

Supplementary Information for: Explaining the symmetry breaking observed in the endofullerenes $\text{H}_2\text{@C}_{60}$, HF@C_{60} , and $\text{H}_2\text{O@C}_{60}$

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1 Molecular and Crystal-fragment Parameters

Tables S1 and S2 summarize the geometries, inertial parameters, and BF quadrupole components that we have assumed for the H_2 and H_2O moieties in computing the TR states of $\text{H}_2\text{@C}_{60}$ and $\text{H}_2\text{O@C}_{60}$, respectively.

Table S3 gives the C nuclear coordinates for the C_{60} “master-cage” geometry assumed for all the C_{60} moieties relevant to this work. The geometry has shared-hexagon (6:6) CC bond lengths equal to 2.60820 bohrs (1.38020 Å) and hexagon-pentagon (6:5) CC bond lengths equal to 2.73047 bohrs (1.44490 Å). The cage-fixed cartesian axis system is centered at the

C_{60} center of mass, has its z axis along one of the C_5 symmetry axes of the cage, and its x axis along one of the C_2 symmetry axes of the cage.

Tables S4 and S5 give the cage-center translation vectors ($\mathbf{T}(k)$) and the direction-cosine matrices ($\hat{R}(k)$) that define the positions and orientations of the thirteen cages in the P and H crystal fragments, respectively, w.r.t. the “space-fixed” (SF) cartesian axis system. These parameters conform to the C_{60} crystal geometries described in Sachidanandam and Harris¹ and Harris and Sachidanandam² for the angle ϕ (defined in those papers) equal to 24° (P orientation) and 84° (H orientation). The SF frame has its origin at the center of the central cage (cage #13) and is oriented such that the C_3 symmetry axis of the fragment is along the (1, 1, 1) direction. To obtain the position vector, \mathbf{R}_i , of the i th C nucleus of cage k relative to the SF frame one uses

$$\mathbf{R}_i = \mathbf{T}(k) + \hat{R}(k)\mathbf{D}_i, \quad (1)$$

where \mathbf{D}_i is the position vector, as given in Table S3, of the i th C nucleus in the cage-fixed axis system. In Tables S4 and S5, cages 1 to 6 are the “axial” and cages 7 to 12 are the “equatorial” cages in the fragment.

2 Basis sets, Grid Parameters, and Lennard-Jones Potential-Energy Parameters

2.1 $H_2@C_{60}$

2.1.1 Basis Functions

The basis functions employed in the variational calculations of the TR states of $H_2@C_{60}$ are of the form $|n, l, m_l\rangle|j, m_j\rangle$.

The $|n, l, m_l\rangle$ are 3D isotropic harmonic-oscillator eigenfunctions:³

$$|n, l, m_l\rangle = N_{nl}R^l e^{-\beta R^2/2} L_k^{(l+1/2)}(\beta R^2) Y_{lm_l}(\Theta, \Phi), \quad (2)$$

where $\beta = 2.9888989$ au, $n = 0, 1, 2, \dots, n_{\max}$, $l = n, n - 2, \dots \geq 0$, $k \equiv (n - l)/2$, $m_l = -l, (-l + 1), \dots, (l - 1), l$,

$$N_{nl} = 2 \left[\frac{\beta^{(2l+3/2)} 2^{k+l} k!}{\sqrt{\pi} [2(k+l) + 1]!!} \right]^{1/2}, \quad (3)$$

the $L_k^{(l+1/2)}$ are associated Laguerre polynomials, and the Y_{lm_l} are spherical harmonics. We used $n_{\max} = 8$.

The $|j, m_j\rangle$ are spherical harmonics

$$|j, m_j\rangle = Y_{jm_j}(\theta, \phi), \quad (4)$$

where $j = 0, 1, 2, \dots, j_{\max}$ and $m_j = -j, (-j + 1), \dots, (j - 1), j$. We used $j_{\max} = 8$.

2.1.2 Grid Parameters

The 5D grid described in Section 2.5 of the main body of the paper consists of (i) $N_a = 12$ Gauss-associated-Laguerre quadrature points R_a , generated as per Felker and Bačić⁴ for $\beta = 2.9888989$ au, (ii) $N_b = 10$ Gauss-Legendre quadrature points $(\cos \beta)_b$, (iii) $N_c = 18$ Fourier grid points α_c , (iv) $N_d = 10$ Gauss-Legendre quadrature points $(\cos \theta)_d$, and (v) $N_e = 18$ Fourier grid points ϕ_e .

2.1.3 Kinetic-Energy Operator, \hat{T}

For $\text{H}_2@C_{60}$ in the rigid-monomer approximation

$$\hat{T} = -\frac{\nabla^2}{2M} + \frac{\hat{J}^2}{2I}, \quad (5)$$

where ∇^2 is the Laplacian associated with \mathbf{R} , \hat{J}^2 is the operator corresponding to the square of the rotational angular momentum of the H_2 , M is the mass of the H_2 , and I is the moment of inertia of the H_2 . The inertial parameters that we have employed are given in Table S1.

