SUPPLEMENTARY MATERIAL

Guanidinium ionic liquid-based surfactant as adequate solvent to separate and preconcentrate cadmium and copper in waters using *insitu* dispersive liquid–liquid microextraction

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Figure S1. Influence of (A) the NaCl concentration and (B) the pH of the aqueous sample on the extraction efficiency of copper with the *in-situ* DLLME-FAAS method using either $C_{16}C_4$ Im-Br or C_{10} Gu-Cl IL-based surfactants as extraction solvent. Fixed experimental conditions: 10 mL of ultrapure water spiked with 0.5 µg·L⁻¹ of copper; 10 g·L⁻¹ of NaCl in the study of the effect of the pH; 500 µL of acetone containing 200 mg·L⁻¹ of BSTC, 10 mmol·L⁻¹ of $C_{16}C_4$ Im-Br or 11 mmol·L⁻¹ of C_{10} Gu-Cl; pH of 7 in the study of the effect of the NaCl content; 60 µL and 65 µL of Li-NTf₂ at 0.5 g·mL⁻¹ for $C_{16}C_4$ Im-Br and C_{10} Gu-Cl, respectively, 2 min of vortex, 2 min of centrifugation at 1921×g; and dilution of the microdroplet up to 120 µL with acetonitrile. All experiments were carried out in triplicate.

Experiment	NaCl concentrat	ion (g·L ⁻¹)	рН			
	C ₁	\mathbf{X}_{1}	C ₂	X ₂		
1	0	25.0	0	5.75		
2	1.00	40.0	0	5.75		
3	0.500	32.5	0.866	8.50		
4	-1.00	10.0	0	5.75		
5	-0.500	17.5	-0.866	3.00		
6	0.500	32.5	-0.866	3.00		
7	-0.500	17.5	0.866	8.50		
8	-0.500	17.5	0	5.75		
9	0.500	32.5	0	5.75		

Table S1. Matrix of the Doehlert experimental design used for the optimization of the method with C_{10} Gu-Cl IL-based surfactant, including the coded and operating values.⁴⁵

 C_1 and C_2 are the coded values for the levels of NaCl concentration (g·L⁻¹) and pH, respectively.

$$C_{i} = \left[\frac{X_{i} - X_{i}^{0}}{\Delta X_{i}}\right] \alpha$$

The relationship between coded and real values is given by:

where C_i is the coded value for the level of factor i, X_i is its real value in an experiment, X^{o_i} is the real value at the center of the experimental domain, ΔX_i is the step of variation of the real value, and α is the coded value limit for each factor.

The number of experiments required (N) is given by $N = k^2 + k + C_0$, where k is the number of variables and C_0 is the number of center points.

Experiment	NaCl concentration (g·L ⁻¹)		Vortex time (min)
	C ₁	X ₁	C ₁	\mathbf{X}_{1}
1	0	25	0	2.25
2	1	40	0	2.25
3	0.5	32.5	0.866	4
4	-1	10	0	2.25
5	-0.5	17.5	-0.866	0.5
6	0.5	32.5	-0.866	0.5
7	-0.5	17.5	0.866	4
8	-0.5	17.5	0	2.25
9	0.5	32.5	0	2.25

Table S2. Matrix of the Doehlert experimental design used for the optimization of the method with $C_{16}C_4$ Im-Br IL-based surfactant, including the coded and operating values.⁴⁵

 C_1 and C_2 are the coded values for the levels of NaCl concentration (g·L⁻¹) and vortex time (min), respectively.

$$C_{i} = \left[\frac{X_{i} - X_{i}^{0}}{\Delta X_{i}}\right] \alpha$$

The relationship between coded and real values is given by:

where C_i is the coded value for the level of factor i, X_i is its real value in an experiment, X^{o_i} is the real value at the center of the experimental domain, ΔX_i is the step of variation of the real value, and α is the coded value limit for each factor.

The number of experiments required (N) is given by $N = k^2 + k + C_0$, where k is the number of variables and C_0 is the number of center points.

Table S3. Reproducibility of the entire *in-situ* DLLME-FAAS method evaluated as the ratio between the slopes corresponding to calibration curves obtained in different non-consecutive days.

Calibration curve	Slope $\pm t_{n-2} \cdot SD^*$	Dataset	Slopes ratio			
Cu ²⁺ determination using C ₁₀ Gu-Cl						
day 1	4.2 ± 0.3	test 1 – 2	0.89			
day 2	4.7 ± 0.2	test 1 – 3	1.04			
day 3	4.0 ± 0.2	test 2 - 3	1.16			
Cu ²⁺ determination using C ₁₆ C ₄ Im-Br						
day 1	7.00 ± 0.05	test 1 – 2	1.09			
day 2	6.4 ± 0.2	test 1 – 3	1.06			
day 3	6.6 ± 0.2	test 2 - 3	0.97			
Cd ²⁺ determination using C ₁₀ Gu-Cl						
day 1	9.8 ± 0.4	test 1 – 2	1.04			
day 2	9.4 ± 0.5	test 1 – 3	0.96			
day 3	10.2 ± 0.4	test 2 - 3	0.92			

* Confidence interval of the slope for n = 7 calibration levels

Table S4. Comparison of several parameters of the analytical performance of the developed *in-situ* DLLME method and other *in-situ* DLLME methods reported in the literature for the determination of Cu^{2+} or Cd^{2+} in water samples.

Metal	Sample (mL)	Complexing	IL	Anion-	μL of the final extract	Detection	LOD ^a	E_{F}^{b}	Ref.
		agent	(concentration)	exchange	(diluted or not) / µL		(µg·L ⁻¹)		
				reagent	subjected to AAS				
Cu ²⁺	tap water (10 mL)	BSTC ^c	C ₁₀ Gu-Cl	Li-NTf ₂	120 / 50	FAAS ^d	0.3	77	this
			$(11 \text{ mmol} \cdot \text{L}^{-1})$						work
Cu^{2+}	tap water and wastewater	DDTC ^e	C ₁₆ C ₄ Im-Br	Li-NTf ₂	270 / 50	FAAS ^d	5.1	36	[25]
	(10 mL)		$(25.2 \text{ mmol} \cdot \text{L}^{-1})$						
Cu^{2+}	aqueous extract from soil	DDTC ^e	C ₆ MIm-Cl	Li-NTf ₂	48 / 10	ETAAS ^f	0.004	200	[26]
	and sediments (10 mL)		$(\sim 10 \text{ mmol} \cdot \text{L}^{-1})$						
Cd^{2+}	tap water (10 mL)	BSTC ^c	C ₁₀ Gu-Cl	Li-NTf ₂	120 / 50	FAAS ^d	0.5	70	this
			(11 mmol·L ⁻¹)						work
Cd^{2+}	seawater, spring and river	DDTP ^g	C ₆ MIm-BF ₄	Na-PF ₆	58 / 58	FAAS ^d	0.07	78	[27]
	water (5 mL)		(~24 mmol·L ⁻¹)						
Cd^{2+}	tap water, bottled water	APDC ^h	C ₈ MIm-Cl	Li-NTf ₂	30 / 30	ETAAS ^f	0.0002	280	[28]
	and seawater (10 mL)		$(10 \text{ mmol} \cdot \text{L}^{-1})$						

^a limit of detection

^b enrichment factor

^c N,N'-bis(salicylidene)thiocarbohydrazide

^d flame atomic absorption spectroscopy

^e diethyl dithiocarbamate

^f electrothermal atomic absorption spectroscopy

^g O,O-diethyldithiophosphate

^h ammonium pyrrolidine dithiocarbamate