

Supplementary Information: Correlating geminal $^2J_{\text{Si-O-Si}}$ couplings to structure in framework silicates.

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S1. GAUSSIAN INTEGRATION GRID SIZE

The effect of change in $^2J_{\text{Si-O-Si}}$ coupling evaluation with the size of the integration grid was tested to avoid integration errors. A series of calculations were run with (1) ‘fine’, pruned (75, 302) and (2) ‘ultrafine’, pruned (99, 590) integration grids. As seen in Fig. S1, no difference in the $^2J_{\text{Si-O-Si}}$ coupling was observed with the increase in the integration grid size. Thus, all remaining calculations were run with ‘fine’ integration grid.

S2. CONTRIBUTIONS TO THE NET J COUPLING

The net J -coupling includes contributions from Fermi contact (FC), Spin-dipolar (SD), paramagnetic spin-orbit (PSO) and diamagnetic spin-orbit (DSO).

$$J = J_{\text{FC}} + J_{\text{SD}} + J_{\text{PSO}} + J_{\text{DSO}}$$

For $^2J_{\text{Si-O-Si}}$ couplings—calculated using Gaussian 09¹ with high level of theory—across a Si-O-Si linkage, the net J -coupling is dominated by the Fermi contact term. As shown in Fig. S2, the combined contribution from SD, PSO, DSO

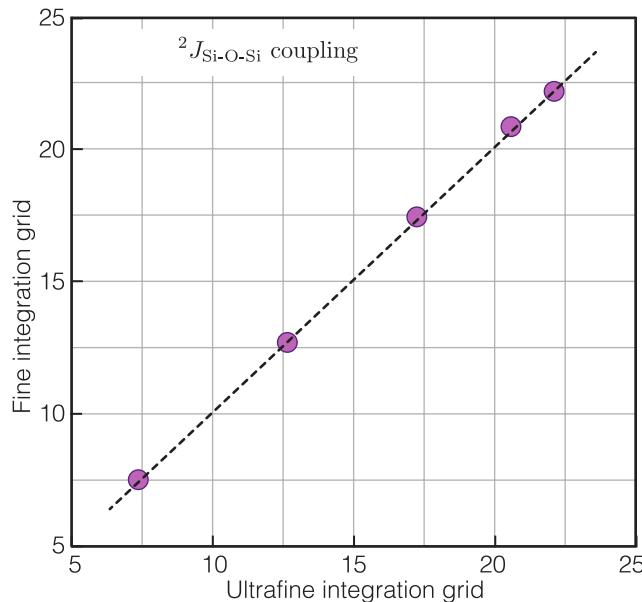


FIG. S1. A perfect correlation of $^2J_{\text{Si-O-Si}}$ coupling evaluated from ‘fine’ and ‘ultrafine’ integration grid.

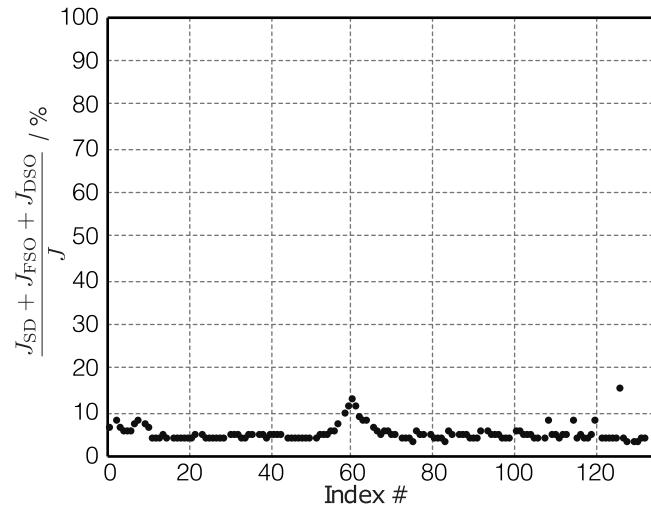


FIG. S2. Combined contribution from SD, PSO and DSO terms accounts to less than 10% of the net J -coupling. The horizontal axis—labeled as index—refer to the index number in Table S1-S3.

terms account to less than 10% of the contribution from net J -coupling. The combined contribution increases slightly around indexes 1 to 10, indexes 52-67 and indexes 108, 114, 120 and 126, and is associated with clusters with lower Si-O-Si bond angles, Ω_0 in the range of 120° to 130° .

S3. S-CHARACTER MODEL

A. s-character at the Si HTO along Si-O bond

In cluster calculations with all the Si-O bond distances fixed at $d_{\text{Si-O}} = 1.6 \text{ \AA}$ and with all intra-tetrahedral-angles fixed at $\angle \text{O-Si-O} = 109.5^\circ$, we found that the a_{Si}^2 of a given Si-O bond depends not only on the Si-O-Si bond angle of its linkage, but also on the other three Si-O-Si bond angles around the silicon. As explained in the main text this arises because the sum of a_{Si}^2 from all four Si-O bonds about the Si tetrahedron must remain constant. A strong correlation between a_{Si}^2 of a given Si-O bond and the four surrounding Si-O-Si bond angles was found to be

$$a_{\text{Si}}^2 \approx c_{\text{Si}} + m_{\text{Si}} (\cos \Omega_0 - \cos \langle \Omega \rangle), \quad (1)$$

where $m_{\text{Si}} = 0.0279$, $c_{\text{Si}} = 0.2465$ with $R^2 = 0.96894$. The *ab-initio*-derived data supporting this correlation are

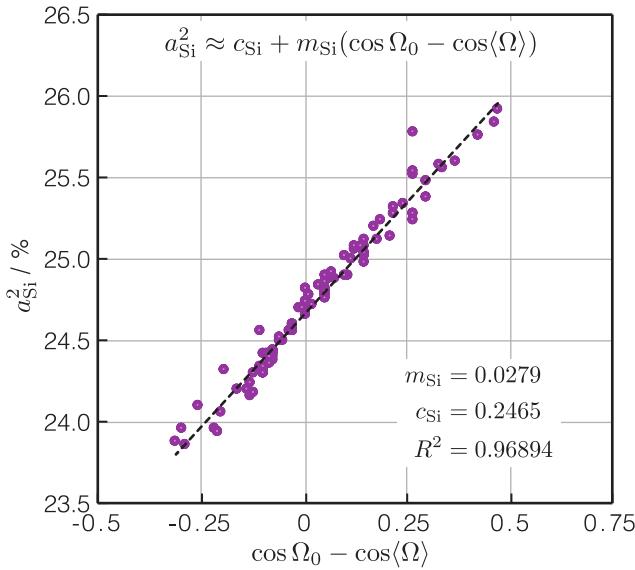


FIG. S3. Variation in the s-character at Si HTO along the Si-O bond as the function of the Si-O-Si tetrahedral angle Ω_0 and average Si-O-Si bond angle, $\langle\Omega\rangle$.

shown in Fig. S3. From Eq. (1), it follows that when all four Si-O-Si bond angles about the Si tetrahedron are equal, the s-character along all four Si-O bonds are also equal.

