

## Supplementary Information

# Efficient Removal of Pb (II) from Water by Magnetic Fe<sub>3</sub>S<sub>4</sub>/reduced Graphene Oxide Composites

Long Kong, Zhichun Li, Xueqiong Huang, Shouqiang Huang, Hua Sun, Min Liu, and Liang Li\*

School of Environmental Science and Engineering, Shanghai Jiao Tong University, 800  
Dongchuan Road, Shanghai 200240, P. R. China  
E-mail: liangli117@sjtu.edu.cn; Tel: +86 21 54747567

Supplementary information contains 12 pages, 11 figures, and 4 tables.

### Adsorption model:

All the adsorption kinetics data were fitted with two different kinetic models, pseudo-first-order model and pseudo-second-order model, expressed as follows: <sup>1</sup>

$$\ln (q_e - q_t) = \ln q_e - k_1 t \quad (1)$$

$$\frac{t}{q_t} = \frac{1}{k_2 q_e^2} + \frac{1}{q_e} t \quad (2)$$

Where  $q_t$  and  $q_e$  are the amount of adsorption at any time  $t$  (min) and equilibrium (mg g<sup>-1</sup>).  $k_1$  (min<sup>-1</sup>) and  $k_2$  (g (mg·min)<sup>-1</sup>) denote the rate constant of pseudo-first-order and pseudo-second-order sorption, respectively.

The Langmuir and Freundlich isotherm model were employed to simulate the adsorption isotherm data and can be described as: <sup>2</sup>

$$\frac{C_e}{q_e} = \frac{C_e}{q_m} + \frac{1}{q_m K_L} \quad (3)$$

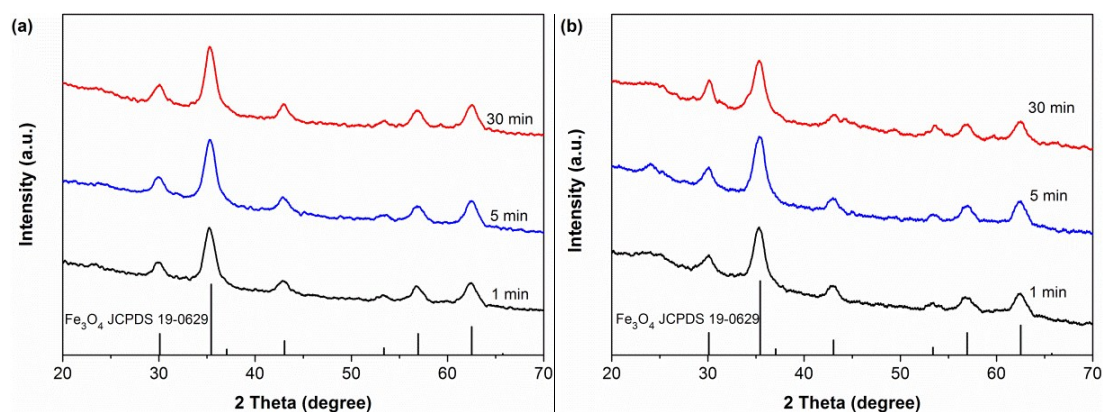
$$\ln q_e = \ln K_F + \frac{1}{n} \ln C_e \quad (4)$$

where  $C_e$  is the equilibrium concentration in the liquid phases (mg L<sup>-1</sup>),  $q_m$  represent the maximum adsorption capacity (mg g<sup>-1</sup>), respectively.  $K_L$  and  $K_F$  are Langmuir sorption constant related to the affinity parameter of adsorbent and Freundlich adsorption capacity, respectively.  $1/n$  refers to the Freundlich adsorption intensity parameter.

