

Electronic Supplementary Information for

## Isolating and Quantifying the Impact of Domain Purity on the Performance of Bulk Heterojunction Solar Cells

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### Derivation of TSI with constant mass fraction.

To solve for the volume fraction of the domains, we use the mass and density of each component of the domains:

$$v_1 = \frac{\frac{m_{11}}{\rho_1} + \frac{m_{21}}{\rho_2}}{\frac{m_{11} + m_{12}}{\rho_1} + \frac{m_{21} + m_{22}}{\rho_2}} \quad (1)$$

$$v_2 = \frac{\frac{m_{12}}{\rho_1} + \frac{m_{22}}{\rho_2}}{\frac{m_{11} + m_{12}}{\rho_1} + \frac{m_{21} + m_{22}}{\rho_2}} \quad (2)$$

where  $m_{ij}$  is the mass (or a fraction of total system mass) of material  $i$  in domain  $j$ , and  $\rho_i$  is the density of material  $i$ . We can normalize  $m_{ij}$  relative to the overall mass of the film by defining the overall fraction of mass of each material ( $m_1$  and  $m_2$  where  $m_1 + m_2 = 1$ ) and the weight percent of component  $i$  in domain  $j$  ( $p_{ij}$ ).

$$m_{11} = m_1 - m_{12} \quad (3)$$

$$m_{22} = m_2 - m_{21} \quad (4)$$

$$\frac{m_{21}}{m_{21} + m_{11}} = P_{21} \quad (5)$$

$$\frac{m_{12}}{m_{12} + m_{22}} = P_{12} \quad (6)$$

The denominator in the preceding two equations is the global mass fraction of the corresponding domain.

Solving these coupled equations for  $v_1$  and  $v_2$  in terms of only relevant or known variables  $m_1, P_{12}, P_{21}, \rho_1$ , and  $\rho_2$  we obtain

$$v_1 = \frac{(m_1 - P_{12}) \left( \frac{1}{\rho_1} + P_{21} \left( \frac{1}{\rho_2} - \frac{1}{\rho_1} \right) \right)}{\left( \frac{1 - m_1}{\rho_2} + \frac{m_1}{\rho_1} \right) (1 - P_{12} - P_{21})} \quad (7)$$

$$v_2 = \frac{\left( \frac{1 - P_{12}}{\rho_2} + \frac{P_{12}}{\rho_1} \right) (1 - m_1 - P_{21})}{\left( \frac{1 - m_1}{\rho_2} + \frac{m_1}{\rho_1} \right) (1 - P_{12} - P_{21})} \quad (8)$$

Contrast between two domains ( $C_{d_1d_2}$ ) is a function of the differences in refractive indices in the two domains,  $n_{d_1}$  and  $n_{d_2}$

$$C_{d_1d_2} = (n_{d_1} - n_{d_2})^2 \quad (9)$$

Defining the indices of refraction for the pure materials as  $n_i$  for material  $i$ , we can solve for  $n_{d_1}$  and  $n_{d_2}$  as the volume average of the components within each domain

$$n_{d_1} = n_1 v_{11} + n_2 v_{21} \quad (10)$$

$$n_{d_2} = n_2 v_{22} + n_1 v_{12} \quad (11)$$

where  $v_{ij}$  is defined to be the volume fraction of material  $i$  in domain  $j$  (importantly different than the earlier  $v_i$  which were volume fractions of the domains), which we can solve for as

$$v_{ij} = \frac{\frac{m_{ij}}{d_i}}{\frac{m_{1j}}{d_1} + \frac{m_{2j}}{d_2}} \quad (12)$$

Using equations (4-7), (11-13), again solving only in terms of known variables, we obtain:

$$n_{d_1} = \frac{\frac{n_1(1 + P_{21})}{\rho_1} + \frac{n_2 P_{21}}{\rho_2}}{\frac{1 - P_{21}}{\rho_1} + \frac{P_{21}}{\rho_2}} \quad (13)$$

$$n_{d_2} = \frac{\frac{n_2(1 + P_{12})}{\rho_2} + \frac{n_1 P_{12}}{\rho_1}}{\frac{1 - P_{12}}{\rho_2} + \frac{P_{12}}{\rho_1}} \quad (14)$$

To calculate the relative contrast between the domains,  $C$  we can normalize by the contrast when there is no mixing,  $C_0$

$$C_0 = (n_1 - n_2)^2 \quad (15)$$

$$C = \frac{C_{d1d2}}{C_0} = \frac{\frac{(1 - P_{12} - P_{21})^2}{\rho_1^2 \rho_2^2}}{\left(\frac{1 - P_{12}}{\rho_2} + \frac{P_{12}}{\rho_1}\right)^2 \left(\frac{P_{21}}{\rho_2} + \frac{1 - P_{21}}{\rho_1}\right)^2} \quad (16)$$