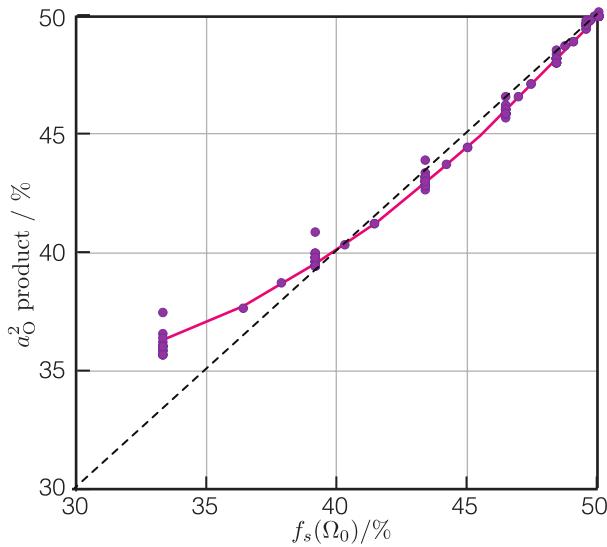


FIG. S4. Comparison of the s-character at bridging oxygen HTO along the Si-O bond against the popular^{2,3} approximation $f_s(\Omega_0)$.

B. s-character at the bridging O HTO along Si-O bond

The popular^{2,3} approximation of the s-character at the bridging oxygen along the Si-O bond follows,

$$f_s(\Omega_0) = \frac{\cos \Omega_0}{\cos \Omega_0 - 1}. \quad (2)$$

Although the approximation in Eq. (2) gives a good agreement with respect to *ab-initio* calculated s-character, a_O^2 , at higher Ω_0 , we show in Fig. S4 that this agreement appears to break at lower Ω_0 .

S4. ²⁹SI ISOTROPIC CHEMICAL SHIFT

In 1983, Smith and Blackwell⁴ first showed a correlation between the ²⁹Si isotropic chemical shift, δ_{CS} , and the average secant of the four Si-O-Si bond angles, Ω , about a Si tetrahedron given by

$$\delta_{CS} = a'_\delta \langle \sec \Omega \rangle + b'_\delta. \quad (3)$$

Later, the same year, Thomas *et. al.*⁵ showed that ²⁹Si isotropic chemical shift correlate linearly with $\langle\Omega\rangle$, according to

$$\delta_{CS} = a_\delta \langle\Omega\rangle + b_\delta. \quad (4)$$

The two models, stating different apparent correlations, both showed a good agreement with experiment. In 1984, Engelhardt and Radeglia³, with the assumption that the chemical shift is dominated by paramagnetic contribution, described ²⁹Si isotropic chemical shift using a simple quantum mechanical model to follow

$$\delta_{CS} = A_\delta \sum_{n=1}^4 f_O(\Omega_n) + B_\delta. \quad (5)$$

The authors showed that the reason Eqs. (3)-(5) all show a good agreement with experiment is that the weak curvature of both $f_O(\Omega)$ and $\sec \Omega$ in the relevant range of about 140°-160° cause the ²⁹Si isotropic chemical shift to remain mostly linear with respect to the average Si-O-Si bond angle, $\langle\Omega\rangle$. Many other models⁶ have since been proposed, however, by far the simplest correlation is given by Thomas *et. al.*⁵, which can be derived by performing a Taylor series expansion of Eq. (5) about 150° with coefficients

$$a_\delta = 1.0025 \times 10^{-2} A_\delta \text{ and } b_\delta = 0.3527 A_\delta + B_\delta.$$

The coefficient $A_\delta = -61.7625 \text{ ppm}/^\circ$ and $B_\delta = 2.19 \text{ ppm}$ from Engelhardt and Radeglia³ yields $a_\delta = -0.6191 \text{ ppm}/^\circ$ and $b_\delta = -19.593 \text{ ppm}$ which is within 1.5% of the linear fit reported in the main document.

S5. J-COUPLING AS A FUNCTION OF Ω_0

Cadars *et. al.*⁷ discussed the scattering of ²J_{Si-O-Si} coupling as a function of the central linkage angle Ω_0 resulting from the local structural variations about the central

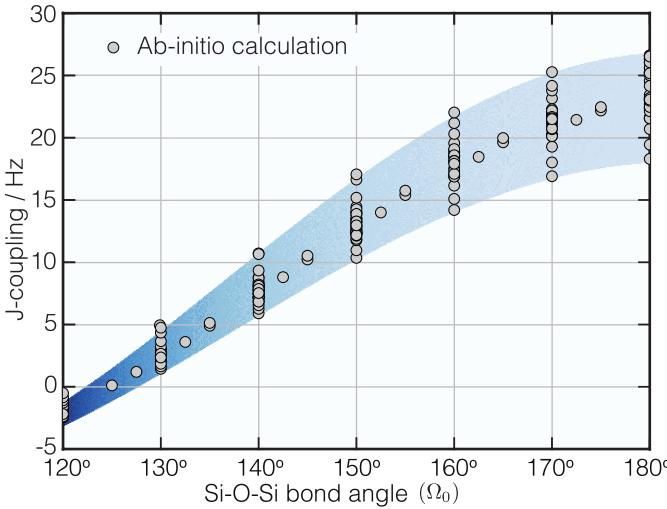


FIG. S5. Scattering of 2J -coupling as a function of central Si-O-Si linkage angle Ω_0 arising from the variation in local structure around the central Si-O-Si linkage, specially the double average $\langle \Omega \rangle$. The gray dots are the *ab-initio* calculated 2J -couplings—and the background image is the intensity plot of 2J -coupling assuming a uniform distribution of $\langle \Omega \rangle$.

Si-O-Si linkage. In Fig. S5 we show the extent of this scattering as a function of Ω_0 . The gray dots are the *ab-initio* calculated J -couplings—presented in Table S1–S4—and the image in the background is calculated using Eq. (19) from the main document—assuming a uniform distribution of $\langle \Omega \rangle$. A significant scatter of J -coupling is observed when only considering the center linkage angle Ω_0 —specially at higher Ω_0 .

S6. J-COUPING MODEL APPROXIMATION

In the main text, we described an analytical expression for calculating the Si-O-Si bond angle

$$\Omega_0(x) = \frac{180^\circ}{\pi} \cos^{-1} \left[-\frac{1}{3}x + \{S(x) + T(x)\} \right], \quad (6)$$

where

$$\begin{aligned} S(x) &= \sqrt[3]{R(x) + \sqrt{D(x)}}, \\ T(x) &= \sqrt[3]{R(x) - \sqrt{D(x)}}, \\ D(x) &= \frac{1}{108}x^2(4x + 27), \\ R(x) &= -\frac{1}{54}x(2x^2 + 18x + 27) \text{ and} \\ x &= \frac{J - J_0}{m_1 \langle \Omega \rangle}. \end{aligned}$$

Due to the overly complicated parameterization of Eq. (6), we approximated Eq. (6) by