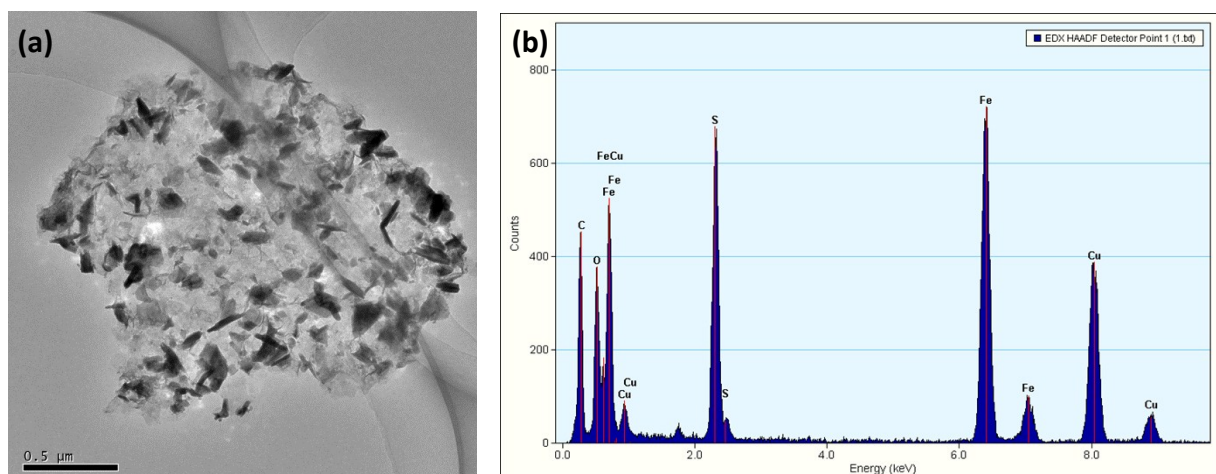
The distribution ratio ( $K_d$ ) was obtained from the following equation: <sup>3</sup>

$$K_d = \frac{(C_0 - C_e) V}{C_0 m} \quad (5)$$

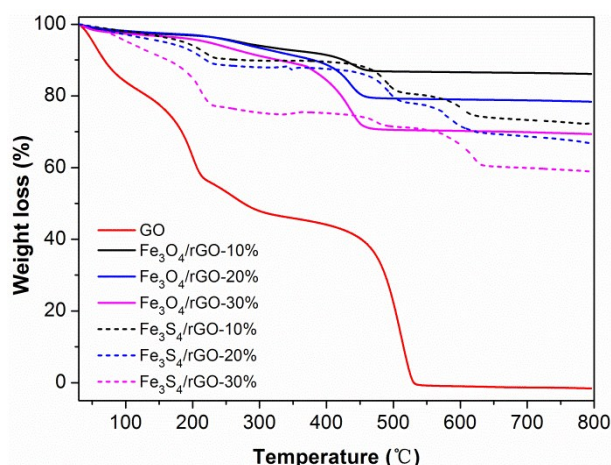
Where  $C_0$  is the initial concentration of Pb(II) (mg/L),  $V$  denotes the volume of the solution (mL),  $m$  is the weight of adsorbent (g).



**Fig S1** XRD patterns of Fe<sub>3</sub>O<sub>4</sub>/rGO after the sulfuration reaction using (a) oleylamine and (b) 1-butylamine as solvent for sulfur powders.

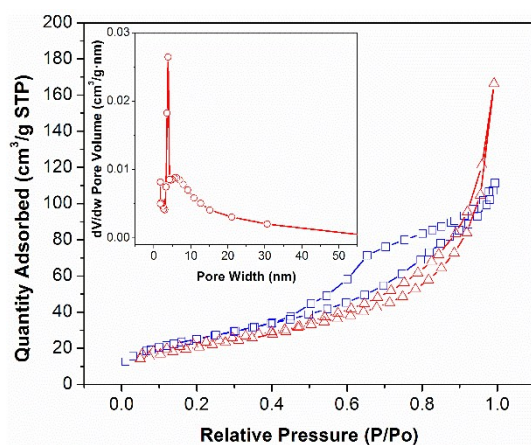


**Fig S2** (a) TEM images of Fe<sub>3</sub>S<sub>4</sub>/rGO after the sulfuration over 5 min, (b) EDX results of selected areas of Fe<sub>3</sub>S<sub>4</sub>/rGO.

