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## CaRMeN: A tool for analysing and deriving kinetics in the real world

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## **Supplemental material**

Table S1: Selection of experimental literature data [Ref.] for CH<sub>4</sub> conversion over Rh and surface reaction mechanisms [Mechanism] used for modeling these experiments.

	CH <sub>4</sub> /Ox	P (bar)	Temp (K)	GHSV/τ/Flow/U	Catalyst	Reactor type	Mechanism	Remarks	Ref.
	CH <sub>4</sub> /O <sub>2</sub> =0.8- 2.2	1.42	600 -1500	U₀(298K)=20.6 cm/s	Rh/ Al <sub>2</sub> O <sub>3</sub>	monolith	Hickman – Schmidt 1993 <sup>1</sup>		Hickman and Schmidt <sup>1</sup>
	CH <sub>4</sub> /O <sub>2</sub> = 1.8	1.10	T <sub>o</sub> =300	flow=7 slpm	Rh/ Al <sub>2</sub> O <sub>3</sub>	monolith	Maier – Deutschmann 2001 <sup>2</sup>		Deutschmann et al. <sup>2</sup>
C P	CH <sub>4</sub> /O <sub>2</sub> =1-1.78	1.10	573-1123	GHSV= 8 × 10 <sup>5</sup> - 4.5 × 10 <sup>6</sup> NI kg <sup>-1</sup> h <sup>-1</sup>	Rh or Rh/ $\gamma$ - Al <sub>2</sub> O <sub>3</sub> coated $\alpha$ -Al <sub>2</sub> O <sub>3</sub> foam	annular reactor	Maestri-Vlachos 2009 <sup>3</sup>	H <sub>2</sub> O, CO <sub>2</sub> , CO co-feed=1–2 %	Maestri et al. <sup>3</sup>
0	CH <sub>4</sub> /O <sub>2</sub> =1-4	1.40- 8.00	1060-1400	τ=1-75 × 10 <sup>-3</sup> s	Rh/α-Al₂O₃	fixed bed	Hickman – Schmidt 1993 <sup>1</sup>	industrially relevant conditions	Slaa et al. <sup>4</sup>
	CH <sub>4</sub> /O <sub>2</sub> =1.4, 2.0, 2.6	1.00	300-1500	flow=5 slpm	Rh-coated foam monoliths	monolith	Maier - Deutschmann 2001 <sup>2</sup> , Maestri- Vlachos 2009 <sup>3</sup>	spatially- resolved data	Williams et al. <sup>5</sup>