$$g(x) = a_j + b_j x + c_j \exp\{d_j x\} \quad (8)$$

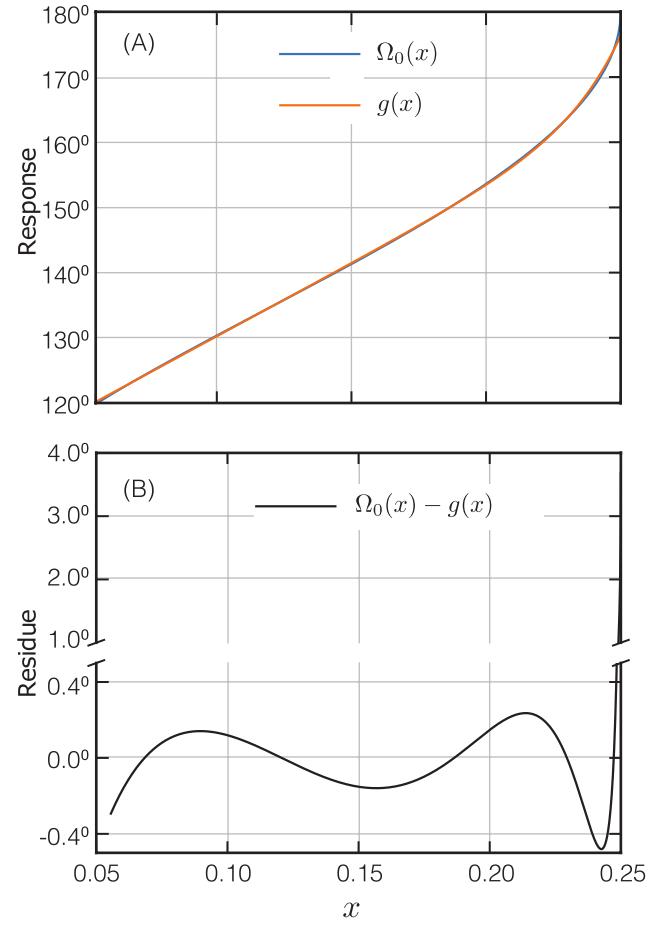


FIG. S6. (A) Comparison of $\Omega_0(x)$ and $g(x)$ as a function of $x \in [1/18, 1/4]$. A good agreement between $g(x)$ and $\Omega_0(x)$ is observed within the range corresponding to $\Omega_0 \in [120^\circ, 176^\circ]$ shown in (B).

where the coefficients $a_j = 107.88^\circ$, $b_j = 223.49^\circ$, $c_j = 0.00002487^\circ$ and $d_j = 53.01$ were determined from the least square minimization. In Fig. S6, we show the comparison between $\Omega_0(x)$ and $g(x)$. A good agreement is observed for the range of x corresponding to $\Omega_0(x) \in [120^\circ, 176^\circ]$ to within $\pm 0.5^\circ$. The deviation at 176° and onwards is significant to a maximum of 3.7° at $\Omega_0(x) = 180^\circ$. However, due to the low probability of Si-O-Si bond angles in this range [$176^\circ, 180^\circ$], this deviation has been neglected in our study.

¹M. J. Frisch, G. W. Trucks, H. B. Schlegel, G. E. Scuseria, M. A. Robb, J. R. Cheeseman, G. Scalmani, V. Barone, B. Mennucci, G. A. Petersson, H. Nakatsuji, M. Caricato, X. Li, H. P. Hratchian, A. F. Izmaylov, J. Bloino, G. Zheng, J. L. Sonnenberg, M. Hada, M. Ehara, K. Toyota, R. Fukuda, J. Hasegawa, M. Ishida, T. Nakajima, Y. Honda, O. Kitao, H. Nakai, T. Vreven, J. A. M. Jr., J. E. Peralta, F. Ogliaro, M. J. Bearpark, J. J. Heyd, E. N. Brothers, K. N. Kudin, V. N. Staroverov, T. A. Keith, R. Kobayashi, J. Normand, K. Raghavachari, A. P. Rendell, J. C. Burant, S. S. Iyengar, J. Tomasi, M. Cossi, N. Rega, J. M. Millam, M. Klene, J. E. Knox, J. B. Cross, V. Bakken, C. Adamo, J. Jaramillo, R. Gomperts, R. E. Stratmann, O. Yazyev, A. J. Austin, R. Cammi, C. Pomelli, J. W. Ochterski, R. L. Martin, K. Morokuma, V. G. Zakrzewski, G. A. Voth, P. Salvador, J. J. Dannenberg, S. Dapprich, A. D. Daniels,

- O. Farkas, J. B. Foresman, J. V. Ortiz, J. Cioslowski, D. J. Fox, Gaussian 09 Revision D.01 (2013).
- ²M. Klessinger, M. Barfield, The structural dependence of geminal ^{13}C - ^{13}C coupling constants, Ellis Horwood, Chichester, 1987, Ch. 16, pp. 269–284.
- ³G. Engelhardt, R. Radeglia, A semi-empirical quantum-chemical rationalization of the correlation between SiOSi angles and ^{29}Si NMR chemical shifts of silica polymorphs and framework aluminosilicates (zeolites), Chemical Physics Letters 108 (1984) 271 – 274. doi:10.1016/0009-2614(84)87063-3.
- ⁴J. V. Smith, C. S. Blackwell, Nuclear magnetic resonance of silica polymorphs, Nature 303 (1983) 223 – 225. doi:10.1038/303223a0.
- ⁵J. Thomas, J. Klinowski, S. Ramdas, B. Hunter, D. Tennakoon, The evaluation of non-equivalent tetrahedral sites from ^{29}Si NMR chemical shifts in zeolites and related aluminosilicates, Chemical Physics Letters 102 (1983) 158 – 162. doi:10.1016/0009-2614(83)87384-9.
- ⁶F. Mauri, A. Pasquarello, B. G. Pfrommer, Y.-G. Yoon, S. G. Louie, Si-O-Si bond-angle distribution in vitreous silica from first-principles ^{29}Si NMR analysis, Phys. Rev. B 62 (8) (2000) 4786–4789.
- ⁷S. Cadars, D. H. Brouwer, B. F. Chmelka, Probing local structures of siliceous zeolite frameworks by solid-state NMR and first-principles calculations of ^{29}Si -O- ^{29}Si scalar couplings, Phys. Chem. Chem. Phys. 11 (2009) 1825–1837. doi:10.1039/b815361b.

TABLE S1. *ab-initio* calculated vs $^2J_{\text{Si-O-Si}}$ coupling model $J(\Omega_0, \overline{\langle \Omega \rangle}, \phi)$ and $J(\Omega_0, \overline{\langle \Omega \rangle})$, Eq. (17) and (19) respectively of the main document, as a function of local parameters including Ω , $\overline{\langle \Omega \rangle}$ and ϕ . The initial geometry was optimized with RHF/6-311G(d). Individual geometry, after structural constraint on Ω_0 , Ω_k and ϕ , was not optimized. All Si-O bond distances were fixed to 1.6 Å and O-Si-O intra-tetrahedral angle set to 109.5°.

