

## *Electronic supplementary information*

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**Table S2** Theoretical vibrational frequencies and assignments of Bz and Bz<sub>2</sub> in the S<sub>0</sub> and S<sub>1</sub> states calculated by the (TD-)M06-2X/cc-pVDZ level of theory.

**Table S3** Comparison between the theoretical average frequencies of the S<sub>0</sub> and S<sub>1</sub> states of Bz and the EXC state of Bz<sub>2</sub> evaluated from values in Table S1.

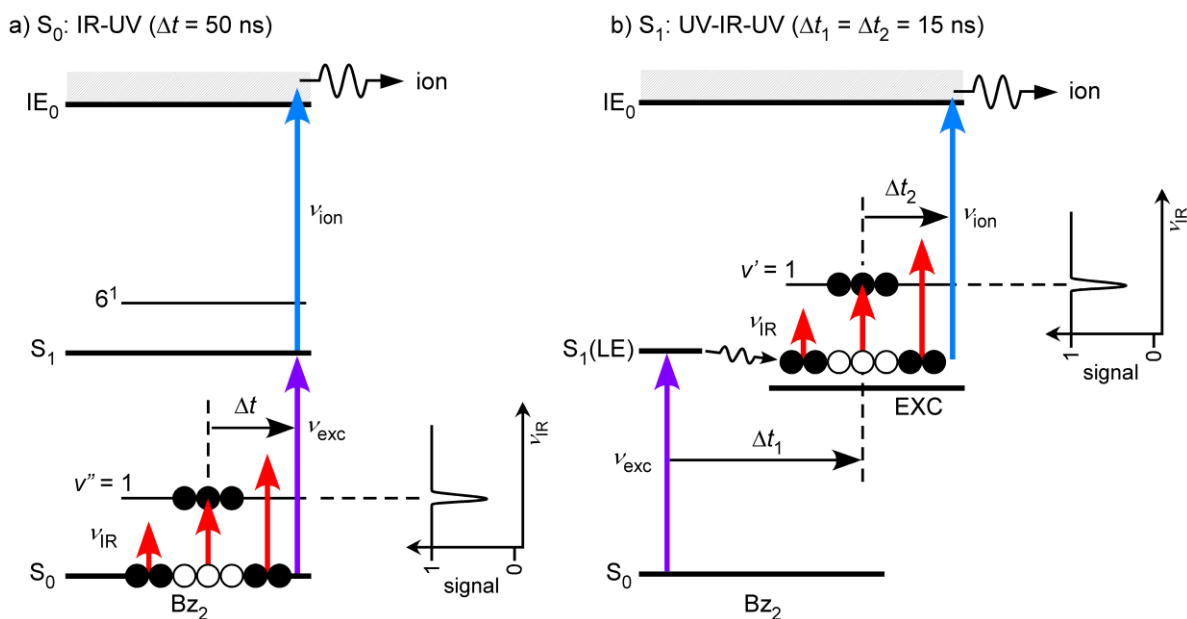
**Table S4** Theoretical vibrational frequencies and assignments of Bz and Bz<sub>2</sub> in the S<sub>0</sub> and S<sub>1</sub> states calculated by the (TD-)CAM-B3LYP/aug-cc-pVTZ level of theory with GD3BJ empirical dispersion correction.

**Table S5** Comparison between the theoretical average frequencies of the S<sub>0</sub> and S<sub>1</sub> states of Bz and the EXC state of Bz<sub>2</sub> evaluated from values in Table S3.

**Table S6** Comparison between the average frequencies of S<sub>0</sub> and S<sub>1</sub> states ( $\nu_{\text{ave}}$ ) and EXC state ( $\nu_{\text{EXC}}$ ) obtained by the (TD-)CAM-B3LYP/aug-cc-pVTZ level of theory with GD3BJ empirical dispersion correction. This is a table corresponding to Table 2 in the main text but with the CAM-B3LYP functional.

**Figure S2** Comparison of vibration frequencies of (a) Bz in S<sub>0</sub>, (b) Bz in S<sub>1</sub> and (c) Bz<sub>2</sub> in S<sub>1</sub> states (SW structure) obtained by CAM-B3LYP/aug-cc-pVTZ and TD-CAM-B3LYP/aug-cc-pVTZ levels of theory with the GD3BJ empirical dispersion correction, and the experimental spectrum (d). This is a figure corresponding to Figure 5 in the main text but with the CAM-B3LYP functional.

Full expression of the excimer state vibrational energy,  $E_{v_{\pm}}^{+/-}$ , derived from the secular determinant given by equation (34) in *Appendix*.



**Figure S1** Excitation schemes of (a) IR-UV spectroscopy for a  $S_0$  state and (b) UV-IR-UV spectroscopy for a  $S_1$  state. In this work,  $\nu_{\text{IR}}$  was fired 50 ns prior to the two UV pulses ( $\Delta t = 50$  ns) for the IR-UV spectroscopy, while  $\nu_{\text{IR}}$  was irradiated 15 ns after  $\nu_{\text{exc}}$ , and  $\nu_{\text{ion}}$  was fired 15 ns after  $\nu_{\text{IR}}$  ( $\Delta t_1 = \Delta t_2 = 15$  ns) for the UV-IR-UV spectroscopy according to the lifetime of the  $S_1$  state of  $\text{Bz}_2$  ( $\sim 40$  ns).<sup>64</sup>  $\nu_{\text{ion}}$  was set to 270 nm for Bz and 285 nm for  $\text{Bz}_2$ , respectively.

**Table S1** Comparison of C–C bond lengths in Bz ( $r_{\text{C-C}}$ ), distances between centers of each Bz ring ( $r_{\text{Bz-Bz}}$ ), binding energies of EXC ( $D_0$ ) of benzene (Bz) and benzene dimer ( $\text{Bz}_2$ ) obtained by (TD-)M06-2X/cc-pVDZ and (TD-)CAM-B3LYP/aug-cc-pVTZ with GD3BJ empirical dispersion correction levels of theory. Upper and lower rows of each parameter show results by M06-2X and CAM-B3LYP functionals, respectively.  $r_{\text{Bz-Bz}}$  means distance between centers of each Bz ring.