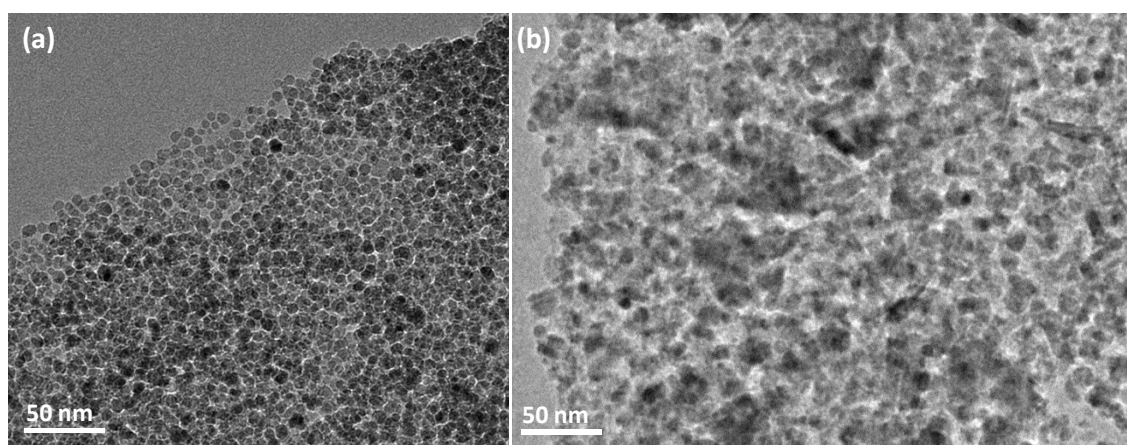


**Fig S3** TGA curves of GO, Fe<sub>3</sub>O<sub>4</sub>/rGO, and Fe<sub>3</sub>S<sub>4</sub>/rGO measured from 25 to 800 °C in air atmosphere.