| Index | $\Omega_0/1^\circ$ | $\Omega_k/1^\circ$ | | | | | | $\overline{\langle \Omega \rangle}/1^\circ$ | $\phi/1^\circ$ | $^2J_{\text{Si-O-Si-coupling}} / \text{Hz}$ | | |
|-------|--------------------|--------------------|------------|------------|------------|------------|------------|---|----------------|---|--|--|
| | | Ω_1 | Ω_2 | Ω_3 | Ω_4 | Ω_5 | Ω_6 | | | <i>ab-initio</i> | $J(\Omega_0, \overline{\langle \Omega \rangle}, \phi)$ | $J(\Omega_0, \overline{\langle \Omega \rangle})$ |
| 1 | 120 | 146 | 146 | 146 | 146 | 146 | 146 | 139.5 | -59.837 | -1.8738 | -1.7949 | -2.1819 |
| 2 | 120 | 146 | 146 | 146 | 146 | 146 | 146 | 139.5 | -45.539 | -1.4292 | -1.9006 | -2.1819 |
| 3 | 120 | 146 | 146 | 146 | 146 | 146 | 146 | 139.5 | -20.286 | -1.8025 | -2.3703 | -2.1819 |
| 4 | 120 | 146 | 146 | 146 | 146 | 146 | 146 | 139.5 | 8.237 | -1.9657 | -2.5334 | -2.1819 |
| 5 | 120 | 146 | 146 | 146 | 146 | 146 | 146 | 139.5 | 36.126 | -1.9524 | -2.0598 | -2.1819 |
| 6 | 130 | 146 | 146 | 146 | 146 | 146 | 146 | 142 | -42.783 | 3.0394 | 2.9474 | 2.6332 |
| 7 | 130 | 146 | 146 | 146 | 146 | 146 | 146 | 142 | -18.639 | 2.4312 | 2.3494 | 2.6332 |
| 8 | 130 | 146 | 146 | 146 | 146 | 146 | 146 | 142 | 7.502 | 2.2193 | 2.1653 | 2.6332 |
| 9 | 130 | 146 | 146 | 146 | 146 | 146 | 146 | 142 | 33.269 | 2.4992 | 2.7195 | 2.6332 |
| 10 | 130 | 146 | 146 | 146 | 146 | 146 | 146 | 142 | 56.619 | 2.9022 | 3.1317 | 2.6332 |
| 11 | 140 | 146 | 146 | 146 | 146 | 146 | 146 | 144.5 | -51.305 | 8.7829 | 8.4861 | 7.9345 |
| 12 | 140 | 146 | 146 | 146 | 146 | 146 | 146 | 144.5 | -40.432 | 8.2917 | 8.2535 | 7.9345 |
| 13 | 140 | 146 | 146 | 146 | 146 | 146 | 146 | 144.5 | -17.334 | 7.4491 | 7.5564 | 7.9345 |
| 14 | 140 | 146 | 146 | 146 | 146 | 146 | 146 | 144.5 | 6.935 | 7.2072 | 7.3604 | 7.9345 |
| 15 | 140 | 146 | 146 | 146 | 146 | 146 | 146 | 144.5 | 30.992 | 7.6871 | 7.9664 | 7.9345 |
| 16 | 140 | 146 | 146 | 146 | 146 | 146 | 146 | 144.5 | 53.6 | 8.4367 | 8.5145 | 7.9345 |
| 17 | 150 | 146 | 146 | 146 | 146 | 146 | 146 | 147 | -58.431 | 14.029 | 13.739 | 13.035 |
| 18 | 150 | 146 | 146 | 146 | 146 | 146 | 146 | 147 | -48.184 | 13.966 | 13.611 | 13.035 |
| 19 | 150 | 146 | 146 | 146 | 146 | 146 | 146 | 147 | -38.449 | 13.526 | 13.338 | 13.035 |
| 20 | 150 | 146 | 146 | 146 | 146 | 146 | 146 | 147 | -27.49 | 12.984 | 12.943 | 13.035 |
| 21 | 150 | 146 | 146 | 146 | 146 | 146 | 146 | 147 | -16.296 | 12.57 | 12.571 | 13.035 |
| 22 | 150 | 146 | 146 | 146 | 146 | 146 | 146 | 147 | -4.938 | 12.342 | 12.352 | 13.035 |
| 23 | 150 | 146 | 146 | 146 | 146 | 146 | 146 | 147 | 6.494 | 12.329 | 12.369 | 13.035 |
| 24 | 150 | 146 | 146 | 146 | 146 | 146 | 146 | 147 | 17.896 | 12.527 | 12.617 | 13.035 |
| 25 | 150 | 146 | 146 | 146 | 146 | 146 | 146 | 147 | 29.171 | 12.915 | 13.004 | 13.035 |
| 26 | 150 | 146 | 146 | 146 | 146 | 146 | 146 | 147 | 40.238 | 13.41 | 13.396 | 13.035 |
| 27 | 150 | 146 | 146 | 146 | 146 | 146 | 146 | 147 | 51.045 | 13.836 | 13.665 | 13.035 |
| 28 | 160 | 146 | 146 | 146 | 146 | 146 | 146 | 149.5 | -50.489 | 18.597 | 18.014 | 17.329 |
| 29 | 160 | 146 | 146 | 146 | 146 | 146 | 146 | 149.5 | -36.792 | 18.051 | 17.6 | 17.329 |
| 30 | 160 | 146 | 146 | 146 | 146 | 146 | 146 | 149.5 | -15.472 | 17.092 | 16.792 | 17.329 |
| 31 | 160 | 146 | 146 | 146 | 146 | 146 | 146 | 149.5 | 6.149 | 16.879 | 16.59 | 17.329 |
| 32 | 160 | 146 | 146 | 146 | 146 | 146 | 146 | 149.5 | 27.718 | 17.534 | 17.236 | 17.329 |
| 33 | 160 | 146 | 146 | 146 | 146 | 146 | 146 | 149.5 | 48.901 | 18.467 | 17.981 | 17.329 |
| 34 | 170 | 146 | 146 | 146 | 146 | 146 | 146 | 152 | -52.533 | 21.793 | 21.099 | 20.331 |
| 35 | 170 | 146 | 146 | 146 | 146 | 146 | 146 | 152 | -35.426 | 21.155 | 20.564 | 20.331 |
| 36 | 170 | 146 | 146 | 146 | 146 | 146 | 146 | 152 | -14.824 | 20.27 | 19.739 | 20.331 |
| 37 | 170 | 146 | 146 | 146 | 146 | 146 | 146 | 152 | 5.882 | 20.123 | 19.54 | 20.331 |
| 38 | 170 | 146 | 146 | 146 | 146 | 146 | 146 | 152 | 26.569 | 20.837 | 20.183 | 20.331 |
| 39 | 170 | 146 | 146 | 146 | 146 | 146 | 146 | 152 | 47.124 | 21.707 | 20.98 | 20.331 |
| 40 | 180 | 146 | 146 | 146 | 146 | 146 | 146 | 154.5 | -34.332 | 22.417 | 21.896 | 21.703 |
| 41 | 180 | 146 | 146 | 146 | 146 | 146 | 146 | 154.5 | -14.327 | 21.623 | 21.076 | 21.703 |
| 42 | 180 | 146 | 146 | 146 | 146 | 146 | 146 | 154.5 | 5.679 | 21.555 | 20.883 | 21.703 |
| 43 | 180 | 146 | 146 | 146 | 146 | 146 | 146 | 154.5 | 25.685 | 22.34 | 21.511 | 21.703 |
| 44 | 180 | 146 | 146 | 146 | 146 | 146 | 146 | 154.5 | 45.691 | 23.158 | 22.331 | 21.703 |
| 45 | 180 | 146 | 146 | 146 | 146 | 146 | 146 | 154.5 | 65.694 | 23.177 | 22.522 | 21.703 |
| 46 | 180 | 180 | 180 | 180 | 180 | 180 | 180 | 180 | 15.68 | 25.269 | 25.954 | 26.635 |
| 47 | 180 | 180 | 180 | 180 | 180 | 180 | 180 | 180 | 25.68 | 25.607 | 26.411 | 26.635 |
| 48 | 180 | 180 | 180 | 180 | 180 | 180 | 180 | 180 | 45.69 | 26.321 | 27.366 | 26.635 |
| 49 | 180 | 180 | 180 | 180 | 180 | 180 | 180 | 180 | 65.694 | 26.604 | 27.589 | 26.635 |
| 50 | 180 | 180 | 180 | 180 | 180 | 180 | 180 | 180 | -14.327 | 25.174 | 25.904 | 26.635 |
| 51 | 180 | 180 | 180 | 180 | 180 | 180 | 180 | 180 | -34.332 | 26.061 | 26.859 | 26.635 |

TABLE S2. *ab-initio* calculated vs $^2J_{\text{Si-O-Si}}$ coupling model. The initial geometry was optimized with RHF/6-311G(d). Individual geometry, after structural constraint on Ω_0 , Ω_k and ϕ , was not optimized. All Si-O bond distances were fixed to 1.6 Å and O-Si-O intra-tetrahedral angle set to 109.5°.