	Bz ( $S_0$ )	Bz ( $S_1$ )	$\text{Bz}_2$ (EXC, SW, $D_{6h}$ )	$\text{Bz}_2$ ( $S_1$ (stem*), T, $C_{2v}$ )
$r_{\text{C-C}} / \text{pm}$	139.5	142.5	140.8	142.5 (stem); 139.5 (top)
	138.5	141.5	139.8	141.4 (stem); 138.5 (top)
$r_{\text{Bz-Bz}} / \text{pm}$			299.8	488.2
			304.7	496.4
$D_0 / \text{cm}^{-1}$			4428	641
			4113	845

**Table S2** Theoretical ( $\nu_{\text{calc}}$ ) vibrational frequencies and the assignments of Bz and Bz<sub>2</sub> in the S<sub>0</sub> and S<sub>1</sub> states calculated by normal mode analyses on the optimized structures obtained by M06-2X/cc-pVDZ and TD-M06-2X/cc-pVDZ level of theory, respectively.

<sup>a)</sup> These are scaled values by 0.98 for skeletal vibrations and 0.95 for CH stretching vibrations, respectively. Values in parentheses are transition intensities in km/mol.

<sup>b)</sup> +/- on the shoulder means the signs of the linear combinations, see text. Symmetry species in the D<sub>6h</sub> point group are denoted in parentheses.

Bz (S <sub>0</sub> )		Bz (S <sub>1</sub> )		Bz <sub>2</sub> (S <sub>1</sub> , SW, D <sub>6h</sub> )		Bz <sub>2</sub> (S <sub>1</sub> , T, C <sub>2v</sub> )	
$\nu_{\text{calc}} / \text{cm}^{-1 \text{ a)}$	assignments <sup>b)</sup>	$\nu_{\text{calc}} / \text{cm}^{-1 \text{ a)}$	assignments	$\nu_{\text{calc}} / \text{cm}^{-1 \text{ a)}$	assignments <sup>b)</sup>	$\nu_{\text{calc}} / \text{cm}^{-1 \text{ a)}$	assignments
				66 (0)	R <sub>z</sub>	-26 (0)	R <sub>y</sub>
				104 (0)	$\beta_{(x,y)}$	-9 (0)	R <sub>x</sub>
				104 (0)	$\beta_{(x,y)}$	13 (0)	R <sub>z</sub>
				118 (0.14)	R <sub>(x,y)</sub>	70 (0)	$\sigma_z$
				118 (0.14)	R <sub>(x,y)</sub>	88 (0)	$\beta_x$
				152 (0)	$\sigma_z$	90 (0)	$\beta_y$
404 (0)	16 (e <sub>2u</sub> )	244 (0)	16	348 (0)	16 <sup>-</sup> (e <sub>2g</sub> )	241 (0)	16a (stem)
				366 (0)	16 <sup>+</sup> (e <sub>2u</sub> )	251 (0)	16b (stem)
		253 (0)	4			262 (0)	4 (stem)
						402 (0)	16b (top)
602 (0)	6 (e <sub>2g</sub> )			512 (0)	6 <sup>+</sup> (e <sub>2g</sub> )	403 (0)	16a (top)
		508 (0)	6	576 (0)	6 <sup>-</sup> (e <sub>2u</sub> )	505 (0)	6b (stem)
						514 (0)	6a (stem)
						549 (93)	11 (stem)
712 (0)	4 (b <sub>2g</sub> )			577 (0)	4 <sup>-</sup> (b <sub>1u</sub> )	561 (0)	10a (stem)
				596 (0)	4 <sup>+</sup> (b <sub>2g</sub> )	585 (0)	10b (stem)
678 (92)	11 (a <sub>2u</sub> )	553 (119)	11	625 (83)	11 <sup>+</sup> (a <sub>2u</sub> )	601 (0)	6a (top)
				643 (0)	11 <sup>-</sup> (a <sub>1g</sub> )	601 (0)	6b (top)
858 (0)	10 (e <sub>1g</sub> )	576 (0)	10	749 (0)	10 <sup>+</sup> (e <sub>1g</sub> )	681 (108)	11 (top)
				751 (7.2)	10 <sup>-</sup> (e <sub>1u</sub> )	708 (0)	4 (top)
						752 (0)	17a (stem)
						777 (0)	17b (stem)
981 (0)	17 (e <sub>2u</sub> )	765 (0)	17	875 (0)	17 <sup>-</sup> (e <sub>2g</sub> )	809 (0)	5 (stem)
				881 (0)	17 <sup>+</sup> (e <sub>2u</sub> )	859 (0)	10a (top)
						863 (0)	10b (top)
						964 (1)	1 (stem)
1012 (0)	5 (b <sub>2g</sub> )	807 (0)	5	900 (0)	5 <sup>-</sup> (b <sub>1u</sub> )	969 (1)	12 (stem)
				914 (0)	5 <sup>+</sup> (b <sub>2g</sub> )	974 (1)	18a (stem)
1018 (0)	1 (a <sub>1g</sub> )	963 (0)	1	914 (38)	1 <sup>-</sup> (a <sub>2u</sub> )	977 (3)	18b (stem)
987 (0)	12 (b <sub>1u</sub> )	963 (0)	12	978 (0)	12 <sup>-</sup> (b <sub>2g</sub> )	982 (0)	17a (top)