2.1.4 Lennard-Jones Potential-Energy Parameters

The V_{LJ} PES function appearing in \hat{H} for $\text{H}_2@\text{C}_{60}$ is taken from Xu, et al.⁵ and is given by

$$V_{LJ} = \sum_{i=1}^3 \sum_{k=1}^{60} 4w_i \epsilon \left[\left(\frac{\sigma}{r_{ik}} \right)^{12} - \left(\frac{\sigma}{r_{ik}} \right)^6 \right], \quad (6)$$

where i runs over the three H_2 sites listed in Table S1, k runs over the 60 nuclear positions of the C atoms in the central cage, r_{ik} is the distance between site i and site k , $w_1 = 6.7$, $w_2 = w_3 = 1$, $\sigma = 5.574692$ bohrs (2.95 Å), and $\epsilon = 3.07 \text{ cm}^{-1}$. Of course, the r_{ik} depend on the position of the H_2 moiety w.r.t. the SF axes, so V_{LJ} is a function of \mathbf{R} and ω .

2.2 $\text{H}_2\text{O}@\text{C}_{60}$

2.2.1 Basis Functions

The basis functions employed in the variational calculations of the TR states of $\text{H}_2\text{O}@\text{C}_{60}$ are of the form $|n, l, m_l\rangle |j, m_j, k\rangle$. The $|n, l, m_l\rangle$ are the same as for $\text{H}_2@\text{C}_{60}$ except that $\beta = 24.38$ au. The $|j, m_j, k\rangle$ are normalized Wigner rotation matrix elements

$$|j, m_j, k\rangle = \sqrt{\frac{2j+1}{8\pi^2}} [D_{m_j, k}^{(j)}(\phi, \theta, \chi)]^*, \quad (7)$$

where $j = 0, 1, 2, \dots, j_{\max}$, $m_j = -j, (-j+1), \dots, (j-1), j$, and $k = -j, (-j+1), \dots, (j-1), j$. We used $j_{\max} = 8$.

2.2.2 Grid Parameters

The 6D grid described in Section 2.5 of the main body of the paper consisted of (i) $N_a = 12$ Gauss-associated-Laguerre quadrature points R_a , generated as per Felker and Bačić⁴ for $\beta = 24.38$ au, (ii) $N_b = 10$ Gauss-Legendre quadrature points $(\cos \beta)_b$, (iii) $N_c = 18$ Fourier grid points α_c , (iv) $N_d = 10$ Gauss-Legendre quadrature points $(\cos \theta)_d$, and (v) $N_e = 18$ Fourier grid points ϕ_e , and (vi) $N_f = 18$ Fourier grid points χ_f .

2.2.3 Kinetic-Energy Operator, \hat{T}

For $\text{H}_2\text{O}@\text{C}_{60}$ in the rigid-monomer approximation

$$\hat{T} = -\frac{\nabla^2}{2M} + \sum_{k=x,y,z} \frac{\hat{J}_k^2}{2I_k}, \quad (8)$$

where ∇^2 is the Laplacian associated with \mathbf{R} , \hat{J}_k^2 is the operator corresponding to the square of the rotational angular momentum of the H_2O about its k th principal axis, M is the mass of the H_2O , and I_k is the moment of inertia of H_2O about its k th principal axis. The inertial parameters that we have employed are given in Table S2.

2.2.4 Lennard-Jones Potential-Energy Parameters

The V_{LJ} PES function appearing in \hat{H} for $\text{H}_2\text{O}@\text{C}_{60}$ is taken from Felker and Bačić⁸ and is given by

$$V_{LJ} = \sum_{i=1}^3 \sum_{k=1}^{60} 4\epsilon_i \left[\left(\frac{\sigma_i}{r_{ik}} \right)^{12} - \left(\frac{\sigma_i}{r_{ik}} \right)^6 \right], \quad (9)$$

where i runs over the three H_2O sites listed in Table S2, k runs over the 60 nuclear positions of the C atoms in the central cage, r_{ik} is the distance between site i and site k , $\sigma_1 = 6.37216$ bohrs (3.372 Å), $\sigma_2 = \sigma_3 = 4.988877$ bohrs (2.640 Å), $\epsilon_1 = 36.34 \text{ cm}^{-1}$, and $\epsilon_2 = \epsilon_3 = 8.95384 \text{ cm}^{-1}$. The r_{ik} depend on the position of the H_2O moiety w.r.t. the SF axes, so V_{LJ} is a function of \mathbf{R} and ω .

3 Transformation properties of the electric-field-gradient tensor, $I_m^{(2)}$

For arbitrary charge density $\rho(\mathbf{r})$ the internal moments of rank 2 (the components of the electric-field-gradient tensor) are given by⁶

$$I_m^{(2)} \equiv \int \frac{\rho(\mathbf{r})}{r^3} C_m^{(2)}(\hat{r}) d\mathbf{r} = \sqrt{\frac{4\pi}{5}} \int \frac{\rho(\mathbf{r})}{r^3} Y_{2m}(\hat{r}) d\mathbf{r}. \quad (10)$$

We examine below how these moments transform subject to (a) inversion through the origin and (b) rotation about an axis going through the origin.

3.1 Transformation by inversion

Inversion (operation E^*) changes the charge density $\rho(\mathbf{r})$ to $\rho'(\mathbf{r})$ such that

$$\rho'(\mathbf{r}) = \rho(-\mathbf{r}). \quad (11)$$

The internal moments corresponding to this new charge density are given by

$$\begin{aligned} I_m^{(2)}(E^*) &= \sqrt{\frac{4\pi}{5}} \int \frac{\rho'(\mathbf{r})}{r^3} Y_{2m}(\hat{r}) d\mathbf{r} = \sqrt{\frac{4\pi}{5}} \int \frac{\rho(-\mathbf{r})}{r^3} Y_{2m}(\hat{r}) d\mathbf{r} \\ &= \sqrt{\frac{4\pi}{5}} \int \frac{\rho(\mathbf{r}')}{r'^3} Y_{2m}(-\hat{r}') d\mathbf{r}', \end{aligned} \quad (12)$$

where we have substituted $\mathbf{r}' = -\mathbf{r}$ to obtain the final equality. Since $Y_{2m}(-\hat{r}') = Y_{2m}(\hat{r}')$, one sees from Eqs. (10) and (12) that

$$I_m^{(2)}(E^*) = I_m^{(2)}. \quad (13)$$

Inversion leaves internal moments of rank 2 unchanged.