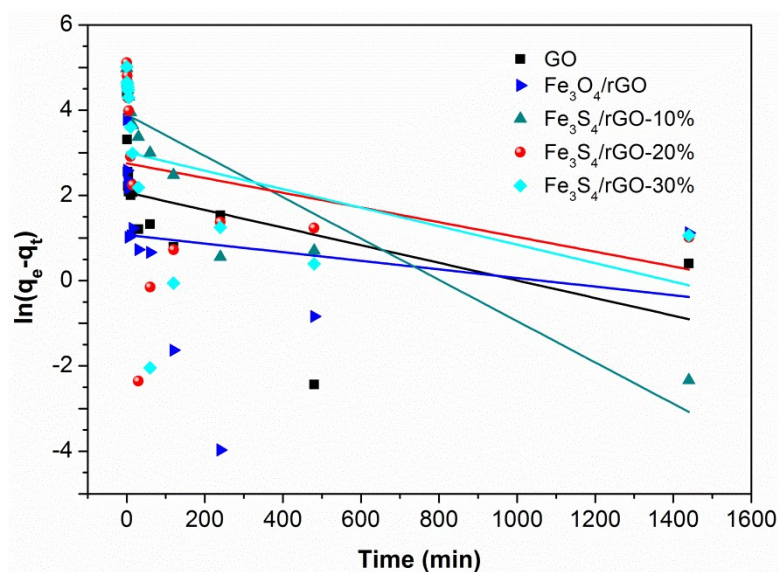
The content of Fe<sub>3</sub>O<sub>4</sub> and Fe<sub>3</sub>S<sub>4</sub> in the resultant Fe<sub>3</sub>O<sub>4</sub>/rGO or Fe<sub>3</sub>S<sub>4</sub>/rGO composites was confirmed by TGA analysis. As shown in Fig S3, the residual weight of Fe<sub>3</sub>O<sub>4</sub>/rGO was 86.13%, 78.38%, and 69.35% for Fe<sub>3</sub>O<sub>4</sub>/rGO-10%, Fe<sub>3</sub>O<sub>4</sub>/rGO-20%, and Fe<sub>3</sub>O<sub>4</sub>/rGO-30% after the samples was heated to 800 in air.<sup>[4]</sup> It was pointed out that the Fe<sub>3</sub>O<sub>4</sub> phase in the Fe<sub>3</sub>O<sub>4</sub>/rGO can be oxidized by air to Fe<sub>2</sub>O<sub>3</sub>. Based on the weight of Fe<sub>2</sub>O<sub>3</sub> after 800 °C, the Fe<sub>3</sub>O<sub>4</sub> content in Fe<sub>3</sub>O<sub>4</sub>/rGO-10%, Fe<sub>3</sub>O<sub>4</sub>/rGO-20%, and Fe<sub>3</sub>O<sub>4</sub>/rGO-30% was calculated to be 83.25%, 75.77%, and 67.21%. Accordingly, the content of rGO was about 16.75 wt%, 24.23 wt%, and 32.79 wt%, respectively. As for Fe<sub>3</sub>S<sub>4</sub>/rGO, it exhibited a different thermal oxidative degradation features since Fe<sub>3</sub>O<sub>4</sub> and Fe<sub>3</sub>S<sub>4</sub> coexisted in the composites. Under test conditions (25-800 °C, air flow), the weight loss of Fe<sub>3</sub>S<sub>4</sub>/rGO corresponds to the oxidation of Fe<sub>3</sub>O<sub>4</sub> and Fe<sub>3</sub>S<sub>4</sub> and the decomposition of rGO, leaving the final products as Fe<sub>2</sub>O<sub>3</sub>. The remaining weight of Fe<sub>3</sub>S<sub>4</sub>/rGO-10%, Fe<sub>3</sub>S<sub>4</sub>/rGO-20%, and Fe<sub>3</sub>S<sub>4</sub>/rGO-30% composites was 72.21%, 66.77%, and 58.89%, respectively. The difference of residual weight between Fe<sub>3</sub>O<sub>4</sub>/rGO and its corresponding Fe<sub>3</sub>S<sub>4</sub>/rGO composite was assigned to the weight loss in oxidation process of Fe<sub>3</sub>S<sub>4</sub>. Therefore, the Fe<sub>3</sub>S<sub>4</sub> content was calculated to be about 61.89%, 51.99%, and 47.59% in Fe<sub>3</sub>S<sub>4</sub>/rGO-10%, Fe<sub>3</sub>S<sub>4</sub>/rGO-20%, and Fe<sub>3</sub>S<sub>4</sub>/rGO-30%. The accurate contents of Fe<sub>3</sub>O<sub>4</sub> and Fe<sub>3</sub>S<sub>4</sub> in the composites were listed in Table S2.



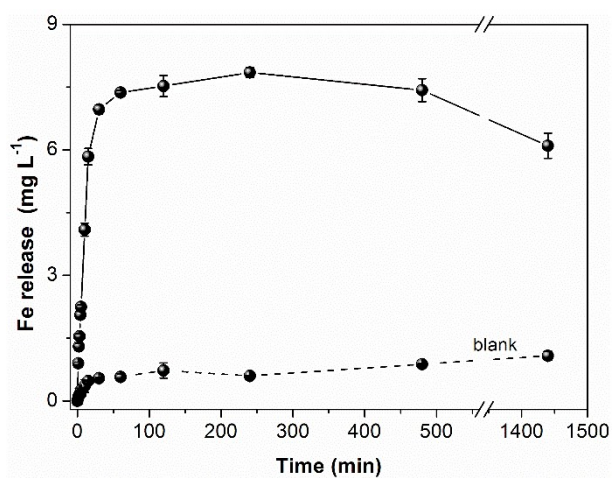
**Fig S4** Nitrogen adsorption-desorption isotherms of  $\text{Fe}_3\text{O}_4/\text{rGO}$  and  $\text{Fe}_3\text{S}_4/\text{rGO}$ . Inset: BJH pore size distribution (mainly 3-4 nm) of  $\text{Fe}_3\text{S}_4/\text{rGO}$ .