| Index | $\Omega_0/1^\circ$ | $\Omega_k/1^\circ$ | | | | | | $\overline{\langle \Omega \rangle}/1^\circ$ | $\phi/1^\circ$ | $^2J_{\text{Si-O-Si-coupling}}/\text{Hz}$ | | |
|-------|--------------------|--------------------|------------|------------|------------|------------|------------|---|----------------|---|--|--|
| | | Ω_1 | Ω_2 | Ω_3 | Ω_4 | Ω_5 | Ω_6 | | | <i>ab-initio</i> | $J(\Omega_0, \overline{\langle \Omega \rangle}, \phi)$ | $J(\Omega_0, \overline{\langle \Omega \rangle})$ |
| 52 | 120 | 120 | 120 | 120 | 120 | 120 | 120 | 120 | 8.237 | -2.4502 | -3.3223 | -3.0199 |
| 53 | 120 | 130 | 130 | 130 | 130 | 130 | 130 | 127.5 | 8.237 | -2.3752 | -3.0189 | -2.6976 |
| 54 | 120 | 140 | 140 | 140 | 140 | 140 | 140 | 135 | 8.237 | -2.1224 | -2.7155 | -2.3753 |
| 55 | 120 | 146 | 146 | 146 | 146 | 146 | 146 | 139.5 | 8.237 | -1.9657 | -2.5334 | -2.1819 |
| 56 | 120 | 150 | 150 | 150 | 150 | 150 | 150 | 142.5 | 8.237 | -1.8819 | -2.412 | -2.0529 |
| 57 | 120 | 160 | 160 | 160 | 160 | 160 | 160 | 150 | 8.237 | -1.6123 | -2.1086 | -1.7306 |
| 58 | 120 | 170 | 170 | 170 | 170 | 170 | 170 | 157.5 | 8.237 | -1.2821 | -1.8052 | -1.4083 |
| 59 | 120 | 180 | 180 | 180 | 180 | 180 | 180 | 165 | 8.237 | -1.083 | -1.5017 | -1.0859 |
| 60 | 130 | 120 | 120 | 120 | 120 | 120 | 120 | 122.5 | 7.5 | 1.4423 | 0.74504 | 1.1487 |
| 61 | 130 | 130 | 130 | 130 | 130 | 130 | 130 | 130 | 7.5 | 1.6351 | 1.2913 | 1.7196 |
| 62 | 130 | 140 | 140 | 140 | 140 | 140 | 140 | 137.5 | 7.5 | 1.9939 | 1.8376 | 2.2906 |
| 63 | 130 | 146 | 146 | 146 | 146 | 146 | 146 | 142 | 7.5 | 2.2193 | 2.1653 | 2.6332 |
| 64 | 130 | 150 | 150 | 150 | 150 | 150 | 150 | 145 | 7.5 | 2.3653 | 2.3838 | 2.8616 |
| 65 | 130 | 160 | 160 | 160 | 160 | 160 | 160 | 152.5 | 7.5 | 2.762 | 2.9301 | 3.4326 |
| 66 | 130 | 170 | 170 | 170 | 170 | 170 | 170 | 160 | 7.5 | 3.2326 | 3.4764 | 4.0035 |
| 67 | 130 | 180 | 180 | 180 | 180 | 180 | 180 | 167.5 | 7.5 | 3.6555 | 4.0226 | 4.5745 |
| 68 | 140 | 120 | 120 | 120 | 120 | 120 | 120 | 125 | 6.935 | 5.8964 | 5.2636 | 5.7602 |
| 69 | 140 | 130 | 130 | 130 | 130 | 130 | 130 | 132.5 | 6.935 | 6.2592 | 6.07 | 6.5965 |
| 70 | 140 | 140 | 140 | 140 | 140 | 140 | 140 | 140 | 6.935 | 6.8246 | 6.8765 | 7.4327 |
| 71 | 140 | 146 | 146 | 146 | 146 | 146 | 146 | 144.5 | 6.935 | 7.2072 | 7.3604 | 7.9345 |
| 72 | 140 | 150 | 150 | 150 | 150 | 150 | 150 | 147.5 | 6.935 | 7.4552 | 7.6829 | 8.269 |
| 73 | 140 | 160 | 160 | 160 | 160 | 160 | 160 | 155 | 6.935 | 8.0411 | 8.4894 | 9.1052 |
| 74 | 140 | 170 | 170 | 170 | 170 | 170 | 170 | 162.5 | 6.935 | 8.722 | 9.2958 | 9.9415 |
| 75 | 140 | 180 | 180 | 180 | 180 | 180 | 180 | 170 | 6.935 | 9.3362 | 10.102 | 10.778 |
| 76 | 150 | 120 | 120 | 120 | 120 | 120 | 120 | 127.5 | 6.494 | 10.354 | 9.6437 | 10.221 |
| 77 | 150 | 130 | 130 | 130 | 130 | 130 | 130 | 135 | 6.494 | 10.962 | 10.692 | 11.304 |
| 78 | 150 | 140 | 140 | 140 | 140 | 140 | 140 | 142.5 | 6.494 | 11.771 | 11.74 | 12.386 |
| 79 | 150 | 146 | 146 | 146 | 146 | 146 | 146 | 147 | 6.494 | 12.329 | 12.369 | 13.035 |
| 80 | 150 | 150 | 150 | 150 | 150 | 150 | 150 | 150 | 6.494 | 12.696 | 12.789 | 13.468 |
| 81 | 150 | 160 | 160 | 160 | 160 | 160 | 160 | 157.5 | 6.494 | 13.527 | 13.837 | 14.55 |
| 82 | 150 | 170 | 170 | 170 | 170 | 170 | 170 | 165 | 6.494 | 14.448 | 14.885 | 15.633 |
| 83 | 150 | 180 | 180 | 180 | 180 | 180 | 180 | 172.5 | 6.494 | 15.182 | 15.933 | 16.715 |
| 84 | 160 | 120 | 120 | 120 | 120 | 120 | 120 | 130 | 6.149 | 14.194 | 13.359 | 14.002 |
| 85 | 160 | 130 | 130 | 130 | 130 | 130 | 130 | 137.5 | 6.149 | 15.085 | 14.602 | 15.282 |
| 86 | 160 | 140 | 140 | 140 | 140 | 140 | 140 | 145 | 6.149 | 16.154 | 15.844 | 16.561 |
| 87 | 160 | 146 | 146 | 146 | 146 | 146 | 146 | 149.5 | 6.149 | 16.879 | 16.59 | 17.329 |
| 88 | 160 | 150 | 150 | 150 | 150 | 150 | 150 | 152.5 | 6.149 | 17.361 | 17.087 | 17.841 |
| 89 | 160 | 160 | 160 | 160 | 160 | 160 | 160 | 160 | 6.149 | 18.462 | 18.329 | 19.121 |
| 90 | 160 | 170 | 170 | 170 | 170 | 170 | 170 | 167.5 | 6.149 | 19.567 | 19.572 | 20.4 |
| 91 | 160 | 180 | 180 | 180 | 180 | 180 | 180 | 175 | 6.149 | 20.308 | 20.814 | 21.68 |
| 92 | 170 | 120 | 120 | 120 | 120 | 120 | 120 | 132.5 | 5.882 | 16.907 | 15.984 | 16.674 |
| 93 | 170 | 130 | 130 | 130 | 130 | 130 | 130 | 140 | 5.882 | 18.015 | 17.352 | 18.081 |
| 94 | 170 | 140 | 140 | 140 | 140 | 140 | 140 | 147.5 | 5.882 | 19.278 | 18.719 | 19.487 |
| 95 | 170 | 146 | 146 | 146 | 146 | 146 | 146 | 152 | 5.882 | 20.123 | 19.54 | 20.331 |
| 96 | 170 | 150 | 150 | 150 | 150 | 150 | 150 | 155 | 5.882 | 20.688 | 20.087 | 20.894 |
| 97 | 170 | 160 | 160 | 160 | 160 | 160 | 160 | 162.5 | 5.882 | 21.978 | 21.455 | 22.301 |
| 98 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 170 | 5.882 | 23.156 | 22.822 | 23.707 |
| 99 | 170 | 180 | 180 | 180 | 180 | 180 | 180 | 177.5 | 5.882 | 23.795 | 24.19 | 25.114 |
| 100 | 180 | 120 | 120 | 120 | 120 | 120 | 120 | 135 | 5.679 | 18.298 | 17.216 | 17.932 |
| 101 | 180 | 130 | 130 | 130 | 130 | 130 | 130 | 142.5 | 5.679 | 19.451 | 18.626 | 19.382 |
| 102 | 180 | 140 | 140 | 140 | 140 | 140 | 140 | 150 | 5.679 | 20.697 | 20.037 | 20.833 |
| 103 | 180 | 146 | 146 | 146 | 146 | 146 | 146 | 154.5 | 5.679 | 21.555 | 20.883 | 21.703 |
| 104 | 180 | 150 | 150 | 150 | 150 | 150 | 150 | 157.5 | 5.679 | 22.13 | 21.448 | 22.283 |
| 105 | 180 | 160 | 160 | 160 | 160 | 160 | 160 | 165 | 5.679 | 23.44 | 22.858 | 23.734 |
| 106 | 180 | 170 | 170 | 170 | 170 | 170 | 170 | 172.5 | 5.679 | 24.552 | 24.269 | 25.184 |
| 107 | 180 | 180 | 180 | 180 | 180 | 180 | 180 | 180 | 5.679 | 25.017 | 25.68 | 26.635 |