3.2 Transformation by rotation about an axis through the origin

We start by expressing $\rho(\mathbf{r})$ as an expansion over spherical harmonics

$$\rho(\mathbf{r}) = \sum_{l,m} a_{lm}(r) Y_{lm}(\hat{r}), \quad (14)$$

where

$$a_{lm}(r) = \int \rho(\mathbf{r}) Y_{lm}^*(\hat{r}) d\hat{r}. \quad (15)$$

Next we substitute this expansion for $\rho(\mathbf{r})$ into Eq. (10) to obtain

$$\begin{aligned} I_m^{(2)} &= \sqrt{\frac{4\pi}{5}} \sum_{l,m'} \int \frac{a_{lm'}(r)}{r^3} Y_{lm'}(\hat{r}) Y_{2m}(\hat{r}) d\mathbf{r} \\ &= \sqrt{\frac{4\pi}{5}} (-)^m \int \frac{a_{2,-m}(r)}{r^3} dr, \end{aligned} \quad (16)$$

where the last equality in Eq. (16) follows from the orthonormality of the spherical harmonics and the fact that

$$Y_{lm}^* = (-)^m Y_{l,-m}. \quad (17)$$

Now we rotate the charge density $\rho(\mathbf{r})$ through an angle γ about an axis \hat{n} going through the origin. The density is transformed as follows

$$e^{-i\hat{J}_n\gamma} \rho(\mathbf{r}) = \sum_{l,m} a_{lm}(r) [e^{-i\hat{J}_n\gamma} Y_{lm}(\hat{r})], \quad (18)$$

where \hat{J}_n is the operator corresponding to angular momentum about \hat{n} .

Consider the new $I_m^{(2)}$ – call them $I_m^{(2)}(\hat{n}, \gamma)$ – corresponding to this rotated density

$$\begin{aligned} \sqrt{\frac{5}{4\pi}} I_m^{(2)}(\hat{n}, \gamma) &= \int \frac{[e^{-i\hat{J}_n\gamma} \rho(\mathbf{r})]}{r^3} Y_{2m}(\hat{r}) d\mathbf{r} \\ &= \sum_{l,m'} \int \frac{a_{l,m'}(r)}{r^3} dr \int [e^{-i\hat{J}_n\gamma} Y_{lm'}] Y_{2m} d\hat{r}. \end{aligned} \quad (19)$$

Now

$$e^{-i\hat{J}_n\gamma}Y_{lm'}(\hat{r}) = \sum_{m''} A_{m'',m'}^{(l)}(\hat{n}, \gamma)Y_{lm''}(\hat{r}), \quad (20)$$

where

$$A_{m'',m'}^{(l)}(\hat{n}, \gamma) \equiv \int Y_{lm''}^*(\hat{r})e^{-i\hat{J}_n\gamma}Y_{lm'}(\hat{r})d\hat{r}. \quad (21)$$

Substituting Eq. (20) into Eq. (19) one obtains

$$\begin{aligned} \sqrt{\frac{5}{4\pi}}I_m^{(2)}(\hat{n}, \gamma) &= \sum_{l,m'} \left[\int \frac{a_{l,m'}(r)}{r^3} dr \times \sum_{m''} A_{m'',m'}^{(l)}(\hat{n}, \gamma) \int Y_{lm''}(\hat{r})Y_{2m}(\hat{r})d\hat{r} \right] \\ &= \sum_{m'} (-)^m A_{-m,m'}^{(2)}(\hat{n}, \gamma) \int \frac{a_{2,m'}(r)}{r^3} dr. \end{aligned} \quad (22)$$

By using Eq. (16) one then obtains

$$I_m^{(2)}(\hat{n}, \gamma) = \sum_{m'} (-)^{m+m'} A_{-m,m'}^{(2)}(\hat{n}, \gamma)I_{-m'}^{(2)} = \sum_{m'} (-)^{m+m'} A_{-m,-m'}^{(2)}(\hat{n}, \gamma)I_{m'}^{(2)}. \quad (23)$$

What remains is to evaluate the $A_{m,m'}^{(2)}(\hat{n}, \gamma)$. If one specifies the direction of the axis \hat{n} by its polar angle β and azimuthal angle α , it is straightforward to show that

$$A_{m,m'}^{(l)}(\alpha, \beta, \gamma) \equiv A_{m,m'}^{(l)}(\hat{n}, \gamma) = e^{i(m'-m)\alpha} \sum_{m''} e^{-im''\gamma} d_{m,m''}^{(l)}(\beta) d_{m'',m'}^{(l)}(\beta), \quad (24)$$

where the $d_{m,m'}^{(l)}(\beta)$ are little- d Wigner rotation matrix elements. From Eq. (24), one can also easily show that

$$(-)^{m+m'} A_{-m,-m'}^{(l)}(\hat{n}, \gamma) = [A_{m,m'}^{(l)}(\hat{n}, \gamma)]^* \quad (25)$$

and that

$$(-)^{m+m'} A_{-m,-m'}^{(l)}(\hat{n}, -\gamma) = A_{m',m}^{(l)}(\hat{n}, \gamma). \quad (26)$$