**Fig S5** TEM images of (a)  $\text{Fe}_3\text{O}_4/\text{rGO}-10\%$  and (b)  $\text{Fe}_3\text{S}_4/\text{rGO}-10\%$ .

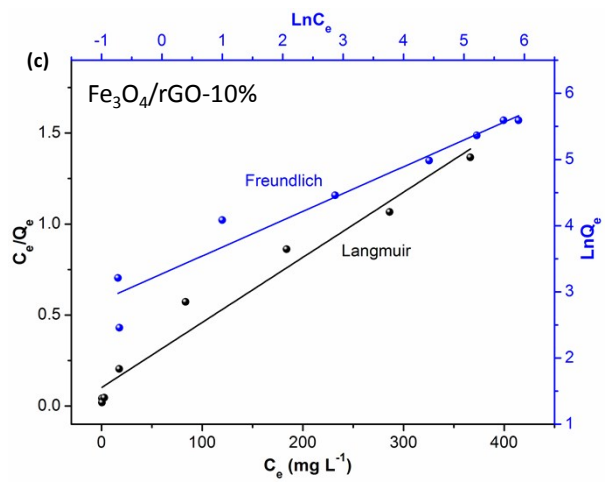
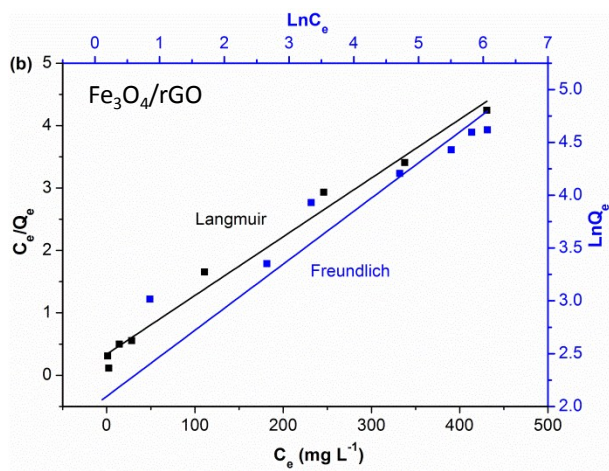
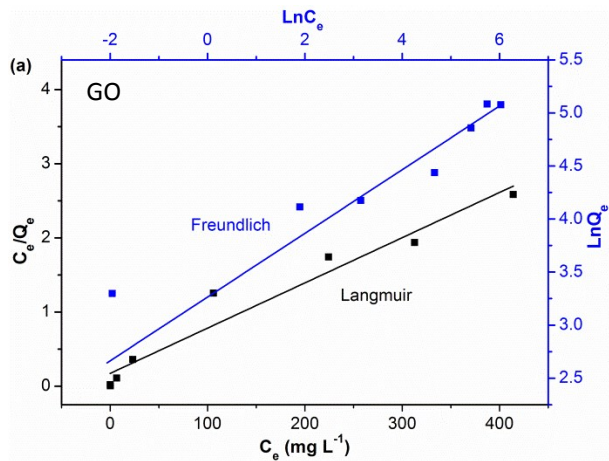


