

## Supplementary Information

### A high-throughput method for the element determination in green coffee bean using diluted nitric acid and ultrasound energy

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**Table S1.** Summary of the obtained models for the experimental design of all analytes.

Analyte	Parameter	Estimate	Std. Error	t value	Pr(> t )
Ba	(Intercept)	0.316	0.111	2.858	0.008**
	A	-0.027	0.068	-0.394	0.696
	B	0.425	0.068	6.278	0.000***
	A <sup>2</sup>	0.091	0.081	1.130	0.268
	B <sup>2</sup>	-0.619	0.081	-7.672	0.000***
	A:B	-0.144	0.096	-1.502	0.145
	Residual standard error: 0.3319 on 27 degrees of freedom, Multiple R <sup>2</sup> : 0.8075, Adjusted R <sup>2</sup> : 0.7718, F-statistic: 22.65 on 5 and 27 DF, p-value: 6.943e-09				
Ca	(Intercept)	0.132	0.083	1.596	0.122
	A	0.038	0.051	0.755	0.457
	B	0.208	0.051	4.119	0.000***
	A <sup>2</sup>	0.030	0.060	0.490	0.628
	B <sup>2</sup>	-0.502	0.060	-8.335	0.000***
	A:B	-0.154	0.072	-2.151	0.041*
	Residual standard error: 0.2479 on 27 degrees of freedom, Multiple R <sup>2</sup> : 0.7892, Adjusted R <sup>2</sup> : 0.7502, F-statistic: 20.22 on 5 and 27 DF, p-value: 2.283e-08				
Cu	(Intercept)	1.449	0.121	11.961	0.000***
	A	0.169	0.074	2.283	0.031*
	B	0.552	0.074	7.445	0.000***
	A <sup>2</sup>	-0.069	0.088	-0.784	0.440
	B <sup>2</sup>	-1.190	0.088	-13.476	0.000***
	A:B	-0.108	0.105	-1.025	0.314
	Residual standard error: 0.3634 on 27 degrees of freedom, Multiple R <sup>2</sup> : 0.904, Adjusted R <sup>2</sup> : 0.8863, F-statistic: 50.87 on 5 and 27 DF, p-value: 6.716e-13				
Fe	(Intercept)	0.881	0.101	8.711	0.000***
	A	0.077	0.062	1.236	0.227
	B	0.856	0.062	13.824	0.000***
	A <sup>2</sup>	-0.331	0.074	-4.486	0.000***
	B <sup>2</sup>	-0.803	0.074	-10.891	0.000***
	A:B	0.413	0.088	4.712	0.000***
	Residual standard error: 0.3034 on 27 degrees of freedom, Multiple R <sup>2</sup> : 0.9255, Adjusted R <sup>2</sup> : 0.9117, F-statistic: 67.05 on 5 and 27 DF, p-value: 2.287e-14				
K	(Intercept)	1.226	0.106	11.540	0.000***
	A	0.179	0.065	2.747	0.011*
	B	0.169	0.065	2.590	0.015*
	A <sup>2</sup>	-0.072	0.077	-0.927	0.362
	B <sup>2</sup>	-0.862	0.077	-11.133	0.000***
	A:B	-0.162	0.092	-1.758	0.090
	Residual standard error: 0.3188 on 27 degrees of freedom, Multiple R <sup>2</sup> : 0.8451,				