Finally, with Eqs. (23), (25), and (26)

$$I_m^{(2)}(\hat{n}, \gamma) = \sum_{m'} [A_{m,m'}^{(2)}(\hat{n}, \gamma)]^* I_{m'}^{(2)} \quad (27)$$

and

$$I_m^{(2)}(\hat{n}, -\gamma) = \sum_{m'} A_{m',m}^{(2)}(\hat{n}, \gamma) I_{m'}^{(2)}. \quad (28)$$

Relevant to the M@C₆₀ crystal-fragment geometries in this work are the rotations by $\pm 2\pi/3$ about \hat{n} when \hat{n} lies along the (1, 1, 1) direction, so that $\beta = \cos^{-1}(\sqrt{1/3})$ and $\alpha = \pi/4$. Evaluation of Eq. (24) for $\gamma = +2\pi/3$ about this axis and for $l = 2$ yields the matrix of values

$$\mathbf{B} \equiv \mathbf{A}^{(2)}(\pi/4, \cos^{-1}(\sqrt{1/3}), 2\pi/3) = \begin{pmatrix} -\frac{1}{4} & \frac{1}{2} & -\sqrt{\frac{3}{8}} & \frac{1}{2} & -\frac{1}{4} \\ \frac{i}{2} & -\frac{i}{2} & 0 & \frac{i}{2} & -\frac{i}{2} \\ \sqrt{\frac{3}{8}} & 0 & -\frac{1}{2} & 0 & \sqrt{\frac{3}{8}} \\ -\frac{i}{2} & -\frac{i}{2} & 0 & \frac{i}{2} & \frac{i}{2} \\ -\frac{1}{4} & -\frac{1}{2} & -\sqrt{\frac{3}{8}} & -\frac{1}{2} & -\frac{1}{4} \end{pmatrix}, \quad (29)$$

where the rows run from $m = -2$ to 2 and the columns from $m' = -2$ to 2.

3.3 Invariant $I_m^{(2)}$ for the M@C₆₀ Crystal Fragment

For this work we take the P and H crystal fragments to be invariant under the operations of the S_6 point group. In addition, we have chosen SF cartesian axes such that the C_3 symmetry axis of S_6 points along the (1, 1, 1) direction. Since the internal moments due to the NN cages must be invariant to a $2\pi/3$ rotation about the C_3 axis, then given Eqs. (27)

and (29), the following must be obeyed

$$\mathbf{B}^* I^{(2)} = I^{(2)}, \quad (30)$$

where $I^{(2)}$ is the column vector composed of internal moments produced by the charge density of the twelve NN cages

$$I^{(2)} \equiv \begin{pmatrix} I_{-2}^{(2)} \\ I_{-1}^{(2)} \\ I_0^{(2)} \\ I_{+1}^{(2)} \\ I_{+2}^{(2)} \end{pmatrix}. \quad (31)$$

Equation (30) is satisfied if $I^{(2)}$ is an eigenvector of \mathbf{B}^* having eigenvalue equal to +1. These eigenvectors can be straightforwardly determined. They are given by

$$I^{(2)} = A \begin{pmatrix} i \\ (-1 + i) \\ 0 \\ (1 + i) \\ -i \end{pmatrix}, \quad (32)$$

where, in general, A is a complex constant.

4 Perturbation theory applied to $j = 1$ level splittings

4.1 $\text{H}_2@C_{60}$ and $\text{HF}@C_{60}$

We take the lowest-energy zeroth-order TR states of $\text{H}_2@C_{60}$ and $\text{HF}@C_{60}$ to be of the form $|T_0\rangle|j, m_j\rangle$,⁷ where $|T_0\rangle$ depends only on \mathbf{R} and $|j, m_j\rangle$ is a rigid-rotor rotational eigenfunction. The matrix elements of V_{quad} connecting the states of a given j level are then given by

$$\langle T_0, j, m'_j | V_{\text{quad}} | T_0, j, m_j \rangle = \sum_m (-)^m I_{-m}^{(2)} \langle T_0, j, m'_j | Q_m^{(2)} | T_0, j, m_j \rangle. \quad (33)$$

By using Eq. (15) of the main text

$$\begin{aligned} \langle T_0, j, m'_j | Q_m^{(2)} | T_0, j, m_j \rangle &= Q_0^{\text{BF}} \langle j, m'_j | [D_{m,0}^{(2)}(\omega)]^* | j, m_j \rangle \\ &+ (-)^m \sqrt{40\pi\mu_z} \sum_{m'} \begin{pmatrix} 1 & 1 & 2 \\ m' & m - m' & -m \end{pmatrix} \\ &\times \langle T_0 | RY_{1,m'}(\Theta, \Phi) | T_0 \rangle \langle j, m'_j | [D_{m-m',0}^{(1)}(\omega)]^* | j, m_j \rangle. \end{aligned} \quad (34)$$