TABLE S3. *ab-initio* calculated vs $^2J_{\text{Si-O-Si}}$ coupling model. Individual geometry, after structural constraint on Ω_0 and Ω_k , was optimized using RHF/6-311G(d). The *ab-initio* J -coupling were then evaluated on the optimized geometry and compare with Eq. (19) of the main document. Excellent agreement in J -coupling model and *ab-initio* result is observed. All Si-O bond distances were fixed to 1.6 Å and O-Si-O intra-tetrahedral angle set to 109.5°.

| Index | $\Omega_0/1^\circ$ | $\Omega_k/1^\circ$ | | | | | | $\overline{\langle \Omega \rangle}/1^\circ$ | $\phi/1^\circ$ optimized | $^2J_{\text{Si-O-Si-coupling}}/\text{Hz}$ | | |
|-------|--------------------|--------------------|------------|------------|------------|------------|------------|---|-----------------------------|---|--|--|
| | | Ω_1 | Ω_2 | Ω_3 | Ω_4 | Ω_5 | Ω_6 | | | <i>ab-initio</i> | $J(\Omega_0, \overline{\langle \Omega \rangle}, \phi)$ | $J(\Omega_0, \overline{\langle \Omega \rangle})$ |
| 108 | 130 | 142 | 142 | 142 | 142 | 142 | 142 | 139 | 48.553 | 2.374 | 2.8141 | 2.4048 |
| 109 | 140 | 142 | 142 | 142 | 142 | 142 | 142 | 141.5 | -3.63 | 7.1588 | 7.0094 | 7.6 |
| 110 | 150 | 142 | 142 | 142 | 142 | 142 | 142 | 144 | -1.01 | 12.333 | 11.911 | 12.602 |
| 111 | 160 | 142 | 142 | 142 | 142 | 142 | 142 | 146.5 | -48.131 | 18.823 | 17.438 | 16.817 |
| 112 | 170 | 142 | 142 | 142 | 142 | 142 | 142 | 149 | -43.526 | 21.655 | 20.298 | 19.769 |
| 113 | 180 | 142 | 142 | 142 | 142 | 142 | 142 | 151.5 | -163.34 | 22.695 | 21.663 | 21.123 |
| 114 | 130 | 146 | 146 | 146 | 146 | 146 | 146 | 142 | -51.352 | 2.2449 | 3.0886 | 2.6332 |
| 115 | 140 | 146 | 146 | 146 | 146 | 146 | 146 | 144.5 | 69.457 | 8.2131 | 8.4749 | 7.9345 |
| 116 | 150 | 146 | 146 | 146 | 146 | 146 | 146 | 147 | 6.494 | 12.329 | 12.369 | 13.035 |
| 117 | 160 | 146 | 146 | 146 | 146 | 146 | 146 | 149.5 | -43.389 | 18.997 | 17.832 | 17.329 |
| 118 | 170 | 146 | 146 | 146 | 146 | 146 | 146 | 152 | -44.749 | 22.294 | 20.911 | 20.331 |
| 119 | 180 | 146 | 146 | 146 | 146 | 146 | 146 | 154.5 | -158.46 | 23.025 | 22.07 | 21.703 |
| 120 | 130 | 149 | 149 | 149 | 149 | 149 | 149 | 144.25 | -53.188 | 2.323 | 3.2866 | 2.8045 |
| 121 | 140 | 149 | 149 | 149 | 149 | 149 | 149 | 146.75 | 68.928 | 8.0614 | 8.7422 | 8.1853 |
| 122 | 150 | 149 | 149 | 149 | 149 | 149 | 149 | 149.25 | -44.896 | 14.262 | 13.864 | 13.36 |
| 123 | 160 | 149 | 149 | 149 | 149 | 149 | 149 | 151.75 | -40.024 | 19.09 | 18.109 | 17.713 |
| 124 | 170 | 149 | 149 | 149 | 149 | 149 | 149 | 154.25 | -36.953 | 22.181 | 21.053 | 20.753 |
| 125 | 180 | 149 | 149 | 149 | 149 | 149 | 149 | 156.75 | -63.423 | 24.16 | 22.994 | 22.138 |
| 126 | 120 | 178 | 178 | 178 | 178 | 178 | 178 | 163.5 | -73.729 | -0.84366 | -0.80904 | -1.1504 |
| 127 | 130 | 178 | 178 | 178 | 178 | 178 | 178 | 166 | -69.237 | 4.3472 | 4.9844 | 4.4603 |
| 128 | 140 | 178 | 178 | 178 | 178 | 178 | 178 | 168.5 | -69.038 | 10.709 | 11.248 | 10.61 |
| 129 | 150 | 178 | 178 | 178 | 178 | 178 | 178 | 171 | -55.352 | 16.639 | 17.296 | 16.498 |
| 130 | 160 | 178 | 178 | 178 | 178 | 178 | 178 | 173.5 | -40.144 | 21.178 | 21.882 | 21.424 |
| 131 | 170 | 178 | 178 | 178 | 178 | 178 | 178 | 176 | -26.716 | 24.167 | 24.668 | 24.833 |
| 132 | 180 | 178 | 178 | 178 | 178 | 178 | 178 | 178.5 | -142.29 | 25.249 | 25.956 | 26.345 |

TABLE S4. *ab-initio* calculated vs $^2J_{\text{Si-O-Si}}$ coupling model. The initial geometry was optimized with RHF/6-311G(d). Individual geometry, after structural constraint on Ω_0 , Ω_k and ϕ , was not optimized. All Si-O bond distances were fixed to 1.6 Å and O-Si-O intra-tetrahedral angle set to 109.5°.