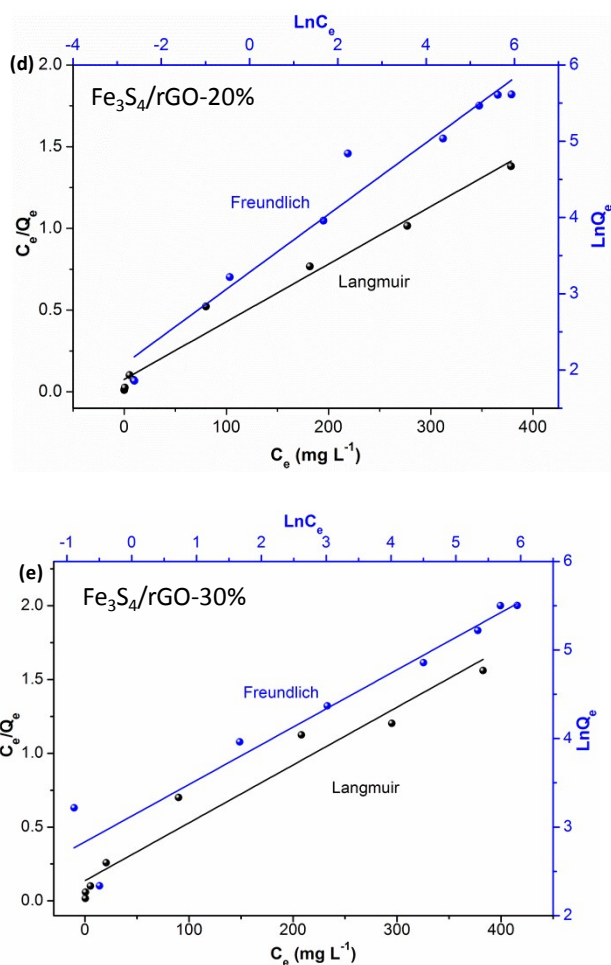
**Fig S6** Test of pseudo-first-order model for adsorption of Pb (II) on different adsorbents. The symbols are experimental data and the solid lines represent the fitted curves.



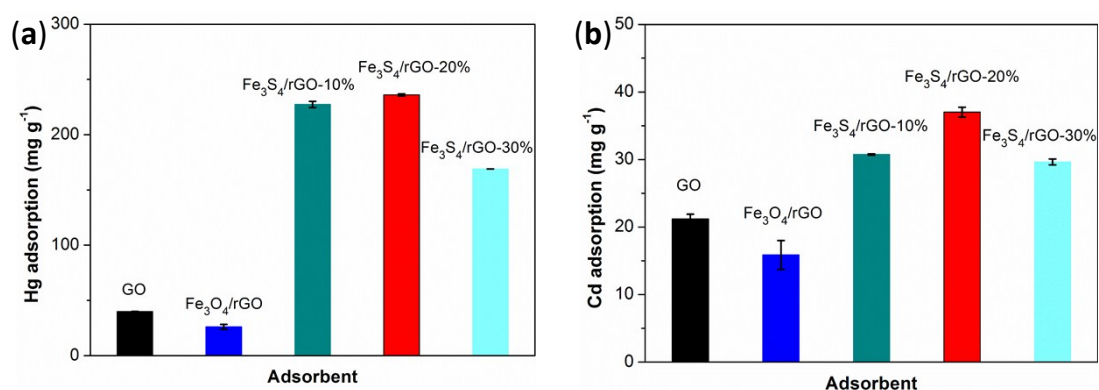
**Fig S7** Fe release kinetics of  $\text{Fe}_3\text{S}_4/\text{rGO}$  in the adsorption process toward Pb (II). Experimental conditions: initial Pb (II) concentration  $50 \text{ mg L}^{-1}$  100 mL, sorbent 25 mg, pH 6, temperature  $25^\circ\text{C}$ . The dash line represented the blank samples,  $\text{Fe}_3\text{S}_4/\text{rGO}$  solution without the addition of Pb (II).