Now the $|T_0, j, m_j\rangle$ have inversion symmetry (due to the I_h environment imposed by the central C_{60} cage), as do the $|j, m_j\rangle$. In consequence, $|T_0\rangle$ also has inversion symmetry. The upshot is that the factors $\langle T_0 | RY_{1,m'}(\Theta, \Phi) | T_0 \rangle$ appearing in Eq. (34) are zero by symmetry, since $RY_{1,m'}(\Theta, \Phi)$ changes sign upon inversion. Thus we need only consider the first term on the rhs of Eq. (34). One finds

$$\langle T_0, j, m'_j | Q_m^{(2)} | T_0, j, m_j \rangle = (-)^{m'_j} (2j + 1) Q_0^{\text{BF}} \begin{pmatrix} j & j & 2 \\ 0 & 0 & 0 \end{pmatrix} \begin{pmatrix} j & j & 2 \\ -m'_j & m_j & m \end{pmatrix}. \quad (35)$$

Substituting Eq. (35) into Eq. (33) one obtains

$$\begin{aligned} \langle T_0, j, m'_j | V_{\text{quad}} | T_0, j, m_j \rangle &= (-)^{m_j} I_{m_j - m'_j}^{(2)} \begin{pmatrix} j & j & 2 \\ -m'_j & m_j & m'_j - m_j \end{pmatrix} \\ &\times (2j + 1) Q_0^{\text{BF}} \begin{pmatrix} j & j & 2 \\ 0 & 0 & 0 \end{pmatrix}. \end{aligned} \quad (36)$$

These matrix elements are readily evaluated for a given value of j . For $j = 1$ the full matrix (rows labeled by $m'_j = -1, 0, 1$ and columns by $m_j = -1, 0, 1$) is given by

$$\langle T_0, 1, \{m'_j\} | V_{\text{quad}} | T_0, 1, \{m_j\} \rangle = \frac{\sqrt{6}}{5} Q_0^{\text{BF}} A \begin{pmatrix} 0 & -\frac{(1+i)}{\sqrt{2}} & i \\ -\frac{(1-i)}{\sqrt{2}} & 0 & \frac{(1+i)}{\sqrt{2}} \\ -i & \frac{(1-i)}{\sqrt{2}} & 0 \end{pmatrix}, \quad (37)$$

where we have used Eq. (32) for the $I_m^{(2)}$. This matrix has eigenvalues $\frac{\sqrt{6}}{5} Q_0^{\text{BF}} A$, $\frac{\sqrt{6}}{5} Q_0^{\text{BF}} A$, and $-2\frac{\sqrt{6}}{5} Q_0^{\text{BF}} A$. These are the first-order corrections to the energies of the $j = 1$ states and give

$$\Delta_{\text{PT}} \equiv E(g = 2) - E(g = 1) = 3A \frac{\sqrt{6}}{5} Q_0^{\text{BF}}, \quad (38)$$

consistent with Eqs. (17) and (18) of the main text.

4.2 H₂O@C₆₀

For H₂O@C₆₀ the lowest-energy zeroth-order states⁸ are very well-approximated by $|T_0\rangle |j_{k_a k_c}, m_j\rangle$, where $|T_0\rangle$ depends only on \mathbf{R} ,

$$|j_{k_a k_c}, m_j\rangle = \sum_k a(j_{k_a k_c}, k) |j, m_j, k\rangle \quad (39)$$

is an eigenfunction of the rigid-H₂O rotational Hamiltonian, and the $|j, m_j, k\rangle$ are symmetric-top rotational eigenfunctions

$$|j, m_j, k\rangle = \sqrt{\frac{2j+1}{8\pi^2}} [D_{m_j, k}^{(j)}(\omega)]^*. \quad (40)$$

Matrix elements of V_{quad} connecting states of a given $|T_0, j_{k_a k_c}\rangle$ level are given by

$$\langle T_0, j_{k_a k_c}, m'_j | V_{\text{quad}} | T_0, j_{k_a k_c}, m_j \rangle = \sum_m (-)^m I_{-m}^{(2)} \langle T_0, j_{k_a k_c}, m'_j | Q_m^{(2)} | T_0, j_{k_a k_c}, m_j \rangle. \quad (41)$$

To evaluate the matrix elements on the rhs of Eq. (41) we use Eq. (15) of the main text and note that, as for H₂ and HF, $|T_0\rangle$ has definite parity. Thus,

$$\langle T_0 | RY_{1, m'}(\Theta, \Phi) | T_0 \rangle = 0 \quad (42)$$

and

$$\langle T_0, j_{k_a k_c}, m'_j | Q_m^{(2)} | T_0, j_{k_a k_c}, m_j \rangle = \sum_{q=-2}^2 Q_q^{\text{BF}} \langle j_{k_a k_c}, m'_j | [D_{m, q}^{(2)}]^* | j_{k_a k_c}, m_j \rangle. \quad (43)$$

By using Eqs. (39) and (40)

$$\begin{aligned} \langle j_{k_a k_c}, m'_j | [D_{m, q}^{(2)}]^* | j_{k_a k_c}, m_j \rangle &= \sum_{k, k'} a(j_{k_a k_c}, k') a(j_{k_a k_c}, k) \langle j, m'_j, k' | [D_{m, q}^{(2)}]^* | j, m_j, k \rangle \\ &= (-)^{m'_j} (2j+1) \begin{pmatrix} j & j & 2 \\ -m'_j & m_j & m \end{pmatrix} \\ &\times \sum_{k, k'} (-)^{k'} a(j_{k_a k_c}, k') a(j_{k_a k_c}, k) \begin{pmatrix} j & j & 2 \\ -k' & k & q \end{pmatrix}. \end{aligned} \quad (44)$$