| Index | $\Omega_0/1^\circ$ | $\Omega_k/1^\circ$ | | | | | | $\overline{\langle \Omega \rangle}/1^\circ$ | $\phi/1^\circ$ | $^2J_{\text{Si-O-Si-coupling}}/\text{Hz}$ | | |
|-------|--------------------|--------------------|------------|------------|------------|------------|------------|---|----------------|---|--|--|
| | | Ω_1 | Ω_2 | Ω_3 | Ω_4 | Ω_5 | Ω_6 | | | <i>ab-initio</i> | $J(\Omega_0, \overline{\langle \Omega \rangle}, \phi)$ | $J(\Omega_0, \overline{\langle \Omega \rangle})$ |
| 133 | 140 | 140 | 140 | 140 | 130 | 130 | 130 | 136.25 | 6.935 | 6.5463 | 6.4733 | 7.0146 |
| 134 | 140 | 140 | 140 | 150 | 150 | 150 | 150 | 143.75 | 6.935 | 7.1414 | 7.2797 | 7.8508 |
| 135 | 140 | 140 | 140 | 160 | 160 | 160 | 160 | 147.5 | 6.935 | 7.4539 | 7.6829 | 8.269 |
| 136 | 140 | 140 | 140 | 170 | 170 | 170 | 170 | 151.25 | 6.935 | 7.7772 | 8.0862 | 8.6871 |
| 137 | 140 | 150 | 150 | 130 | 130 | 130 | 130 | 140 | 6.935 | 6.867 | 6.8765 | 7.4327 |
| 138 | 140 | 150 | 150 | 140 | 140 | 140 | 140 | 143.75 | 6.935 | 7.1414 | 7.2797 | 7.8508 |
| 139 | 140 | 150 | 150 | 160 | 160 | 160 | 160 | 151.25 | 6.935 | 7.7665 | 8.0862 | 8.6871 |
| 140 | 140 | 150 | 150 | 170 | 170 | 170 | 170 | 155 | 6.935 | 8.0846 | 8.4894 | 9.1052 |
| 141 | 150 | 130 | 146 | 146 | 146 | 146 | 146 | 145 | 6.494 | 11.882 | 12.09 | 12.747 |
| 142 | 150 | 140 | 146 | 146 | 146 | 146 | 146 | 146.25 | 6.494 | 12.129 | 12.264 | 12.927 |
| 143 | 150 | 150 | 146 | 146 | 146 | 146 | 146 | 147.5 | 6.494 | 12.47 | 12.439 | 13.107 |
| 144 | 150 | 160 | 146 | 146 | 146 | 146 | 146 | 148.75 | 6.494 | 12.848 | 12.614 | 13.288 |
| 145 | 150 | 170 | 146 | 146 | 146 | 146 | 146 | 150 | 6.494 | 13.223 | 12.789 | 13.468 |
| 146 | 120 | 154.5 | 153.24 | 142.43 | 158.36 | 134.56 | 157.87 | 142.62 | 47.643 | -2.1903 | -1.7321 | -2.0478 |
| 147 | 130 | 157.08 | 153.88 | 145.05 | 160.56 | 135.83 | 157.46 | 146.23 | 50.461 | 2.3991 | 3.4132 | 2.9554 |
| 148 | 140 | 160.95 | 155.8 | 147.36 | 161.25 | 137.16 | 153.78 | 149.54 | 51.534 | 8.11 | 9.0703 | 8.4962 |
| 149 | 150 | 164.5 | 159.12 | 148.42 | 160.44 | 138.09 | 149.49 | 152.51 | 52.6 | 13.882 | 14.508 | 13.83 |
| 150 | 160 | 158.21 | 163.61 | 149.71 | 158.25 | 139.28 | 147.48 | 154.57 | 55.06 | 18.593 | 18.973 | 18.194 |
| 151 | 170 | 153.31 | 166.12 | 149.46 | 157.43 | 140.91 | 144.64 | 156.48 | 56.761 | 21.393 | 22.015 | 21.172 |
| 152 | 125 | 142 | 156 | 160 | 158 | 149 | 161 | 147 | 7.845 | 0.10924 | 0.060112 | 0.48901 |
| 153 | 135 | 142 | 156 | 160 | 158 | 149 | 161 | 149.5 | 7.2 | 4.9043 | 5.3085 | 5.8538 |
| 154 | 145 | 142 | 156 | 160 | 158 | 149 | 161 | 152 | 6.701 | 10.224 | 10.705 | 11.353 |

TABLE S4. ...continued. *ab-initio* calculated vs $^2J_{\text{Si-O-Si}}$ coupling model, continued. The initial geometry was optimized with RHF/6-311G(d). Individual geometry, after structural constraint on Ω_0 , Ω_k and ϕ , was not optimized. All Si-O bond distances were fixed to 1.6 Å and O-Si-O intra-tetrahedral angle set to 109.5°.