				979 (0)	12 <sup>+</sup> (b <sub>1u</sub> )	985 (0)	17b (top)
				993 (0)	1 <sup>+</sup> (a <sub>1g</sub> )	987 (0)	12 (top)
1048 (10)	18 (e <sub>1u</sub> )	976 (6)	18	1014 (8.6)	18 <sup>+</sup> (e <sub>1u</sub> )	1012 (0)	5 (top)
				1017 (0)	18 <sup>-</sup> (e <sub>1g</sub> )	1015 (0)	1 (top)
						1047 (4)	18a (top)
						1048 (5)	18b (top)
1129 (0)	15 (b <sub>2u</sub> )	1132 (0)	15	1132 (0)	15 <sup>-</sup> (b <sub>1g</sub> )	1128 (1)	15 (stem)
				1135 (0)	15 <sup>+</sup> (b <sub>2u</sub> )	1131 (0)	15 (top)
1162 (0)	9 (e <sub>2g</sub> )	1146 (0)	9	1135 (0)	9 <sup>-</sup> (e <sub>2u</sub> )	1139 (1)	9a (stem)
				1155 (0)	9 <sup>+</sup> (e <sub>2g</sub> )	1147 (2)	9b (stem)
						1161 (0)	9a (top)
						1164 (0)	9b (top)
1330 (0)	3 (a <sub>2g</sub> )	1315 (0)	3	1321 (0)	3 <sup>-</sup> (a <sub>1u</sub> )	1312 (0)	3 (stem)
				1321 (0)	3 <sup>+</sup> (a <sub>2g</sub> )	1327 (0)	14 (top)
1326 (0)	14 (b <sub>2u</sub> )	1573 (0)	14	1435 (0)	14 <sup>+</sup> (b <sub>2u</sub> )	1331 (0)	3 (top)
1486 (18)	19 (e <sub>1u</sub> )	1420 (14)	19	1449 (44)	19 <sup>+</sup> (e <sub>1u</sub> )	1415 (12)	19a (stem)
				1453 (0)	19 <sup>-</sup> (e <sub>1g</sub> )	1420 (5)	19b (stem)
						1484 (10)	19a (top)
						1486 (9)	19b (top)
				1454 (0)	14 <sup>-</sup> (b <sub>1g</sub> )	1572 (1)	14 (stem)
1649 (0)	8 (e <sub>2g</sub> )	1583 (0)	8	1541 (0)	8 <sup>-</sup> (e <sub>2u</sub> )	1582 (0)	8b (stem)
				1615 (0)	8 <sup>+</sup> (e <sub>2g</sub> )	1582 (0)	8a (stem)
						1644 (0)	8b (top)
						1645 (0)	8a (top)
3039 (0)	13 (b <sub>1u</sub> )	3064 (0)	13	3047 (0)	13 <sup>-</sup> (b <sub>2g</sub> )	3042 (0)	13 (top)
				3048 (0)	13 <sup>+</sup> (b <sub>1u</sub> )	3050 (0)	7b (top)
3048 (0)	7 (e <sub>2g</sub> )	3068 (0)	7	3052 (0)	7 <sup>+</sup> (e <sub>2g</sub> )	3053 (0)	7a (top)
				3055 (0)	7 <sup>-</sup> (e <sub>2u</sub> )	3061 (0)	13 (stem)
						3063 (0)	7b (stem)
						3064 (18)	20b (top)
3063 (52)	20 (e <sub>1u</sub> )	3084 (34)	20	3070 (0)	20 <sup>-</sup> (e <sub>1g</sub> )	3067 (18)	20a (top)
				3071 (68)	20 <sup>+</sup> (e <sub>1u</sub> )	3070 (13)	7a (stem)
						3075 (0)	2 (top)
						3079 (18)	20b (stem)
3072 (0)	2 (a <sub>1g</sub> )	3094 (0)	2	3076 (32)	2 <sup>-</sup> (a <sub>2u</sub> )	3087 (5)	20a (stem)
				3082 (0)	2 <sup>+</sup> (a <sub>1g</sub> )	3115 (3)	2 (stem)

**Table S3** Comparison between the theoretical average frequencies of the  $S_0$  and  $S_1$  states ( $\nu_{ave}$ ) and the EXC state ( $\nu_{EXC}$ ) calculated at M06-2X/cc-pVDZ and TD-M06-2X/cc-pVDZ level of theory with GD3BJ empirical dispersion correction, respectively. The second column lists frequencies in the EXC state,  $\nu_{EXC}$ , and absolute values of splitting of the modes,  $|\Delta\nu_{EXC}(+/-)| = |\nu_{EXC}(+) - \nu_{EXC}(-)|$ , and percentage of the splitting to the average frequencies  $\langle\nu_{EXC}\rangle = (\nu_{EXC}(+) + \nu_{EXC}(-))/2$ . The third column shows deviations from the average values ( $\Delta\nu = \nu_{EXC} - \nu_{ave}$ ) and percentages of difference to the average values.

Mode	$\nu_{ave} / \text{cm}^{-1}$ ( $\nu(S_0)$ ; $\nu(S_1)$ ; $\Delta\nu(S_1/S_0)$ )	$\nu_{EXC} / \text{cm}^{-1}$ ( $ \Delta\nu_{EXC}(+/-) $ ; $ \Delta\nu_{EXC}(+/-) /\langle\nu_{EXC}\rangle$ )	$\Delta\nu / \text{cm}^{-1}$ ( $\Delta\nu / \nu_{ave}$ )
$\nu_{16}$ ( $e_{2u}$ ; op)	324 (404; 244; -160)	241(-), 251(+) (10; 4.1 %)	-83, -73 (-26 %, -23 %)
$\nu_6$ ( $e_{2g}$ ; ip)	555 (602; 508; -94)	512(+), 576(-) (64; 12 %)	-43, -21 (-7.7 %, -3.8 %)
$\nu_4$ ( $b_{2g}$ ; op)	483 (712; 253; -459)	577(-), 596(+) (19; 3.2 %)	+94, +113 (+19 %, +23 %)
$\nu_{11}$ ( $a_{2u}$ ; op)	616 (678; 553; -135)	625(+), 643(-) (18; 2.8 %)	+9, +27 (+1.5 %, +4.4 %)
$\nu_{10}$ ( $e_{1g}$ ; op)	717 (858; 576; -282)	749(+), 751(-) (2; 0.3 %)	+32, +34 (+4.5 %, +4.7 %)
$\nu_{17}$ ( $e_{2u}$ ; op)	873 (981; 765; -216)	875(-), 881(+) (6; 0.7 %)	+2, +8 (+0.2 %, +0.9 %)
$\nu_5$ ( $b_{2g}$ ; op)	910 (1012; 807; -205)	900(-), 914(+) (14; 1.5 %)	-10, +4 (-1.1 %, +0.4 %)
$\nu_1$ ( $a_{1g}$ ; ip)	991 (1018; 963; -55)	914(-), 993(+) (79; 8.3 %)	-77, +2 (-7.8 %, +0.2 %)
$\nu_{12}$ ( $b_{1u}$ ; ip)	975 (987; 963; -24)	978(-), 979(+) (1; 0.1 %)	+3, +4 (+0.3 %, +0.4 %)
$\nu_{18}$ ( $e_{1u}$ ; ip)	1012 (1048; 976; -72)	1014(+), 1017(-) (3; 0.3 %)	+2, +5 (+0.2 %, +0.5 %)
$\nu_{15}$ ( $b_{2u}$ ; ip)	1131 (1129; 1132; +3)	1132(-), 1135(+) (3; 0.3 %)	+1, +4 (+0.1 %, +0.4 %)
$\nu_9$ ( $e_{2g}$ ; ip)	1154 (1162; 1146; -16)	1135(-), 1155(+) (20; 1.7 %)	-7, +13 (-0.4 %, +0.7 %)
$\nu_3$ ( $a_{2g}$ ; ip)	1323 (1330; 1315; -15)	1321(-), 1321(+) (0; 0 %)	-2, -2 (-0.2 %, -0.2 %)
$\nu_{14}$ ( $b_{2u}$ ; ip)	1450 (1326; 1573; +247)	1435(+), 1454(-) (9; 0.6 %)	-15, +4 (-1.0 %, 0.3 %)
$\nu_{19}$ ( $e_{1u}$ ; ip)	1453 (1486; 1420; -66)	1449(+), 1453(-) (4; 0.3 %)	-4, 0 (-0.3 %, 0 %)
$\nu_8$	1616	1541(-), 1615(+)	-76, -1