	CH₄/Ox	P (bar)	Temp (K)	GHSV/τ/Flow/U	Catalyst	Reactor type	Mechanism	Remarks	Ref.
	CH <sub>4</sub> /O <sub>2</sub> =1.4, 2.0, 2.8	1.00	300-1500	flow=5 slpm or 10 slpm	Rh-coated foam monoliths	monolith	Maier – Deutschmann 2001 <sup>2</sup>	spatially- resolved data	Horn et al. <sup>6</sup>
	CH <sub>4</sub> /O <sub>2</sub> =2.0	1.32- 1.52	T <sub>o</sub> =300	GHSV=200-500 Nm <sup>3</sup> kg <sup>-1</sup> h <sup>-1</sup>	Rh/ Al <sub>2</sub> O <sub>3</sub> spheres	fixed bed	Maier – Deutschmann 2001 <sup>2</sup>	integral conversion and selectivity	Bizzi et al. <sup>7</sup>
	CH <sub>4</sub> /O <sub>2</sub> =3.0	1.32- 1.52	T <sub>o</sub> =300	GHSV=200-500 Nm <sup>3</sup> kg <sup>-1</sup> h <sup>-1</sup>	Rh/ Al₂O₃ spheres	fixed bed	Maier – Deutschmann 2001 <sup>2</sup>		Bizzi et al. <sup>8</sup>
	CH <sub>4</sub> /O <sub>2</sub> =1.7	1.10	385-1000	τ=20×10 <sup>-3</sup> s	Rh/α-Al₂O₃	honeycomb monolith	Maier – Deutschmann 2001 <sup>2, 9</sup>	transient light- off experiments	Schwiedernoch et al. <sup>9</sup>
	CH <sub>4</sub> /O <sub>2</sub> = 2, 1.7	1.10	T₀=298	GHSV=1.0 × 10 <sup>5</sup> h <sup>-1</sup>	Rh/α-Al₂O₃	foam monolith	Maier – Deutschmann 2001 <sup>2</sup>	Effect of He, $H_2O$ , and $CO_2$ addition	Ding et al. <sup>10</sup>
	CH <sub>4</sub> /O <sub>2</sub> = 2.0	1.10	$T_o$ =ambient	GHSV=4.0 × 10 <sup>5</sup> h <sup>-1</sup>	Rh/γ-Al₂O₃	monolith	Maier – Deutschmann 2001 <sup>9</sup>	Transient species profiles	Williams et al. <sup>11</sup>
	CH <sub>4</sub> /O <sub>2</sub> = 0.9– 1.75	5.00	T <sub>o</sub> =429-457	U <sub>in</sub> =0.28-0.57 m/s	Rh/Al₂O₃ ceramic plates	coated channel flow reactor	Maier – Deutschmann 2001 <sup>9</sup> , Kraus - Lindstedt 2017 <sup>12</sup>	optically accessible channel flow reactor- Raman-LIF	Sui et al. <sup>13</sup>
	CH <sub>4</sub> /O <sub>2</sub> = 0.15- 0.2	2.00- 12.00	T <sub>o</sub> =377-476	U <sub>in</sub> =0.21-1.25 m/s	Rh/Al₂O₃ coated ceramic plates	coated channel flow reactor	Karakaya - Deutschmann 2016 <sup>14</sup> , Deshmuhk - Vlachos 2007 <sup>15</sup> , Kraus - Lindstedt 2017 <sup>12</sup>	in situ Raman	Sui et al. <sup>16</sup>
	CH4/O2 = 2.5-4	4.00- 6.00	T₀ =385-673	U <sub>in</sub> =0.19-13.20 m/s	Rh/ZrO <sub>2</sub> coated ceramic plates	coated channel flow reactor	Maier – Deutschmann 2001 <sup>9</sup> , Kraus - Lindstedt 2017 <sup>12</sup>	in situ Raman	Appel et al. <sup>17</sup>

	CH <sub>4</sub> /Ox	P (bar)	Temp (K)	GHSV/τ/Flow/U	Catalyst	Reactor type	Mechanism	Remarks	Ref.
	CH <sub>4</sub> /O <sub>2</sub> = 2.0	5.00	T₀ =473, 573, 623 K	U <sub>in</sub> =3.90-5.10 m/s	Rh/Al <sub>2</sub> O <sub>3,</sub> Rh/ZrO <sub>2</sub> , Rh/CeO <sub>2</sub> - ZrO <sub>2</sub>	coated channel flow reactor	Maier – Deutschmann 2001 <sup>9</sup>	<i>in situ</i> Raman, H <sub>2</sub> O and CO <sub>2</sub> co-feed	Ericksson et al. <sup>18</sup>
	CH <sub>4</sub> /O <sub>2</sub> =0.56- 2.06	0.50	873-1023	flow=15.5 slpm	Rh/ Al <sub>2</sub> O <sub>3</sub>	stagnation flow	Karakaya – Deutschmann 2016 <sup>14</sup>		Karakaya et al. <sup>14</sup>
	CH4/O2=2	1.10	T <sub>o</sub> =423, T <sub>cat</sub> <673	flow=5 slpm	Rh or Rh/ $\gamma$ - Al <sub>2</sub> O <sub>3</sub> coated $\alpha$ -Al <sub>2</sub> O <sub>3</sub> foam	annular reactor	Maestri - Vlachos 2009 <sup>3</sup>	spatially resolved autothermal experiments - effect of washcoat addition	Donazzi et al. <sup>19</sup>
	CH4/O2=1.78	1.10	T₀ =533-623	flow=10 Nl/m	Rh/ α-Al <sub>2</sub> O <sub>3</sub> monolith	adiabatic lab scale reactor	Maestri - Vlachos 2009 <sup>3</sup>	spatially resolved CPO experiments - CO <sub>2</sub> addition	Donazzi et al. <sup>20</sup>
	CH4/O2=1-1.78	1.10	623-1123	GHSV= 8 × $10^{5}$ - 4.5 × $10^{6}$ NI/ kg <sup>-1</sup> h <sup>-1</sup>	Rh/ $\alpha$ -Al <sub>2</sub> O <sub>3</sub>	annular reactor	Maestri - Vlachos 2009 <sup>3</sup>	H <sub>2</sub> O, CO <sub>2</sub> , CO, H <sub>2</sub> co-feed=1– 2%	Donazzi et al. <sup>21</sup>
	CH4/O2=1.75	1.00- 4.00	T <sub>o</sub> =623	flow=10 NI/m	Rh/Al₂O₃	honeycomb monolith	Maestri - Vlachos 2009 <sup>3</sup>	spatially resolved temperature and concentration profiles	Donazzi et al. <sup>22</sup>
S	S/C = 1-3	1.10	673–823	GHSV=30000-70000 h <sup>-1</sup>	$Rh/CeO_2$ - $ZrO_2$ -La $_2O_3$	fixed bed	Kechagiopoulos – Lemonidou 2017 <sup>23</sup>	low temperature SR	Kechagiopoulos et al. <sup>23</sup>
R	S/C =1.5, 2, 2.5	1.10	623-1123	GHSV= 2 × 10 <sup>6</sup> NI kg <sup>-1</sup> h <sup>-1</sup>	$Rh/\alpha$ - $Al_2O_3$	annular reactor	Maestri - Vlachos 2009 <sup>3</sup>		Donazzi et al. <sup>21</sup>