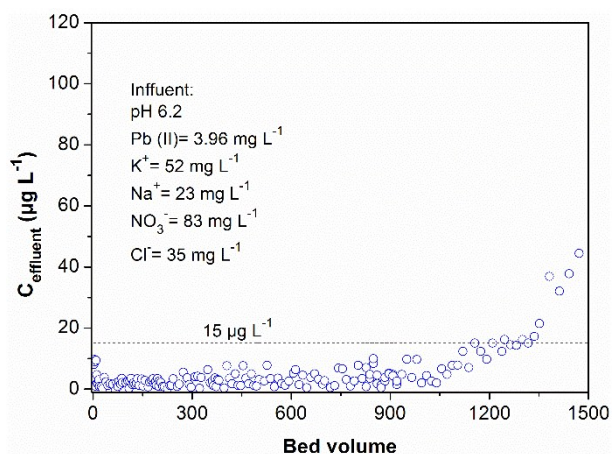


**Fig S8** The fittings of Langmuir model and Freundlich model for the adsorption of Pb (II) by GO (a),  $\text{Fe}_3\text{O}_4/\text{rGO}$  (b),  $\text{Fe}_3\text{S}_4/\text{rGO}-10\%$  (c),  $\text{Fe}_3\text{S}_4/\text{rGO}-20\%$  (d), and  $\text{Fe}_3\text{S}_4/\text{rGO}-30\%$  (e). The symbols are experimental data; the solid lines represent the fitted curves.

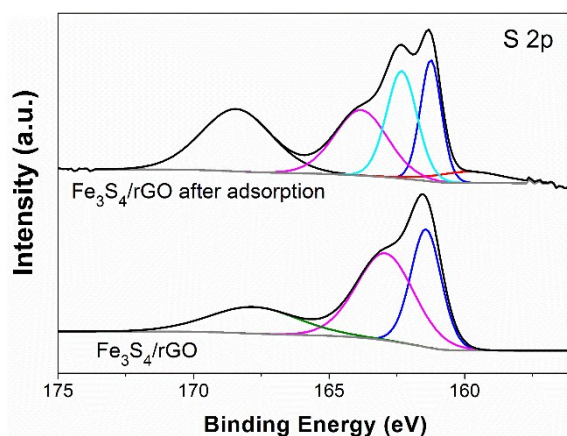


**Fig S9** Adsorption performance of GO,  $\text{Fe}_3\text{O}_4/\text{rGO}$ , and  $\text{Fe}_3\text{S}_4/\text{rGO}$  composites toward (a) Hg (II) and (b) Cd (II). Experimental conditions: initial concentration (60 mg L<sup>-1</sup> Hg (II), 50 mg L<sup>-1</sup> Cd (II)) 100 mL, sorbent 25 mg, pH 6, contact time 24 h, temperature 25 °C.





**Fig S10** Column adsorption of Pb (II) by  $\text{Fe}_3\text{S}_4/\text{rGO}$  from a synthetic Pb (II) feeding solution.



**Fig S11** XPS spectra of S 2p for  $\text{Fe}_3\text{S}_4/\text{rGO}$  before and after Pb (II) adsorption.

**Table S1** Element content of the  $\text{Fe}_3\text{S}_4/\text{rGO}$  sample from the XPS analysis.

Name	Pos.	FWHM	Area	At%	Wt%
C 1s	284.82	1.44	10231.13	50.87	29.80
Fe 2p	711.18	4.55	25750.38	12.03	32.76
S 2p	161.33	2.32	5236.89	10.84	10.84
O 1s	531.63	3.19	14818.42	26.26	26.26

**Table S2** Contents of the Fe<sub>3</sub>O<sub>4</sub>/rGO and Fe<sub>3</sub>S<sub>4</sub>/rGO samples from the TGA analysis.