(e <sub>2g</sub> ; ip)	(1649; 1583; -66)	(74; 4.7 %)	(-4.7 %, -0.1 %)
v <sub>13</sub>	3052	3047(-),3048(+)	-5, -4
(b <sub>2u</sub> ; ip)	(3039; 3064; +25)	(1; 0.0 %)	(-0.2 %, -0.1 %)
v <sub>7</sub>	3058	3052(+),3055(-)	-6, -3
(e <sub>2g</sub> ; ip)	(3048; 3068; +20)	(3; 0.1 %)	(-0.2 %, -0.1 %)
v <sub>20</sub>	3074	3070(-),3071(+)	-4, -3
(e <sub>1u</sub> ; ip)	(3063; 3084; +21)	(1; 0.0 %)	(-0.1 %, -0.1 %)
v <sub>2</sub>	3083	3076(-),3082(+)	-7, -1
(a <sub>1g</sub> ; ip)	(3072; 3094; +22)	(6; 0.2 %)	(-0.2 %, -0.0 %)

**Table S4** Theoretical ( $\nu_{\text{calc}}$ ) vibrational frequencies and the assignments of Bz and Bz<sub>2</sub> in the S<sub>0</sub> and S<sub>1</sub> states calculated by normal mode analyses on the optimized structures obtained by CAM-B3LYP/aug-cc-pVTZ and TD-CAM-B3LYP/aug-cc-pVTZ level of theory with GD3BJ empirical dispersion correction, respectively.

<sup>a)</sup> These are scaled values by 0.98 for skeletal vibrations and 0.95 for CH stretching vibrations, respectively. Values in parentheses are transition intensities in km/mol.

<sup>b)</sup> +/- on the shoulder means the signs of the linear combinations, see text. Symmetry species in the D<sub>6h</sub> point group are denoted in parentheses.

Bz (S <sub>0</sub> )		Bz (S <sub>1</sub> )		Bz <sub>2</sub> (S <sub>1</sub> , SW, D <sub>6h</sub> )		Bz <sub>2</sub> (S <sub>1</sub> , T, C <sub>2v</sub> )	
$\nu_{\text{calc}} / \text{cm}^{-1 \text{ a)}$	assignments <sup>b)</sup>	$\nu_{\text{calc}} / \text{cm}^{-1 \text{ a)}$	assignments	$\nu_{\text{calc}} / \text{cm}^{-1 \text{ a)}$	assignments <sup>b)</sup>	$\nu_{\text{calc}} / \text{cm}^{-1 \text{ a)}$	assignments
				64 (0)	R <sub>z</sub>	-23 (0)	R <sub>x</sub>
				118 (0)	$\beta_{(x,y)}$	11 (0)	R <sub>y</sub>
				118 (0)	$\beta_{(x,y)}$	41(0)	R <sub>z</sub>
				132 (1)	R <sub>(x,y)</sub>	53 (0)	$\sigma_z$
				132 (1)	R <sub>(x,y)</sub>	61 (0)	$\beta_x$
				154 (0)	$\sigma_z$	62 (0)	$\beta_y$
410 (0)	16 (e <sub>2u</sub> )	246 (0)	16 (e <sub>2u</sub> )	359 (0)	16 <sup>-</sup> (e <sub>2g</sub> )	244 (0)	16a (stem)
				382 (0)	16 <sup>+</sup> (e <sub>2u</sub> )	247 (0)	16b (stem)
		340 (0)	4 (b <sub>2g</sub> )			346 (0)	4 (stem)
						410 (0)	16b (top)
617 (0)	6 (e <sub>2g</sub> )			534 (0)	6 <sup>+</sup> (e <sub>2g</sub> )	410 (0)	16a (top)
		524 (0)	6 (e <sub>2g</sub> )	592 (0)	6 <sup>-</sup> (e <sub>2u</sub> )	520 (0)	6b (stem)
						529 (0)	6a (stem)
						562 (120)	11 (stem)
718 (0)	4 (b <sub>2g</sub> )			598 (0)	4 <sup>-</sup> (b <sub>1u</sub> )	617 (0)	6b (top)
				616 (0)	4 <sup>+</sup> (b <sub>2g</sub> )	617(0)	6a (top)
688 (113)	11 (a <sub>2u</sub> )	562 (147)	11 (a <sub>2u</sub> )	643 (117)	11 <sup>+</sup> (a <sub>2u</sub> )	624 (0)	10a (stem)
				675 (0)	11 <sup>-</sup> (a <sub>1g</sub> )	624 (0)	10b (stem)
868 (0)	10 (e <sub>1g</sub> )	623 (0)	10 (e <sub>1g</sub> )	778 (0)	10 <sup>+</sup> (e <sub>1g</sub> )	689 (126)	11 (top)
				774 (4)	10 <sup>-</sup> (e <sub>1u</sub> )	723 (0)	4 (top)
						773 (0)	17a (stem)
						796 (0)	17b (stem)
997 (0)	17 (e <sub>2u</sub> )	778 (0)	17 (e <sub>2u</sub> )	897 (0)	17 <sup>-</sup> (e <sub>2g</sub> )	826 (0)	5 (stem)
				906 (0)	17 <sup>+</sup> (e <sub>2u</sub> )	870 (0)	10b (top)
						870 (0)	10a (top)
						960 (1)	1 (stem)
1023 (0)	5 (b <sub>2g</sub> )	811 (0)	5 (b <sub>2g</sub> )	920 (0)	5 <sup>-</sup> (b <sub>1u</sub> )	978 (2)	18a (stem)
				934 (0)	5 <sup>+</sup> (b <sub>2g</sub> )	979 (5)	18b (stem)
1015 (0)	1 (a <sub>1g</sub> )	961 (0)	1 (a <sub>1g</sub> )	910 (50)	1 <sup>-</sup> (a <sub>2u</sub> )	1000 (1)	12 (stem)