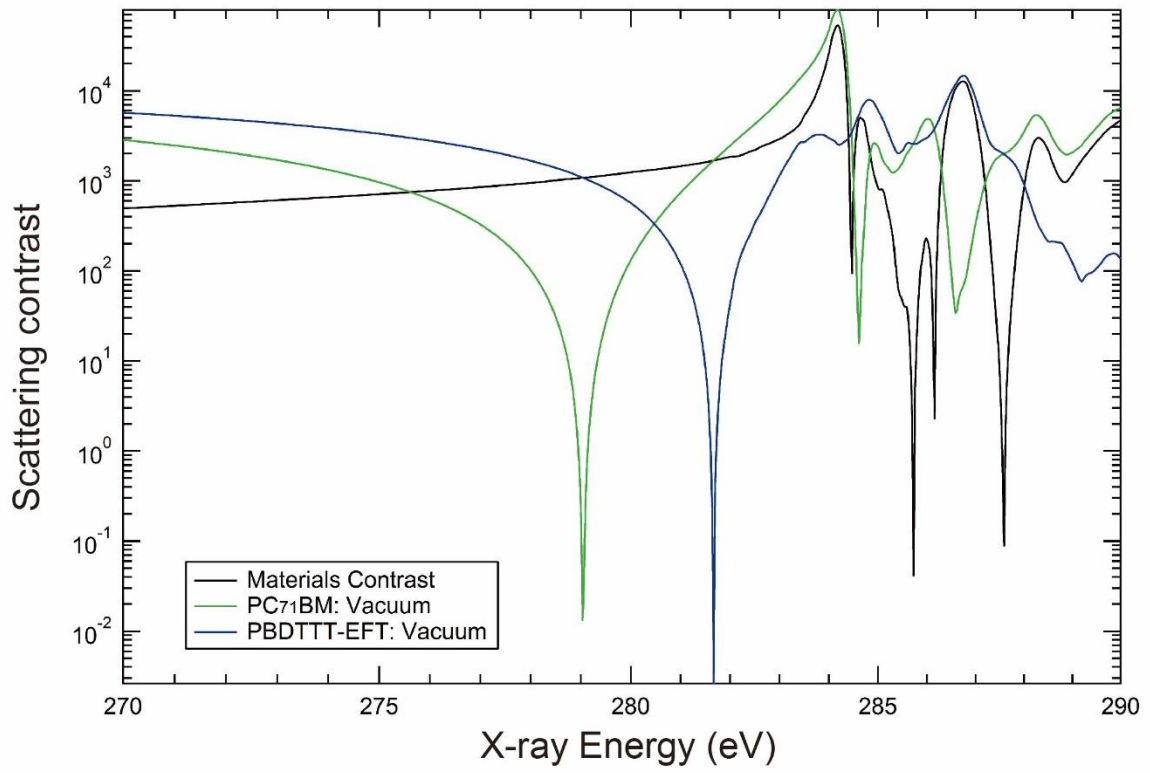
so only the densities of the components and the degree of mixing matters in the final relative contrast.

We find it useful to define rather than  $\rho_1$  and  $\rho_2$  the relative difference between the densities  $\rho_r$  as

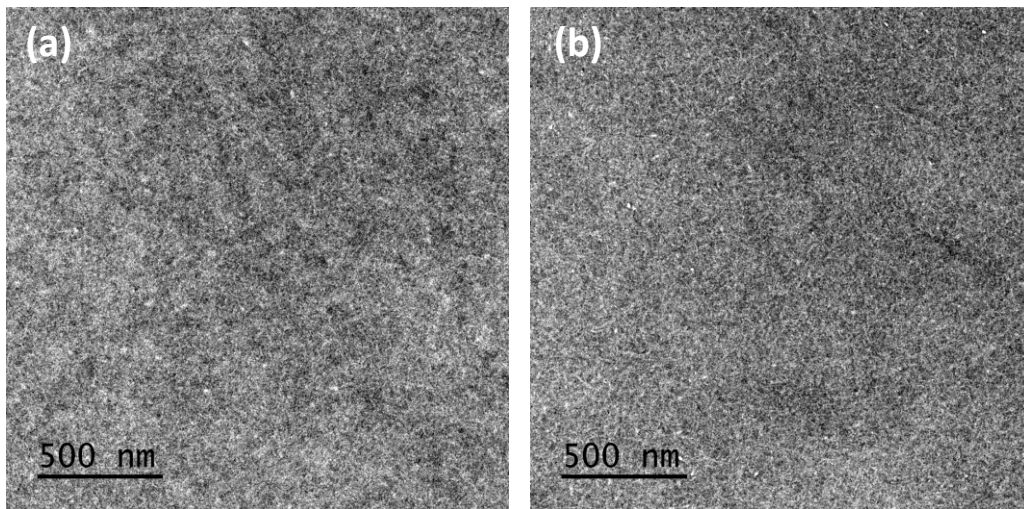
$$\rho_r = 1 - \frac{\rho_1}{\rho_2} \quad (17)$$