Sample	Fe <sub>3</sub> O <sub>4</sub> (wt%)	Fe <sub>3</sub> S <sub>4</sub> (wt%)	rGO (wt%)
Fe <sub>3</sub> O <sub>4</sub> /rGO-10%	83.25	--	16.75
Fe <sub>3</sub> O <sub>4</sub> /rGO-20%	75.77	--	24.23
Fe <sub>3</sub> O <sub>4</sub> /rGO-30%	67.21	--	32.79
Fe <sub>3</sub> S <sub>4</sub> /rGO-10%	21.36	61.89	16.75
Fe <sub>3</sub> S <sub>4</sub> /rGO-20%	23.78	51.99	24.23
Fe <sub>3</sub> S <sub>4</sub> /rGO-30%	19.62	47.59	32.79

**Table S3** Adsorption isotherm parameters for Langmuir and Freundlich model of Pb (II) adsorption.

Adsorbent	Langmuir model			Freundlich model		
	Q <sub>m</sub> (mg g <sup>-1</sup> )	K <sub>L</sub> (L mg <sup>-1</sup> )	R <sup>2</sup>	K <sub>F</sub> (mg g <sup>-1</sup> )	n	R <sup>2</sup>
GO	163.93	0.036	0.984	26.16	3.33	0.849
Fe <sub>3</sub> O <sub>4</sub> /rGO	106.27	0.028	0.984	7.48	2.18	0.844
Fe <sub>3</sub> S <sub>4</sub> /rGO-10%	279.33	0.036	0.964	26.36	2.47	0.935
Fe <sub>3</sub> S <sub>4</sub> /rGO-20%	285.71	0.046	0.976	26.65	2.36	0.950
Fe <sub>3</sub> S <sub>4</sub> /rGO-30%	255.51	0.029	0.948	22.71	2.48	0.924

**Table S4** Comparison of Pb (II) adsorption capacities of various adsorbents

Adsorbent	Sorption capacity	Adsorption conditions	Refs
	( $Q_{\max}$ mg g <sup>-1</sup> )		
Graphene nanosheets	35.46	pH 4, 303K	5
Graphene oxide	152.71	pH 4.5, 298K	6
Fe <sub>3</sub> O <sub>4</sub>	52.94	pH 6, 298K	7
Amorphous Fe <sub>3</sub> O <sub>4</sub>	22.83	pH = 5 ± 0.2, 303K	8
Porous NiFe <sub>2</sub> O <sub>4</sub>	48.98	pH 5, 308K	9
Fe <sub>2</sub> O <sub>3</sub> -APTES-EDTA	100.20	room temperature (295-298K).	10
Fe <sub>3</sub> O <sub>4</sub> -SiO <sub>2</sub> -TETA	62.16	pH 7, room temperature	11
multiwall carbon nanotubes/Fe <sub>3</sub> O <sub>4</sub> (MWCNTs/ Fe <sub>3</sub> O <sub>4</sub> )	41.77	pH 5.3, 303K	12
MWCNTs/Fe <sub>3</sub> O <sub>4</sub> -NH <sub>2</sub>	75.02	pH 5.3, 303K	12
Iron oxides	5.60	pH 5.5, 293K	13
MWCNTs/iron oxides	9.85	pH 5.5, 293K	13
MWCNTs/iron oxides/cyclodextrin	12.29	pH 5.5, 293K	13
Thiol-functionalized magnetic mesoporous silica	91.50	pH 6.5, 298K	14
Graphene-Fe <sub>3</sub> O <sub>4</sub> composites	69.00	pH 5, 300K	15
Magnetic chitosan/graphene oxide composites	76.94	pH 5, 303K	16
Amino functionalized Fe <sub>3</sub> O <sub>4</sub> / graphenes composite	27.95	pH 6-7, room temperature	17
Layered Double Hydroxide Intercalated with MoS <sub>4</sub> <sup>2-</sup> Ions	288.90	pH 5.1, room temperature	18
Fe <sub>3</sub> S <sub>4</sub> hollow spheres	92.10	NA	19
Fe <sub>3</sub> S <sub>4</sub> /rGO-10%	279.33		
Fe <sub>3</sub> S <sub>4</sub> /rGO-20%	285.71	pH 6, 298K	This work
Fe <sub>3</sub> S <sub>4</sub> /rGO-30%	255.51		

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