1020 (0)	12 ( $b_{1u}$ )	1000 (0)	12 ( $b_{1u}$ )	1012 (0)	$12^- (b_{2g})$	1000 (0)	17a (top)
				1012 (0)	$12^+ (b_{1u})$	1001 (0)	17b (top)
				994 (0)	$1^+ (a_{1g})$	1012 (0)	1 (top)
1054 (11)	18 ( $e_{1u}$ )	979 (9)	18 ( $e_{1u}$ )	1018 (6)	$18^+ (e_{1u})$	1020 (0)	12 (top)
				1023 (0)	$18^- (e_{1g})$	1029 (0)	5 (top)
						1054 (5)	18b (top)
						1054 (4)	18a (top)
1150 (0)	15 ( $b_{2u}$ )	1159 (0)	15 ( $b_{2u}$ )	1160 (0)	$15^- (b_{1g})$	1152 (0)	15 (top)
				1161 (0)	$15^+ (b_{2u})$	11572 (1)	15 (stem)
1182 (0)	9 ( $e_{2g}$ )	1163 (0)	9 ( $e_{2g}$ )	1153 (0)	$9^- (e_{2u})$	1161 (1)	9a (stem)
				1175 (0)	$9^+ (e_{2g})$	1164 (1)	9b (stem)
						1183 (0)	9a (top)
						1183 (0)	9b (top)
1370 (0)	3 ( $a_{2g}$ )	1351 (0)	3 ( $a_{2g}$ )	1359 (0)	$3^- (a_{1u})$	1307 (0)	14 (top)
				1360 (0)	$3^+ (a_{2g})$	1351 (0)	3 (stem)
1306 (0)	14 ( $b_{2u}$ )	1538 (0)	14 ( $b_{2u}$ )	1414 (0)	$14^+ (b_{2u})$	1371 (0)	3 (top)
1504 (15)	19 ( $e_{1u}$ )	1442 (8)	19 ( $e_{1u}$ )	1472 (16)	$19^+ (e_{1u})$	1440 (6)	19a (stem)
				1474 (0)	$19^- (e_{1g})$	1442 (2)	19b (stem)
						1505 (9)	19a (top)
						1505 (8)	19b (top)
				1428 (0)	$14^- (b_{1g})$	1536 (1)	14 (stem)
1638 (0)	8 ( $e_{2g}$ )	1571 (0)	8 ( $e_{2g}$ )	1542 (0)	$8^- (e_{2u})$	1570 (0)	8b (stem)
				1609 (0)	$8^+ (e_{2g})$	1570 (0)	8a (stem)
						1636 (0)	8b (top)
						1636 (1)	8a (top)
3022 (0)	13 ( $b_{1u}$ )	3049 (0)	13 ( $b_{1u}$ )	3036 (0)	$13^- (b_{2g})$	3025 (0)	13 (top)
				3037 (0)	$13^+ (b_{1u})$	3033 (0)	7b (top)
3032 (0)	7 ( $e_{2g}$ )	3054 (0)	7 ( $e_{2g}$ )	3043 (0)	$7^+ (e_{2g})$	3034 (0)	7a (top)
				3044 (0)	$7^- (e_{2u})$	3048 (19)	20b (top)
						3048 (0)	13 (stem)
						3049 (20)	20a (top)
3046 (54)	20 ( $e_{1u}$ )	3069 (27)	20 ( $e_{1u}$ )	3057 (0)	$20^- (e_{1g})$	3052 (0)	7b (stem)
				3059 (30)	$20^+ (e_{1u})$	3057 (0)	2 (top)
						3059 (11)	7a (stem)
						3067 (14)	20b (stem)
3056 (0)	2 ( $a_{1g}$ )	3079 (0)	2 ( $a_{1g}$ )	3063 (28)	$2^- (a_{2u})$	3074 (2)	2 (stem)
				3070 (0)	$2^+ (a_{1g})$	3100 (4)	20a (stem)



**Table S5** Comparison between theoretical average frequencies of the  $S_0$  and  $S_1$  states ( $\nu_{ave}$ ) and the EXC state ( $\nu_{EXC}$ ) calculated at CAM-B3LYP/aug-cc-pVTZ and TD-CAM-B3LYP/aug-cc-pVTZ level of theory with GD3BJ empirical dispersion correction, respectively. The second column lists frequencies in the EXC state,  $\nu_{EXC}$ , and absolute values of splitting of the modes,  $|\Delta\nu_{EXC}(+/-)| = |\nu_{EXC}(+) - \nu_{EXC}(-)|$ , and percentage of the splitting to the average frequencies  $\langle\nu_{EXC}\rangle = (\nu_{EXC}(+) + \nu_{EXC}(-))/2$ . The third column shows deviations from the average values ( $\Delta\nu = \nu_{EXC} - \nu_{ave}$ ) and percentages of difference to the average values.