	CH₄/Ox	P (bar)	Temp (K)	GHSV/τ/Flow/U	Catalyst	Reactor type	Mechanism	Remarks	Ref.
	S/C =1.04-1.06	0.50	973, 1008	flow=17.2 slpm	Rh/ Al <sub>2</sub> O <sub>3</sub>	stagnation flow	Karakaya – Deutschmann 2016 <sup>14</sup>		Karakaya et al. <sup>14</sup>
	S/C =2.2-4	1.10	673-1123	GHSV= 40000 h <sup>-1</sup>	Rh/ Al <sub>2</sub> O <sub>3</sub>	honeycomb monolith	Schädel - Deutschmann 2009 <sup>24</sup>	Exp. also with $C_2H_6$ , $C_3H_8$ , $C_4H_{10}$	Schädel et al. <sup>24</sup>
	S/C=4	1.10	973	GHSV= 48000 h <sup>-1</sup>	Rh/CeO₂	Microchan nel reactor	Thormann - Deutschmann 2009 <sup>25</sup>	Exp. also with propane and hexadecane	Thormann et al. 25
A T R	16.7% CH₄, 0– 40.0% H₂O, 1.7–16.7% O₂	1.00	573-1073	GHSV=7200 h <sup>-1</sup>	Rh/ Al <sub>2</sub> O <sub>3</sub>	fixed bed	Maier - Deutschmann 2001 <sup>2</sup>	Exp. data taken from Ayabe et al. <sup>26</sup>	Dixit et al. <sup>27</sup>
D R	$CO_2=1-4\%$ , $CH_4=1-2\%$ , $O_2$ co-feed=0.1%, $H_2$ $co-$ feed=0.1-1%	1.10	623-1123	GHSV= $2 \times 10^6$ NI kg <sub>cat</sub> <sup>-1</sup> h <sup>-1</sup>	Rh/a-Al₂O₃	annular reactor	Maestri-Vlachos 2009 <sup>3</sup>		Donazzi et al. <sup>28</sup>
	CH <sub>4</sub> /CO <sub>2</sub> =1.1	0.50	973	Flow=15.5 slpm	Rh/ Al <sub>2</sub> O <sub>3</sub>	stagnation flow	Karakaya – Deutschmann 2016 <sup>14</sup>		Karakaya et al. <sup>14</sup>
W G S	CO/H <sub>2</sub> O/N <sub>2</sub> = 4/2.7/93.3, 1.5/2.3/96.2, 1.5/3.5/95.	1.10	623-546	GHSV= $2 \times 10^6$ NI kg <sub>cat</sub> <sup>-1</sup> h <sup>-1</sup>	Rh/ Al₂O₃	annular reactor	Maestri - Vlachos 2009 <sup>3</sup>		Donazzi et al. <sup>21</sup>
R W G S	CO=1-2%, H <sub>2</sub> O=1-4%	1.10	623-546	GHSV= $2 \times 10^6$ NI kg <sub>cat</sub> <sup>-1</sup> h <sup>-1</sup>	Rh/ Al <sub>2</sub> O <sub>3</sub>	annular reactor	Maestri-Vlachos 2009 <sup>3</sup>	Also CO & H <sub>2</sub> - rich combustion tests	Donazzi et al. <sup>28</sup>

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