Substituting Eq. (44) into Eq. (43) and then the latter into Eq. (41) one obtains

$$\begin{aligned} \langle T_0, j_{k_a k_c}, m'_j | V_{\text{quad}} | T_0, j_{k_a k_c}, m_j \rangle &= (-)^{m_j} I_{m_j - m'_j}^{(2)} \begin{pmatrix} j & j & 2 \\ -m'_j & m_j & m'_j - m_j \end{pmatrix} \\ &\times (2j + 1) \sum_q Q_q^{\text{BF}} \sum_{k', k} (-)^{k'} a(j_{k_a k_c}, k') a(j_{k_a k_c}, k) \begin{pmatrix} j & j & 2 \\ -k' & k & q \end{pmatrix}. \end{aligned} \quad (45)$$

For $j = 1$ the Eq.-(45) matrix (rows labeled by $m'_j = -1, 0, 1$ and columns by $m_j = -1, 0, 1$) is given by

$$\langle T_0, 1_{k_a k_c}, \{m'_j\} | V_{\text{quad}} | T_0, 1_{k_a k_c}, \{m_j\} \rangle = Af(Q^{\text{BF}}) \begin{pmatrix} 0 & -\frac{(1+i)}{\sqrt{2}} & i \\ -\frac{(1-i)}{\sqrt{2}} & 0 & \frac{(1+i)}{\sqrt{2}} \\ -i & \frac{(1-i)}{\sqrt{2}} & 0 \end{pmatrix}, \quad (46)$$

where we have used Eq. (32) for the $I_m^{(2)}$ and

$$f(Q^{\text{BF}}) \equiv \frac{3}{\sqrt{5}} \left[\sum_q Q_q^{\text{BF}} \sum_{k', k} (-)^{k'} a(j_{k_a k_c}, k') a(j_{k_a k_c}, k) \begin{pmatrix} 1 & 1 & 2 \\ -k' & k & q \end{pmatrix} \right]. \quad (47)$$

Diagonalization of Eq. (46) yields the eigenvalues $Af(Q^{\text{BF}})$, $Af(Q^{\text{BF}})$, and $-2Af(Q^{\text{BF}})$ and the level splitting

$$\Delta_{\text{PT}} = E(g = 2) - E(g = 1) = 3Af(Q^{\text{BF}}). \quad (48)$$

For the 1_{01} level, the *ortho* ground state,

$$a(1_{01}, 1) = -a(1_{01}, -1) = \frac{1}{\sqrt{2}} \quad a(1_{01}, 0) = 0 \quad (49)$$

and

$$f(Q^{\text{BF}}, 1_{01}) = \frac{3}{5} \left[-\frac{1}{\sqrt{6}} Q_0^{\text{BF}} + \frac{1}{2} (Q_2^{\text{BF}} + Q_{-2}^{\text{BF}}) \right]. \quad (50)$$

For the first excited rotational state of the *ortho* species, 1_{10} ,

$$a(1_{01}, 1) = a(1_{01}, -1) = \frac{1}{\sqrt{2}} \quad a(1_{01}, 0) = 0 \quad (51)$$

and

$$f(Q^{\text{BF}}, 1_{10}) = \frac{3}{5} \left[+\frac{1}{\sqrt{6}} Q_0^{\text{BF}} + \frac{1}{2} (Q_2^{\text{BF}} + Q_{-2}^{\text{BF}}) \right]. \quad (52)$$

Finally, for the first excited rotational state of the *para* species, 1_{11} ,

$$a(1_{11}, 1) = a(1_{11}, -1) = 0 \quad a(1_{11}, 0) = 1 \quad (53)$$

and

$$f(Q^{\text{BF}}, 1_{11}) = \frac{\sqrt{6}}{5} Q_0^{\text{BF}}. \quad (54)$$

References

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- (5) M. Xu, S. Ye, A. Powers, R. Lawler, N. J. Turro, and Z. Bačić, J. Chem. Phys. **139**, 064309 (2013).
- (6) For example, For example, R. N. Zare, *Angular Momentum* (Wiley, New York, 1988), Eq. (7), p. 246.
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Table 1: H₂ BF site coordinates (in bohrs), site masses (in amu), rotational constant (in cm⁻¹), and BF quadrupole (in au).

Site #	x	y	z	mass
1	0.000000	0.000000	0.000000	0.0000
2	0.000000	0.000000	+0.699199	1.0078
3	0.000000	0.000000	-0.699199	1.0078

$(2I)^{-1} = 58.378$

$Q_0^{\text{BF}} = 0.499$

Table 2: H₂O BF site coordinates (in bohrs), site masses (in amu), rotational constants (in cm⁻¹), and BF quadrupole and dipole components (in au).

Site #	x	y	z	mass
1	0.000000	0.000000	0.125534	15.9949
2	1.453650	0.000000	-0.996156	1.0078
3	-1.453650	0.000000	-0.996156	1.0078
$(2I_x)^{-1}$	$(2I_y)^{-1}$	$(2I_z)^{-1}$		
27.877	9.285	14.512		
$Q_0^{(\text{BF})}$	$Q_{\pm 2}^{(\text{BF})}$	$\vec{\mu} = \mu \hat{z}$		
-0.09973	1.53843	-0.737196		

Table 3: Carbon nuclear coordinates (in bohrs) for the “master cage” C_{60} geometry. Coordinates are referenced to a cage-fixed cartesian axis system having its origin at the center of the cage, its z axis along one of the C_5 symmetry axes of the cage, and its x axis along one of the C_2 symmetry axes of the cage.