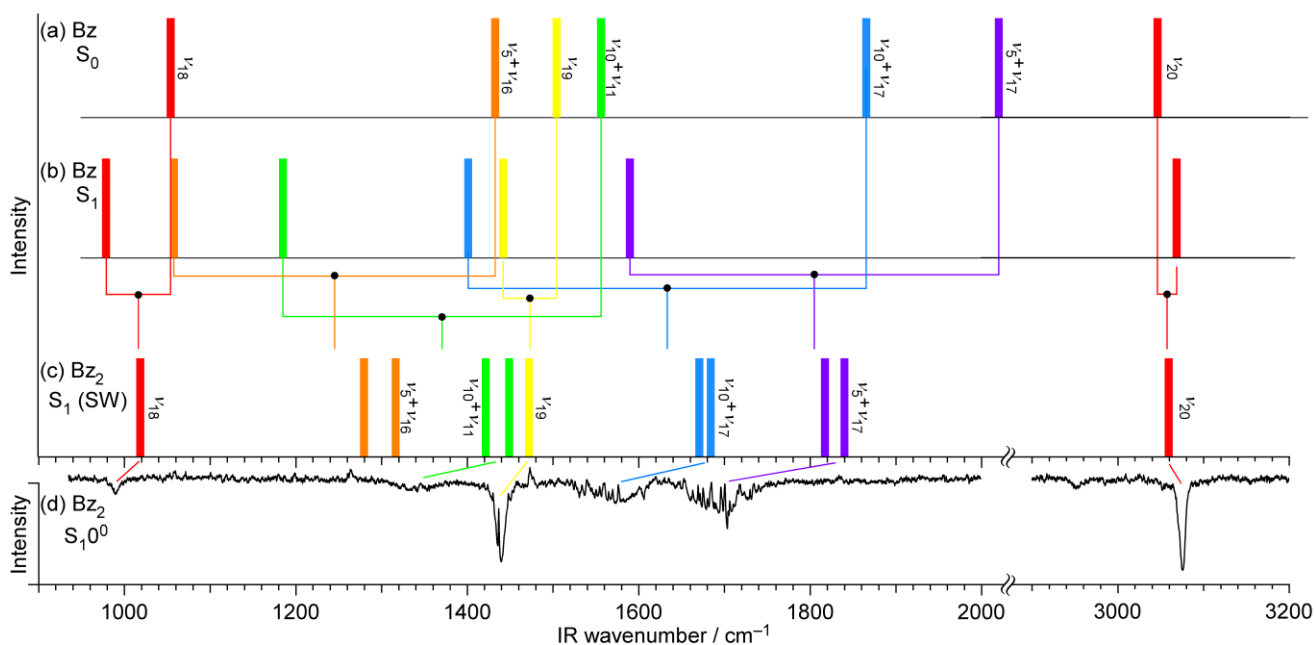
Mode	$\nu_{ave} / \text{cm}^{-1}$ ( $\nu(S_0)$ ; $\nu(S_1)$ ; $\Delta\nu(S_1/S_0)$ )	$\nu_{EXC} / \text{cm}^{-1}$ ( $ \Delta\nu_{EXC}(+/-) $ ; $ \Delta\nu_{EXC}(+/-) /\langle\nu_{EXC}\rangle$ )	$\Delta\nu / \text{cm}^{-1}$ ( $\Delta\nu / \nu_{ave}$ )
$\nu_{16}$ ( $e_{2u}$ ; op)	331 (410; 246; -163)	359 (-), 382 (+) (23; 6.2 %)	+29, +52 (+8.8 %, +15.7 %)
$\nu_6$ ( $e_{2g}$ ; ip)	570 (617; 523; -93)	534 (+), 592 (-) (59; 10.4 %)	-37, +22 (-6.4 %, +3.9 %)
$\nu_4$ ( $b_{2g}$ ; op)	529 (718; 340; -378)	598 (-), 616 (+) (18; 3.0 %)	+69, +87 (+13.0 %, +16.4 %)
$\nu_{11}$ ( $a_{2u}$ ; op)	625 (688; 562; -126)	643 (+), 675 (-) (32; 4.8 %)	+18, +50 (+3.0 %, +8.1 %)
$\nu_{10}$ ( $e_{1g}$ ; op)	746 (868; 623; -246)	778 (+), 774 (-) (5; 0.6 %)	+33, +28 (+4.4 %, +3.8 %)
$\nu_{17}$ ( $e_{2u}$ ; op)	888 (997; 778; -219)	897 (-), 906 (+) (9; 1.0 %)	+10, +18 (+1.1 %, +2.1 %)
$\nu_5$ ( $b_{2g}$ ; op)	917 (1023; 811; -211)	920 (-), 934 (+) (14; 1.5 %)	+3, +17 (+0.3 %, +1.8 %)
$\nu_1$ ( $a_{1g}$ ; ip)	988 (1015; 961; -54)	910 (-), 994 (+) (83; 8.8 %)	-78, +6 (-7.9 %, +0.6 %)
$\nu_{12}$ ( $b_{1u}$ ; ip)	1010 (1020; 1000; -20)	1012 (-), 1012 (+) (0; 0.0 %)	+2, +3 (+0.2 %, +0.3 %)
$\nu_{18}$ ( $e_{1u}$ ; ip)	1016 (1054; 979; -75)	1018 (+), 1023 (-) (5; 0.4 %)	+2, +7 (+0.2 %, +0.7 %)
$\nu_{15}$ ( $b_{2u}$ ; ip)	1155 (1150; 1159; +9)	1160 (-), 1161 (+) (1; 0.1 %)	+5, +6 (+0.4 %, +0.5 %)
$\nu_9$ ( $e_{2g}$ ; ip)	1173 (1182; 1163; -19)	1153 (-), 1175 (+) (22; 1.9 %)	-20, +2 (-1.7 %, +0.2 %)
$\nu_3$ ( $a_{2g}$ ; ip)	1361 (1370; 1351; -19)	1359 (-), 1360 (+) (1; 0.1 %)	-1, -0 (-0.1 %, -0.0 %)
$\nu_{14}$ ( $b_{2u}$ ; ip)	1422 (1306; 1538; +232)	1414 (+), 1428 (-) (13.89; 0.98 %)	-8, +6 (-0.5 %, +0.4 %)
$\nu_{19}$ ( $e_{1u}$ ; ip)	1473 (1504; 1442; -62)	1472 (+), 1474 (-) (2; 0.2 %)	-1, +1 (-0.1 %, +0.1 %)
$\nu_8$	1605	1542 (-), 1609 (+)	-63, +4

$(e_{2g}; ip)$	(1638; 1571; -67)	(67; 4 %)	(-3.9 %, +0.2 %)
$v_{13}$	3036	3036 (-), 3037 (+)	+0, +2
$(b_{2u}; ip)$	(3022; 3049; +27)	(1; 0.1 %)	(+0.0 %, +0.1 %)
$v_7$	3043	3043 (+), 3044 (-)	-0, -1
$(e_{2g}; ip)$	(3032; 3054; +22)	(1; 0.0 %)	(-0.0 %, -0.0 %)
$v_{20}$	3058	3057 (-), 3059 (+)	-0, +2
$(e_{1u}; ip)$	(3046; 3069; +22)	(2; 0.1 %)	(-0.0 %, +0.1 %)
$v_2$	3067	3063 (-), 3070 (+)	-4, +2
$(a_{1g}; ip)$	(3056; 3079; +23)	(6; 0.2 %)	(-0.1 %, +0.1 %)

**Table S6** Comparison between average frequencies in the  $S_0$  and  $S_1$  states ( $\nu_{ave}$ ) and those in the EXC state ( $\nu_{EXC}$ ). Difference of these values ( $\Delta\nu = \nu_{EXC} - \nu_{ave}$ ) are listed in the third column. Calculated values obtained by CAM-B3LYP/aug-cc-pVTZ and TD-CAM-B3LYP/aug-cc-pVTZ levels of theory with GD3BJ empirical dispersion correction are shown below the experimental values. Two IR active modes are possible for combination modes from degenerate species, see text.

<sup>a)</sup> Deperturbed values taken from ref. 84 and ref. 87.