| Index | $\Omega_0/1^\circ$ | $\Omega_k/1^\circ$ | | | | | | $\langle \overline{\Omega} \rangle/1^\circ$ | $\phi/1^\circ$ | $^2J_{\text{Si-O-Si-coupling}}/\text{Hz}$ | | |
|-------|--------------------|--------------------|------------|------------|------------|------------|------------|---|----------------|---|--|--|
| | | Ω_1 | Ω_2 | Ω_3 | Ω_4 | Ω_5 | Ω_6 | | | <i>ab-initio</i> | $J(\Omega_0, \langle \overline{\Omega} \rangle, \phi)$ | $J(\Omega_0, \langle \overline{\Omega} \rangle)$ |
| 155 | 155 | 142 | 156 | 160 | 158 | 149 | 161 | 154.5 | 6.311 | 15.398 | 15.572 | 16.307 |
| 156 | 165 | 142 | 156 | 160 | 158 | 149 | 161 | 157 | 6.007 | 19.632 | 19.344 | 20.144 |
| 157 | 175 | 142 | 156 | 160 | 158 | 149 | 161 | 159.5 | 5.772 | 22.186 | 21.594 | 22.436 |
| 158 | 170 | 145 | 155 | 160 | 167 | 172 | 161 | 162.5 | 5.882 | 21.671 | 21.455 | 22.301 |
| 159 | 170 | 137 | 170 | 153 | 150.1 | 179.9 | 170 | 162.5 | 5.882 | 20.741 | 21.455 | 22.301 |
| 160 | 170 | 157 | 166 | 137 | 166 | 173 | 161 | 162.5 | 5.882 | 21.563 | 21.455 | 22.301 |
| 161 | 170 | 146 | 164 | 150 | 162 | 168 | 170 | 162.5 | 5.882 | 21.491 | 21.455 | 22.301 |
| 162 | 160 | 145 | 155 | 160 | 167 | 172 | 161 | 160 | 6.149 | 18.143 | 18.329 | 19.121 |
| 163 | 160 | 137 | 170 | 153 | 150.1 | 179.9 | 170 | 160 | 6.149 | 17.095 | 18.329 | 19.121 |
| 164 | 160 | 157 | 166 | 137 | 166 | 173 | 161 | 160 | 6.149 | 18.127 | 18.329 | 19.121 |
| 165 | 160 | 146 | 164 | 150 | 162 | 168 | 170 | 160 | 6.149 | 17.913 | 18.329 | 19.121 |
| 166 | 150 | 145 | 155 | 160 | 167 | 172 | 161 | 157.5 | 6.494 | 13.23 | 13.837 | 14.55 |
| 167 | 150 | 137 | 170 | 153 | 150.1 | 179.9 | 170 | 157.5 | 6.494 | 12.175 | 13.837 | 14.55 |
| 168 | 150 | 157 | 166 | 137 | 166 | 173 | 161 | 157.5 | 6.494 | 13.275 | 13.837 | 14.55 |
| 169 | 150 | 146 | 164 | 150 | 162 | 168 | 170 | 157.5 | 6.494 | 12.964 | 13.837 | 14.55 |
| 170 | 130 | 145 | 155 | 160 | 167 | 172 | 161 | 152.5 | 7.502 | 2.5666 | 2.9301 | 3.4326 |
| 171 | 130 | 137 | 170 | 153 | 150.1 | 179.9 | 170 | 152.5 | 7.502 | 1.8455 | 2.9301 | 3.4326 |
| 172 | 130 | 157 | 166 | 137 | 166 | 173 | 161 | 152.5 | 7.502 | 2.6513 | 2.9301 | 3.4326 |
| 173 | 130 | 146 | 164 | 150 | 162 | 168 | 170 | 152.5 | 7.502 | 2.3541 | 2.9301 | 3.4326 |
| 174 | 180 | 145 | 155 | 160 | 167 | 172 | 161 | 165 | 5.679 | 23.192 | 22.858 | 23.734 |
| 175 | 180 | 137 | 170 | 153 | 150.1 | 179.9 | 170 | 165 | 5.679 | 22.472 | 22.858 | 23.734 |
| 176 | 180 | 157 | 166 | 137 | 166 | 173 | 161 | 165 | 5.679 | 22.973 | 22.858 | 23.734 |
| 177 | 180 | 146 | 164 | 150 | 162 | 168 | 170 | 165 | 5.679 | 23.06 | 22.858 | 23.734 |
| 178 | 135 | 164 | 155 | 140 | 150 | 166 | 172 | 152.12 | 7.2 | 5.1271 | 5.5453 | 6.1002 |
| 179 | 145 | 164 | 155 | 140 | 150 | 166 | 172 | 154.62 | 6.701 | 10.523 | 11.031 | 11.691 |
| 180 | 155 | 164 | 155 | 140 | 150 | 166 | 172 | 157.12 | 6.311 | 15.748 | 15.976 | 16.723 |
| 181 | 165 | 164 | 155 | 140 | 150 | 166 | 172 | 159.62 | 6.007 | 19.973 | 19.804 | 20.617 |
| 182 | 175 | 164 | 155 | 140 | 150 | 166 | 172 | 162.12 | 5.772 | 22.458 | 22.084 | 22.939 |
| 183 | 127.5 | 135.6 | 142.8 | 161.2 | 155.4 | 147.3 | 169.8 | 145.89 | 7.668 | 1.1973 | 1.2069 | 1.6604 |
| 184 | 132.5 | 135.6 | 142.8 | 161.2 | 155.4 | 147.3 | 169.8 | 147.14 | 7.346 | 3.5995 | 3.8128 | 4.324 |
| 185 | 142.5 | 135.6 | 142.8 | 161.2 | 155.4 | 147.3 | 169.8 | 149.64 | 6.814 | 8.8003 | 9.1787 | 9.7959 |
| 186 | 152.5 | 135.6 | 142.8 | 161.2 | 155.4 | 147.3 | 169.8 | 152.14 | 6.399 | 13.998 | 14.183 | 14.89 |
| 187 | 162.5 | 135.6 | 142.8 | 161.2 | 155.4 | 147.3 | 169.8 | 154.64 | 6.076 | 18.462 | 18.233 | 19.01 |
| 188 | 172.5 | 135.6 | 142.8 | 161.2 | 155.4 | 147.3 | 169.8 | 157.14 | 5.825 | 21.434 | 20.87 | 21.695 |
| 189 | 120 | 168.34 | 168.34 | 168.34 | 169.06 | 169.06 | 169.06 | 156.53 | -68.642 | -0.50969 | -1.0596 | -1.4502 |
| 190 | 129.9 | 168.34 | 168.34 | 168.34 | 169.06 | 169.06 | 169.06 | 159 | -63.499 | 4.9418 | 4.428 | 3.8716 |
| 191 | 130 | 172.78 | 172.78 | 172.78 | 173.11 | 173.11 | 173.11 | 162.21 | -63.442 | 4.7433 | 4.7408 | 4.1717 |
| 192 | 140 | 177.8 | 177.8 | 177.8 | 177.24 | 177.24 | 177.24 | 168.14 | -59.26 | 10.655 | 11.284 | 10.57 |
| 193 | 150 | 175.4 | 175.4 | 175.4 | 178.13 | 178.13 | 178.13 | 170.07 | -57 | 17.058 | 17.172 | 16.365 |
| 194 | 160 | 179.1 | 179.1 | 179.1 | 177.75 | 177.75 | 177.75 | 173.82 | -53.18 | 22.027 | 22.327 | 21.478 |
| 195 | 170 | 179.97 | 179.97 | 179.97 | 179.73 | 179.73 | 179.73 | 177.39 | -51.021 | 25.272 | 25.957 | 25.093 |
| 196 | 180 | 178.58 | 178.58 | 178.58 | 178.68 | 178.68 | 178.68 | 178.97 | -49.354 | 26.525 | 27.279 | 26.436 |
| 197 | 140 | 145 | 155 | 160 | 167 | 172 | 161 | 155 | 6.935 | 7.7815 | 8.4894 | 9.1052 |
| 198 | 140 | 137 | 170 | 153 | 150.1 | 179.9 | 170 | 155 | 6.935 | 6.8387 | 8.4894 | 9.1052 |
| 199 | 140 | 157 | 166 | 137 | 166 | 173 | 161 | 155 | 6.935 | 7.8553 | 8.4894 | 9.1052 |
| 200 | 140 | 146 | 164 | 150 | 162 | 168 | 170 | 155 | 6.935 | 7.5261 | 8.4894 | 9.1052 |

TABLE S5. *ab-initio* calculated vs $^2J_{\text{Si-O-Si}}$ coupling model from Sigma-2

| Index | $\Omega_0/1^\circ$ | $\Omega_k/1^\circ$ | | | | | | $\langle \overline{\Omega} \rangle/1^\circ$ | $\phi/1^\circ$ | $^2J_{\text{Si-O-Si-coupling}}/\text{Hz}$ | | |
|----------|--------------------|--------------------|------------|------------|------------|------------|------------|---|----------------|---|--|--|
| | | Ω_1 | Ω_2 | Ω_3 | Ω_4 | Ω_5 | Ω_6 | | | <i>ab-initio</i> | $J(\Omega_0, \langle \overline{\Omega} \rangle, \phi)$ | $J(\Omega_0, \langle \overline{\Omega} \rangle)$ |
| site 2-3 | 153.45 | 148.7 | 153.45 | 148.7 | 172.76 | 153.45 | 160.8 | 155.595 | 0.47 | 16.0 | 15.035 | 15.035 |
| site 1-3 | 172 | 137.2 | 158.21 | 158.21 | 160.8 | 153.45 | 153.45 | 158.165 | -0.45 | 22.07 | 20.958 | 20.958 |
| site 4-1 | 137.2 | 158.21 | 172.26 | 158.21 | 148.78 | 152.04 | 148.74 | 151.575 | 0.0 | 6.48 | 6.552 | 6.552 |
| site 4-2 | 148.74 | 137.2 | 148.74 | 152.04 | 148.74 | 153.45 | 153.45 | 148.8878 | 27.95 | 11.09 | 12.652 | 11.993 |