C nucleus	x	y	z
1	0.000000	2.322672	6.238707
2	-2.208993	0.717744	6.238707
3	-1.365233	-1.879081	6.238707
4	1.365233	-1.879081	6.238707
5	2.208993	0.717744	6.238707
6	4.319071	1.403350	4.867496
7	5.684303	-0.475731	3.432005
8	4.878326	-2.956276	3.432005
9	2.669332	-3.674020	4.867496
10	1.304100	-5.553102	3.432005
11	-1.304100	-5.553102	3.432005
12	-2.669332	-3.674020	4.867496
13	-4.878326	-2.956276	3.432005
14	-5.684303	-0.475731	3.432005
15	-4.319071	1.403350	4.867496
16	-4.319071	3.726024	3.432005
17	-5.684303	3.282433	1.109333
18	-6.528064	0.685606	1.109333
19	-6.528064	-0.685606	-1.109333
20	-5.684303	-3.282433	-1.109333
21	-4.878326	-4.391767	1.109333
22	-2.669332	-5.996694	1.109333
23	-1.365233	-6.420422	-1.109333

24	1.365233	-6.420422	-1.109333
25	2.669332	-5.996694	1.109333
26	4.878326	-4.391767	1.109333
27	5.684303	-3.282433	-1.109333
28	6.528064	-0.685606	-1.109333
29	6.528064	0.685606	1.109333
30	5.684303	3.282433	1.109333
31	4.878326	4.391767	-1.109333
32	4.878326	2.956276	-3.432005
33	5.684303	0.475731	-3.432005
34	4.319071	-1.403350	-4.867496
35	4.319071	-3.726024	-3.432005
36	2.208993	-5.259085	-3.432005
37	0.000000	-4.541340	-4.867496
38	-2.208993	-5.259085	-3.432005
39	-4.319071	-3.726024	-3.432005
40	-4.319071	-1.403350	-4.867496
41	-5.684303	0.475731	-3.432005
42	-4.878326	2.956276	-3.432005
43	-4.878326	4.391767	-1.109333
44	-2.669332	5.996694	-1.109333
45	-1.304100	5.553102	-3.432005
46	-2.669332	3.674020	-4.867496
47	-1.365233	1.879081	-6.238707
48	-2.208993	-0.717744	-6.238707
49	0.000000	-2.322672	-6.238707
50	2.208993	-0.717744	-6.238707

51	1.365233	1.879081	-6.238707
52	2.669332	3.674020	-4.867496
53	1.304100	5.553102	-3.432005
54	2.669332	5.996694	-1.109333
55	1.365233	6.420422	1.109333
56	-1.365233	6.420422	1.109333
57	-2.208993	5.259085	3.432005
58	0.000000	4.541340	4.867496
59	2.208993	5.259085	3.432005
60	4.319071	3.726024	3.432005

Table 4: Cage center translation vector, \mathbf{T} (in bohrs) and rotation matrix, \hat{R} , defining the position of each of the cages in the 13-cage fragment corresponding to the P orientation of $\text{M@C}_{60}(s)$.

Cage # (k)	$\mathbf{T}(k)$	$\hat{R}(k)$
1	(13.265878, 0.000000, 13.265878)	$\begin{pmatrix} 0.556377 & -0.457993 & -0.693316 \\ -0.566903 & 0.400811 & -0.719702 \\ 0.607508 & 0.793469 & -0.036636 \end{pmatrix}$
2	(0.000000, 13.265878, 13.265878)	$\begin{pmatrix} 0.556377 & -0.457993 & -0.693316 \\ 0.566903 & -0.400811 & 0.719702 \\ -0.607508 & -0.793469 & 0.036636 \end{pmatrix}$
3	(13.265878, 13.265878, 0.000000)	$\begin{pmatrix} -0.556377 & 0.457993 & 0.693316 \\ -0.566903 & 0.400811 & -0.719702 \\ -0.607508 & -0.793469 & 0.036636 \end{pmatrix}$
4	(-13.265878, 0.000000, -13.265878)	$\begin{pmatrix} 0.556377 & -0.457993 & -0.693316 \\ -0.566903 & 0.400811 & -0.719702 \\ 0.607508 & 0.793469 & -0.036636 \end{pmatrix}$
5	(0.000000, -13.265878, -13.265878)	$\begin{pmatrix} 0.556377 & -0.457993 & -0.693316 \\ 0.566903 & -0.400811 & 0.719702 \\ -0.607508 & -0.793469 & 0.036636 \end{pmatrix}$