Mode		$\nu_{ave} / \text{cm}^{-1}$ ( $S_0; S_1 6^1$ )	$\nu_{EXC} / \text{cm}^{-1}$ (FWHM / $\text{cm}^{-1}$ )	$\Delta\nu / \text{cm}^{-1}$ ( $\Delta\nu / \nu_{ave}$ )
$\nu_{18}$ (in plane)	Obs	980 (1040; 920)	989 (12)	+9 (+0.9 %)
	Calc	1016 (1054; 979; -75)	1018	+2 (+0.2 %)
$\nu_5 + \nu_{16}$ (out-of-plane)	Obs	– (1390; –)	– (–)	– (–)
	Calc	1245 (1433; 1053)	1280, 1317	+34, +71 (+2.8 %, +5.7 %)
$\nu_{10} + \nu_{11}$ (out-of-plane)	Obs	1308 (1519; 1096)	1340 (~60)	+32 (+2.4 %)
	Calc	1370 (1556; 1185)	1421, 1449	+51, +78 (+3.7 %, +5.7 %)
$\nu_{19}$ (in plane)	Obs	1444 (1485; 1402)	1439 (9)	–5 (–0.3 %)
	Calc	1473 (1504; 1442)	1472	–1 (–0.1 %)
$\nu_{10} + \nu_{17}$ (out-of-plane)	Obs	1557 (1814; 1300)	1570 (~80)	+13 (+0.8 %)
	Calc	1633 (1865; 1401)	1671, 1684	+37, +51 (+2.3 %, +3.1 %)
$\nu_5 + \nu_{17}$ (out-of-plane)	Obs	1713 (1960; 1465)	1700 (~60)	–13 (–0.6 %)
	Calc	1805 (2020; 1590)	1817, 1840	+12, +35 (+0.7 %, +2.0 %)
$\nu_{20}$ (in plane)	Obs	3072 (3065; 3079) <sup>a)</sup>	3075 (6)	+3 (+0.1 %)
	Calc	3057 (3046; 3069)	3059	+2 (+0.1 %)



**Figure S2** Comparison of vibration frequencies of (a) Bz in  $S_0$ , (b) Bz in  $S_1$  and (c) Bz<sub>2</sub> in  $S_1$  states (SW structure) obtained by CAM-B3LYP/aug-cc-pVTZ and TD-CAM-B3LYP/aug-cc-pVTZ levels of theory with the GD3BJ empirical dispersion correction, and the experimental spectrum (d). Positions of the combination bands are calculated as simple sums of the respective fundamental frequencies. Black circles indicate the average positions of the vibration frequencies in the  $S_0$  and  $S_1$  states of Bz. Vertical lines down from the circles compare the average positions with frequencies calculated for the SW EXC state. In the panel (c), two bars with the same color show positions of two different IR active combinations, see the main text. This is a figure corresponding to Figure 5 in the main text but with the CAM-B3LYP functional.

The full expression of the excimer state vibrational energy,  $E_{v_{\pm}}^{+/-}$ , derived from the secular determinant given by equation (33) in Appendix.

Since the secular determinant derives a quadratic equation, the solution is written in the standard form:

$$E_{v_{\pm}}^{+/-} = \frac{B^{+/-} \pm \sqrt{C}}{2A}. \quad (S1)$$

Here, factors  $A$ ,  $B$ , and  $C$  are expressed as follows (notation of factors follows that in **Appendix**):

$$\begin{aligned} A &= \left\{1 \pm \langle S \rangle \langle FC_{0^*v}^{\phi} \rangle^2 \mathbf{FC}_{0^*0}{}^2\right\} \left\{1 \pm \langle S \rangle \langle FC_{v^*0}^{\phi} \rangle^2 \mathbf{FC}_{0^*0}{}^2\right\} - \langle S \rangle^2 \langle FC_{v^*v}^{\phi} \rangle^2 \mathbf{FC}_{0^*0}{}^4 \\ &= 1 \pm \langle S \rangle \left( \langle FC_{0^*v}^{\phi} \rangle^2 + \langle FC_{v^*0}^{\phi} \rangle^2 \right) \mathbf{FC}_{0^*0}{}^2 + \langle S \rangle^2 \left( \langle FC_{0^*v}^{\phi} \rangle^2 \langle FC_{v^*0}^{\phi} \rangle^2 - \langle FC_{v^*v}^{\phi} \rangle^2 \right) \mathbf{FC}_{0^*0}{}^4, \end{aligned} \quad (S2)$$

$$\begin{aligned} B &= \left\{1 \pm \langle S \rangle \langle FC_{v^*0}^{\phi} \rangle^2 \mathbf{FC}_{0^*0}{}^2\right\} \left\{hv \pm (\langle EXC \rangle + 2\langle S \rangle \langle T_{0^*v} \rangle) \langle FC_{0^*v}^{\phi} \rangle^2 \mathbf{FC}_{0^*0}{}^2\right\} \\ &\quad + \left\{1 \pm \langle S \rangle \langle FC_{0^*v}^{\phi} \rangle^2 \mathbf{FC}_{0^*0}{}^2\right\} \left\{hv^* \pm (\langle EXC \rangle + 2\langle S \rangle \langle T_{v^*0} \rangle) \langle FC_{v^*0}^{\phi} \rangle^2 \mathbf{FC}_{0^*0}{}^2\right\} \\ &\quad - 2\langle S \rangle (\langle EXC \rangle + \langle S \rangle \langle T_{v^*v} \rangle) \langle FC_{v^*0}^{\phi} \rangle^2 \mathbf{FC}_{0^*0}{}^4 \\ &= hv + hv^* \pm \left( (\langle EXC \rangle + 2\langle S \rangle \langle T_{0^*v} \rangle) \langle FC_{0^*v}^{\phi} \rangle^2 + (\langle EXC \rangle + 2\langle S \rangle \langle T_{v^*0} \rangle) \langle FC_{v^*0}^{\phi} \rangle^2 + \langle S \rangle \left( \langle FC_{0^*v}^{\phi} \rangle^2 hv^* + \langle FC_{v^*0}^{\phi} \rangle^2 hv \right) \right) \mathbf{FC}_{0^*0}{}^2 + \\ &\quad 2\langle S \rangle \left( (\langle EXC \rangle + \langle S \rangle (\langle T_{0^*v} \rangle + \langle T_{v^*0} \rangle)) \langle FC_{0^*v}^{\phi} \rangle^2 \langle FC_{v^*0}^{\phi} \rangle^2 - (\langle EXC \rangle + \langle S \rangle \langle T_{v^*v} \rangle) \langle FC_{v^*v}^{\phi} \rangle^2 \right) \mathbf{FC}_{0^*0}{}^4, \end{aligned} \quad (S3)$$