Putting this all together, we can now solve for TSI in terms of relevant variables.

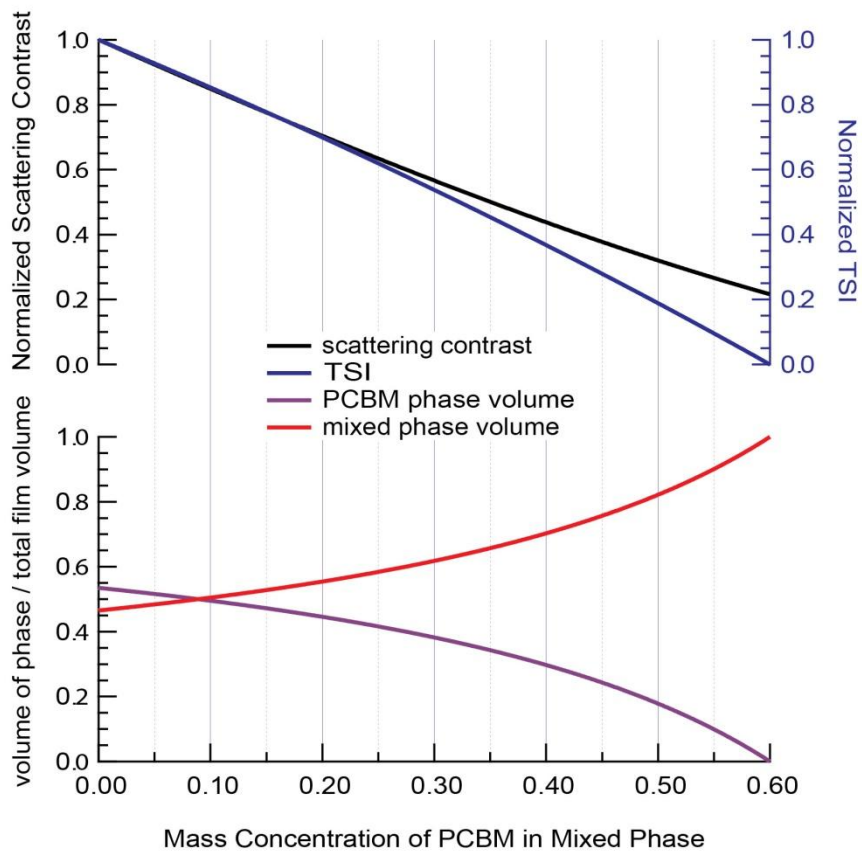
$$TSI \propto \frac{(1 + \rho_r)^2 (m_1 - P_{12}) (1 - m_1 - P_{21})}{(1 + m_1 \rho_r)^2 (1 + \rho_r P_{12}) (1 + \rho_r (1 - P_{21}))} \quad (18)$$



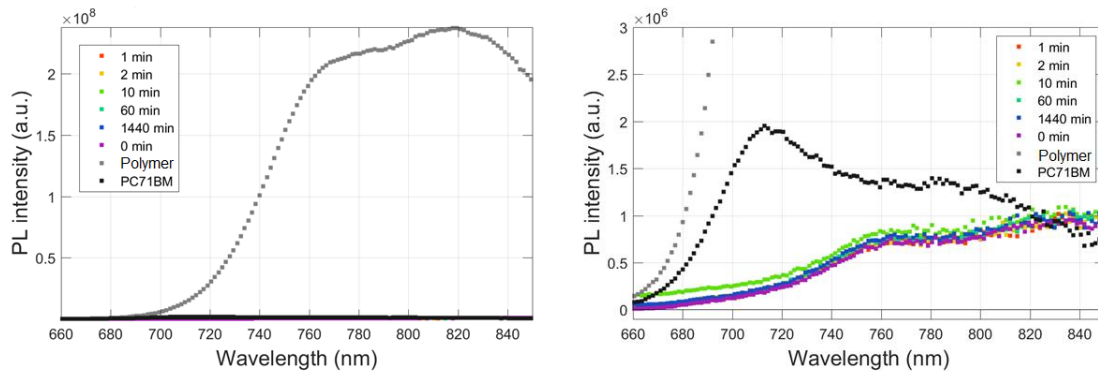
**Fig. S1** Calculation of R-SoXS scattering functions



**Fig. S2** Bright-field TEM images of PBDTTT-EFT:PC<sub>71</sub>BM films prepared with (a) AST just after spin-coating and (b) after 24 hours revealing no significant difference in the visual morphology.