$$\begin{array}{r}
6 \\
7 \\
8 \\
9 \\
10 \\
11 \\
12
\end{array}
\begin{array}{l}
(-13.265878, -13.265878, 0.000000) \\
(0.000000, 13.265878, -13.265878) \\
(13.265878, 0.000000, -13.265878) \\
(0.000000, -13.265878, 13.265878) \\
(13.265878, -13.265878, 0.000000) \\
(-13.265878, 0.000000, 13.265878) \\
(-13.265878, 13.265878, 0.000000)
\end{array}
\begin{array}{l}
\begin{pmatrix} -0.556377 & 0.457993 & 0.693316 \\ -0.566903 & 0.400811 & -0.719702 \\ -0.607508 & -0.793469 & 0.036636 \end{pmatrix} \\
\begin{pmatrix} 0.556377 & -0.457993 & -0.693316 \\ 0.566903 & -0.400811 & 0.719702 \\ -0.607508 & -0.793469 & 0.036636 \end{pmatrix} \\
\begin{pmatrix} 0.556377 & -0.457993 & -0.693316 \\ -0.566903 & 0.400811 & -0.719702 \\ 0.607508 & 0.793469 & -0.036636 \end{pmatrix} \\
\begin{pmatrix} 0.556377 & -0.457993 & -0.693316 \\ 0.566903 & -0.400811 & 0.719702 \\ -0.607508 & -0.793469 & 0.036636 \end{pmatrix} \\
\begin{pmatrix} -0.556377 & 0.457993 & 0.693316 \\ -0.566903 & 0.400811 & -0.719702 \\ -0.607508 & -0.793469 & 0.036636 \end{pmatrix} \\
\begin{pmatrix} 0.556377 & -0.457993 & -0.693316 \\ -0.566903 & 0.400811 & -0.719702 \\ 0.607508 & 0.793469 & -0.036636 \end{pmatrix} \\
\begin{pmatrix} -0.556377 & 0.457993 & 0.693316 \\ -0.566903 & 0.400811 & -0.719702 \\ -0.607508 & -0.793469 & 0.036636 \end{pmatrix}
\end{array}$$

$$13 \quad (0.000000, 0.000000, 0.000000) \quad \begin{pmatrix} -0.556377 & 0.457993 & 0.693316 \\ 0.566903 & -0.400811 & 0.719702 \\ 0.607508 & 0.793469 & -0.036636 \end{pmatrix}$$

Table 5: Cage center translation vector, \mathbf{T} (in bohrs) and rotation matrix, \hat{R} , defining the position of each of the cages in the 13-cage fragment corresponding to the H orientation of $\text{M@C}_{60}(s)$.

Cage # (k)	$\mathbf{T}(k)$	$\hat{R}(k)$
1	(13.265878, 0.000000, 13.265878)	$\begin{pmatrix} 0.154881 & -0.967912 & -0.197886 \\ 0.195485 & 0.226368 & -0.954224 \\ 0.968400 & 0.109107 & 0.224272 \end{pmatrix}$
2	(0.000000, 13.265878, 13.265878)	$\begin{pmatrix} 0.154881 & -0.967912 & -0.197886 \\ -0.195485 & -0.226368 & 0.954224 \\ -0.968400 & -0.109107 & -0.224272 \end{pmatrix}$
3	(13.265878, 13.265878, 0.000000)	$\begin{pmatrix} -0.154881 & 0.967912 & 0.197886 \\ 0.195485 & 0.226368 & -0.954224 \\ -0.968400 & -0.109107 & -0.224272 \end{pmatrix}$
4	(-13.265878, 0.000000, -13.265878)	$\begin{pmatrix} 0.154881 & -0.967912 & -0.197886 \\ 0.195485 & 0.226368 & -0.954224 \\ 0.968400 & 0.109107 & 0.224272 \end{pmatrix}$
5	(0.000000, -13.265878, -13.265878)	$\begin{pmatrix} 0.154881 & -0.967912 & -0.197886 \\ -0.195485 & -0.226368 & 0.954224 \\ -0.968400 & -0.109107 & -0.224272 \end{pmatrix}$

$$\begin{array}{r}
6 \\
7 \\
8 \\
9 \\
10 \\
11 \\
12
\end{array}
\begin{array}{l}
(-13.265878, -13.265878, 0.000000) \\
(0.000000, 13.265878, -13.265878) \\
(13.265878, 0.000000, -13.265878) \\
(0.000000, -13.265878, 13.265878) \\
(13.265878, -13.265878, 0.000000) \\
(-13.265878, 0.000000, 13.265878) \\
(-13.265878, 13.265878, 0.000000)
\end{array}
\begin{array}{l}
\begin{pmatrix} -0.154881 & 0.967912 & 0.197886 \\ 0.195485 & 0.226368 & -0.954224 \\ -0.968400 & -0.109107 & -0.224272 \end{pmatrix} \\
\begin{pmatrix} 0.154881 & -0.967912 & -0.197886 \\ -0.195485 & -0.226368 & 0.954224 \\ -0.968400 & -0.109107 & -0.224272 \end{pmatrix} \\
\begin{pmatrix} 0.154881 & -0.967912 & -0.197886 \\ 0.195485 & 0.226368 & -0.954224 \\ 0.968400 & 0.109107 & 0.224272 \end{pmatrix} \\
\begin{pmatrix} 0.154881 & -0.967912 & -0.197886 \\ -0.195485 & -0.226368 & 0.954224 \\ -0.968400 & -0.109107 & -0.224272 \end{pmatrix} \\
\begin{pmatrix} -0.154881 & 0.967912 & 0.197886 \\ 0.195485 & 0.226368 & -0.954224 \\ -0.968400 & -0.109107 & -0.224272 \end{pmatrix} \\
\begin{pmatrix} 0.154881 & -0.967912 & -0.197886 \\ 0.195485 & 0.226368 & -0.954224 \\ 0.968400 & 0.109107 & 0.224272 \end{pmatrix} \\
\begin{pmatrix} -0.154881 & 0.967912 & 0.197886 \\ 0.195485 & 0.226368 & -0.954224 \\ -0.968400 & -0.109107 & -0.224272 \end{pmatrix}
\end{array}$$

$$13 \quad (0.000000, 0.000000, 0.000000) \quad \begin{pmatrix} -0.154881 & 0.967912 & 0.197886 \\ -0.195485 & -0.226368 & 0.954224 \\ 0.968400 & 0.109107 & 0.224272 \end{pmatrix}$$