$$\begin{aligned} C &= \\ &\left[ \left\{1 \pm \langle S \rangle \langle FC_{v^*0}^{\phi} \rangle^2 \mathbf{FC}_{0^*0}{}^2\right\} \left\{hv \pm (\langle EXC \rangle + 2\langle S \rangle \langle T_{0^*v} \rangle) \langle FC_{0^*v}^{\phi} \rangle^2 \mathbf{FC}_{0^*0}{}^2\right\} - \right. \\ &\left. \left\{1 \pm \langle S \rangle \langle FC_{0^*v}^{\phi} \rangle^2 \mathbf{FC}_{0^*0}{}^2\right\} \left\{hv^* \pm (\langle EXC \rangle + 2\langle S \rangle \langle T_{v^*0} \rangle) \langle FC_{v^*0}^{\phi} \rangle^2 \mathbf{FC}_{0^*0}{}^2\right\} \right]^2 + 4 \langle FC_{v^*v}^{\phi} \rangle^2 \mathbf{FC}_{0^*0}{}^4 \left[ \langle S \rangle hv - \right. \\ &\left. (\langle EXC \rangle + \langle S \rangle \langle T_{v^*v} \rangle) \right] \pm \langle S \rangle^2 (2\langle T_{0^*v} \rangle - \langle T_{v^*v} \rangle) \langle FC_{0^*v}^{\phi} \rangle^2 \mathbf{FC}_{0^*0}{}^2 \left[ \langle S \rangle hv^* - (\langle EXC \rangle + \langle S \rangle \langle T_{v^*v} \rangle) \right] \pm \\ &\left. \langle S \rangle^2 (2\langle T_{v^*0} \rangle - \langle T_{v^*v} \rangle) \langle FC_{v^*0}^{\phi} \rangle^2 \mathbf{FC}_{0^*0}{}^2 \right]. \end{aligned} \quad (S4)$$

In the case of a non-totally symmetric mode, two FC factors vanish due to a requirement of the symmetry,  $\langle FC_{0^*v}^{\phi} \rangle = \langle FC_{v^*0}^{\phi} \rangle = 0$ . This condition reduces the above terms as follows:

$$A = 1 - \langle S \rangle^2 \langle FC_{v^*v}^{\phi} \rangle^2 \mathbf{FC}_{0^*0}{}^4, \quad (S2')$$

$$B = hv + hv^* - 2\langle S \rangle (\langle EXC \rangle + \langle S \rangle \langle T_{v^*v} \rangle) \langle FC_{v^*v}^{\phi} \rangle^2 \mathbf{FC}_{0^*0}{}^4, \quad (S3')$$

$$\begin{aligned}
C &= (hv - hv^*)^2 + 4 \langle FC_{v^*v}^\phi \rangle^2 \mathbf{FC}_{0^*0}^4 \{ \langle S \rangle hv - (\langle EXC \rangle + \langle S \rangle \langle T_{v^*v} \rangle) \} \{ \langle S \rangle hv^* - (\langle EXC \rangle + \langle S \rangle \langle T_{v^*v} \rangle) \} \\
&= \left\{ 1 - \langle S \rangle^2 \langle FC_{v^*v}^\phi \rangle^2 \mathbf{FC}_{0^*0}^4 \right\} (hv - hv^*)^2 + \{ 2(\langle EXC \rangle + \langle S \rangle \langle T_{v^*v} \rangle) - \langle S \rangle (hv + hv^*) \}^2 \langle FC_{v^*v}^\phi \rangle^2 \mathbf{FC}_{0^*0}^4.
\end{aligned} \tag{S4'}$$

The first term of equation (S4') is considered to be much smaller than the second term because of a factor of vibrational energy difference. Thus, square root of equation (S4') can be expanded as follows:

$$\begin{aligned}
\sqrt{C} &= \\
&\{ 2(\langle EXC \rangle + \langle S \rangle \langle T_{v^*v} \rangle) - \\
&\langle S \rangle (hv + hv^*) \} \langle FC_{v^*v}^\phi \rangle \mathbf{FC}_{0^*0}^2 \left( 1 + \frac{\{ 1 - \langle S \rangle^2 \langle FC_{v^*v}^\phi \rangle^2 \mathbf{FC}_{0^*0}^4 \} (hv - hv^*)^2}{\{ 2(\langle EXC \rangle + \langle S \rangle \langle T_{v^*v} \rangle) - \langle S \rangle (hv + hv^*) \}^2 \langle FC_{v^*v}^\phi \rangle^2 \mathbf{FC}_{0^*0}^4} \right)^{\frac{1}{2}} \\
&\approx \{ 2(\langle EXC \rangle + \langle S \rangle \langle T_{v^*v} \rangle) - \langle S \rangle (hv + hv^*) \} \langle FC_{v^*v}^\phi \rangle \mathbf{FC}_{0^*0}^2 + \frac{1}{2} \frac{\{ 1 - \langle S \rangle^2 \langle FC_{v^*v}^\phi \rangle^2 \mathbf{FC}_{0^*0}^4 \} (hv - hv^*)^2}{\{ 2(\langle EXC \rangle + \langle S \rangle \langle T_{v^*v} \rangle) - \langle S \rangle (hv + hv^*) \} \langle FC_{v^*v}^\phi \rangle \mathbf{FC}_{0^*0}^2}.
\end{aligned} \tag{S5'}$$

Then, the expression of  $E_{v_\pm}^{+/-'}$ , which is used in the appendix as equation (36), can be obtained by substituting equation (S2')–(S5') into (S1).

$$\begin{aligned}
E_{v_\pm}^{+/-'} &\approx \frac{(hv + hv^*)}{2(1^{+/-} - \langle S \rangle \langle FC_{v^*v}^\phi \rangle \mathbf{FC}_{0^*0}^2)} + / - \frac{(\langle EXC \rangle + \langle S \rangle \langle T_{v^*v} \rangle) \langle FC_{v^*v}^\phi \rangle \mathbf{FC}_{0^*0}^2}{(1^{+/-} - \langle S \rangle \langle FC_{v^*v}^\phi \rangle \mathbf{FC}_{0^*0}^2)} \\
&\quad + / - \frac{(hv - hv^*)^2}{4\{ 2(\langle EXC \rangle + 2\langle S \rangle \langle T_{v^*v} \rangle) - \langle S \rangle (hv + hv^*) \} \langle FC_{v^*v}^\phi \rangle \mathbf{FC}_{0^*0}^2}
\end{aligned} \tag{S6}$$