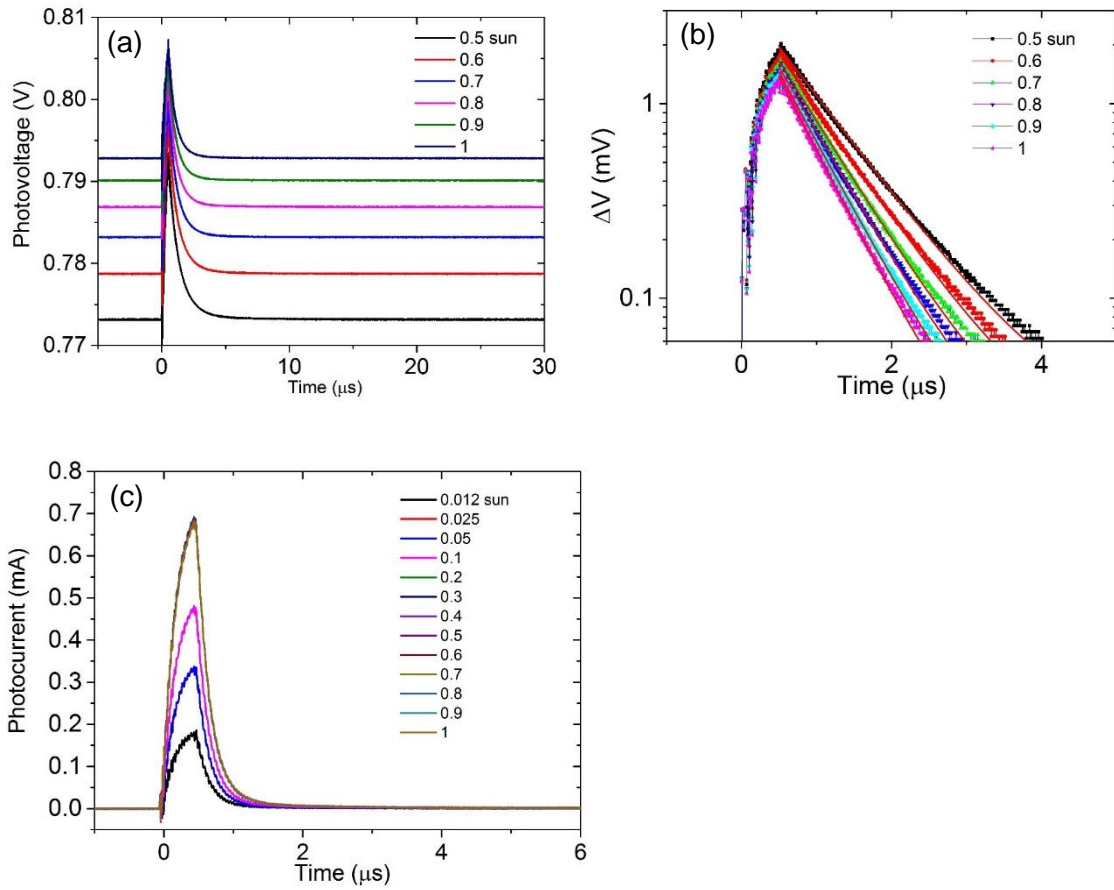
**Fig. S3** Plot of equation 2 from the main manuscript.



**Fig. S4.** Photoluminescence spectra of PBDTTT-EFT/PC<sub>71</sub>BM blends referenced to the photoluminescence spectra of neat polymer and fullerene films. A wavelength of 625 nm was used for photoexcitation.

**Table S1.** Calculated PL Quenching efficiencies

Delay time	PL Quenching Efficiency (%)
1 minute	93.4
2 minutes	99.4
10 minutes	99.2
1 hour	99.3
24 hours	99.3
No AST	99.4



**Fig. S5** (a) Raw data of transient photovoltage measurements at different background intensities. (b) Plot showing  $\Delta V$  as the function of time with the monoexponential fits. (c) Transient photocurrent curves obtained by using  $50 \Omega$  termination in the oscilloscope.