# Kinetic differences in the intercalation of linear and cyclic penta(ethylene oxide)s into graphite oxide leading to separation by topology

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# **S1. SUPPLEMENTAL GRAPHS**



Fig. S1. *In situ* XRD data of GO and an excess of  $5EG_{OH}$  showing monolayer intercalation as a function of time at 40 °C and 80°C. The diffractograms were recorded every 3.7 min.



Fig. S2. In situ XRD data of GO and an excess of  $5EG_{OMe}$  showing monolayer intercalation as a function of time at 40 °C and 80°C. The diffractograms were recorded every 3.7 min.



Fig. S3. *In situ* XRD data of GO and an excess of 15C5 showing monolayer intercalation as a function of time at 80 °C. The diffractograms were recorded every 30 min.



Fig. S4. XRD data of GO and an excess of  $15C5_{OH}$  showing monolayer intercalation as a function of time. Total time = 19 days. Intercalation was carried out in an oven at 80 °C.



Fig. S5. XRD data showing the monolayer/bilayer reversibility for  $5EG_{OH}$  intercalated in GO by cooling and heating. Upon fast cooling to 20 °C, the formation of the bilayer and the total disappearance of the monolayer occur in about 1.5 h. Upon fast heating to 80 °C, the formation of the monolayer and the total disappearance of the bilayer are practically instantaneous.



Fig. S6. Variation of  $T_g$  with the weight fraction of linear chains (L) in blends of cyclic/linear chains (C/L). Dashed line shows the Gordon-Taylor fit using the Eq. S2.



Fig. S7. (Left axis) Whole DSC thermogram for the *in situ* intercalation of a blend (75/25 wt% 15C5/5EG<sub>OH</sub>) in GO by using a GO/5EG<sub>OH</sub> ratio of 80/20 wt% at heating rates of 10 °C/min and nominal cooling rates of 50 °C/min (since the equipment cannot follow this cooling rate in the whole temperature range, a change in the heat flow at about -30 °C is observed). (Right axis) Time-temperature lines following the cooling, heating and isothermal runs.



Fig. S8. XRD data of a mixture of GO and 90:10 wt% 15C5:5EG<sub>OH</sub> showing monolayer intercalation as a function of time at 40°C. Total intercalation time = 140 min.



Fig. S9. Cold crystallization and melting of  $15C5/5EG_{OH}$  blends of different composition (wt%).



Fig. S10. Variation of  $T_g$  as a function of intercalation time in DSC experiments for *in* situ intercalation of blends of 15C5 and 5EG<sub>OH</sub> at 40 °C (composition indicated in 15C5/5EG<sub>OH</sub> wt%).

# **S2. EVALUATION OF DATA**

## S2.1 Extent of reaction

The extent of intercalation at any time (t) is defined as follows: <sup>1</sup>

$$\alpha(t) = I_{001}(t) / I_{001}(t_{\infty})$$
 Eq S1

where  $I_{001}(t)$  represents the integrated intensity of the 001 reflection at time *t*, and  $I_{001}(t_{\infty})$  is the integrated intensity when the intercalation is complete.  $I_{001}(t_{\infty})$  was determined from the *y* intercept obtained by linearly fitting the  $I_{001}(t)$  of intercalate *vs* the  $I_{001}(t)$  of GO.

#### S2.2 Composition of non-intercalated liquid

In blends of 15C5 and 5EG<sub>OH</sub>, the large  $T_g$  variation allowed us to establish a method to quantify the composition of non-intercalated liquid in GO (red diamonds of Figure S6). This method could not be established for the 15C5/5EG<sub>OMe</sub> blends due to the insignificant variation of  $T_g$  at low amounts of the linear component (green triangles of Figure S6). The higher  $T_g$  observed for 5EG<sub>OH</sub> respect to that for 15C5 can be attributed to hydrogen-bond interactions in the hydroxyl-terminated linear compound. This effect is not present in the methoxyl-terminated linear compound, 5EG<sub>OMe</sub>, resulting in a  $T_g$  slightly lower than that of 15C5, in agreement with theoretical and experimental expectations.<sup>2, 3</sup>

To calculate the composition of non-intercalated liquid in GO, we used the concentration dependence of  $T_g$  of Figure S6 as a calibration curve. The variation of the  $T_g$  data for 15C5/5EG<sub>OH</sub> showed a composition dependence that is well-described by the Gordon–Taylor equation.<sup>4</sup>

$$T_g = \frac{f_1 T_{g,1} + K_{GT} (1 - f_1) T_{g,2}}{f_1 + K_{GT} (1 - f_1)}$$
Eq S2

 $T_g$  is the glass transition temperature of the blend at the  $f_1$  composition,  $f_1$  is the fraction of 5EG<sub>OH</sub> in the blend,  $f_1 = 1 - f_2$ ,  $f_2$  is the fraction of 15C5 in the blend,  $T_{g,1} = 194.46 K$ ,  $T_{g,2} = 173.11 K$  and  $K_{GT} = 0.576$ , as obtained from the fitting (R<sup>2</sup> =0.999). The parameter  $K_{GT}$  shows unequal contributions of both components to the blend; observed as different heat capacity steps ( $\Delta C_p$ ) at the glass transition:  $\Delta C_p$  (15C5)= 0.86 J/gK and  $\Delta C_p$ (5EG<sub>OH</sub>) = 1.50 J/gK.

The composition of  $f_1$  in the non-intercalated liquid was determined by isolating  $f_1$  from Eq S2:

$$f_1 = \frac{K_{GT}(T_{g,2} - T_g)}{K_{GT}(T_{g,2} - T_g) + (T_g - T_{g,1})}$$
Eq S3

In this case,  $T_g$  is the glass transition of non-intercalated liquid during intercalation.

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