numbering of atoms of added cyanide is C (62), N (63) and fluoride is F (62). Geometry at boron centers in 1, 2 and 3 is trigonal planar while as geometry at boron centers in 1F-3F and 1CN-3CN is tetrahedral.



Figure S7: Excited state optimized structures of **1F** (third excited state,  $S_3$ ), **1CN** (fourth excited state,  $S_4$ ), **2F** (fifth excited state,  $S_5$ ), **2CN** (fourth excited state,  $S_4$ ), **3F** (fourth excited state,  $S_4$ ) and **3CN** (fourth excited state,  $S_4$ ) calculated at CAM-B3LYP/6-31G(d) level with the CPCM solvation model. Hydrogen atoms are omitted for clarity.



Figure S8: Scheme of the different mechanisms of fluorescence emission for 2, 2F and 2CN.



Figure S9: Scheme of the different mechanisms of fluorescence emission for 3, 3F and 3CN.

## References

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