	Adjusted R <sup>2</sup> : 0.8164, F-statistic: 29.46 on 5 and 27 DF, p-value: 3.919e-10				
Mg	(Intercept)	0.503	0.117	4.309	0.000***
	A	0.141	0.071	1.974	0.059
	B	0.150	0.071	2.103	0.045*
	A <sup>2</sup>	0.063	0.085	0.736	0.468
	B <sup>2</sup>	-0.636	0.085	-7.483	0.000***
	A:B	-0.128	0.101	-1.265	0.217
Residual standard error: 0.3501 on 27 degrees of freedom, Multiple R <sup>2</sup> : 0.7362, Adjusted R <sup>2</sup> : 0.6874, F-statistic: 15.07 on 5 and 27 DF, p-value: 4.296e-07					
Mn	(Intercept)	-0.121	0.102	-1.186	0.246
	A	0.047	0.062	0.758	0.455
	B	0.100	0.062	1.607	0.120
	A <sup>2</sup>	0.081	0.074	1.088	0.286
	B <sup>2</sup>	-0.353	0.074	-4.745	0.000***
	A:B	-0.081	0.088	-0.921	0.365
Residual standard error: 0.3058 on 27 degrees of freedom, Multiple R <sup>2</sup> : 0.5521, Adjusted R <sup>2</sup> : 0.4691, F-statistic: 6.656 on 5 and 27 DF, p-value: 0.0003712					
P	(Intercept)	0.581	0.172	3.382	0.002**
	A	-0.117	0.105	-1.113	0.275
	B	0.722	0.105	6.863	0.000***
	A <sup>2</sup>	-0.107	0.125	-0.856	0.400
	B <sup>2</sup>	-0.661	0.125	-5.273	0.000***
	A:B	0.364	0.149	2.445	0.021*
Residual standard error: 0.5156 on 27 degrees of freedom, Multiple R <sup>2</sup> : 0.7538, Adjusted R <sup>2</sup> : 0.7082, F-statistic: 16.53 on 5 and 27 DF, p-value: 1.75e-07					
Sr	(Intercept)	0.266	0.104	2.562	0.016*
	A	-0.005	0.063	-0.081	0.936
	B	0.405	0.063	6.379	0.000***
	A <sup>2</sup>	0.090	0.076	1.188	0.245
	B <sup>2</sup>	-0.622	0.076	-8.231	0.000***
	A:B	-0.112	0.090	-1.246	0.223
Residual standard error: 0.311 on 27 degrees of freedom, Multiple R <sup>2</sup> : 0.8215, Adjusted R <sup>2</sup> : 0.7884, F-statistic: 24.85 on 5 and 27 DF, p-value: 2.56e-09					
Zn	(Intercept)	0.989	0.197	5.028	0.000***
	A	-0.082	0.120	-0.678	0.503
	B	0.266	0.120	2.206	0.036*
	A <sup>2</sup>	-0.559	0.143	-3.902	0.001***
	B <sup>2</sup>	-0.803	0.143	-5.603	0.000***
	A:B	-0.363	0.170	-2.129	0.043*
Residual standard error: 0.5902 on 27 degrees of freedom, Multiple R <sup>2</sup> : 0.6342, Adjusted R <sup>2</sup> : 0.5664, F-statistic: 9.362 on 5 and 27 DF, p-value: 2.899e-05					

Significance codes: 0 '\*\*\*' 0.001 '\*\*' 0.01 '\*' ; A (time in minutes); B ( $\text{HNO}_3$

concentration in mol/L); DF (degrees of freedom)

**Table S2.** The total concentration of elements, in  $\mu\text{g g}^{-1}$ , in various coffee bean samples determined by ICP-OES after UAE (results expressed as a mean  $\pm$  interval with 95% of confidence level).

Sample	Ba	Ca	Cu	Fe	K	Mg	Mn	Sr	P	Zn
A-MG14	$2.3 \pm 1.6$	$2387 \pm 1418$	$27 \pm 18$	$28 \pm 3$	$55741 \pm 33555$	$3216 \pm 1664$	$33.7 \pm 16.0$	$5.8 \pm 3.6$	$1614 \pm 561$	$6 \pm 1$
C20-15-MG16	$1.1 \pm 0.1$	$1785 \pm 107$	$16 \pm 1$	$27 \pm 3$	$32513 \pm 1796$	$2260 \pm 111$	$28.0 \pm 1.6$	$2.9 \pm 0.1$	$1181 \pm 113$	$12 \pm 1$
C24-137-MG16	$0.2 \pm 0.1$	$1548 \pm 224$	$13 \pm 3$	$24 \pm 1$	$34944 \pm 4705$	$2661 \pm 371$	$32.7 \pm 4.1$	$2.0 \pm 0.3$	$1453 \pm 148$	$6 \pm 1$
C2-SL-MG14	$1.8 \pm 0.2$	$2209 \pm 210$	$19 \pm 3$	$29 \pm 3$	$38943 \pm 6118$	$2762 \pm 636$	$30.8 \pm 6.8$	$3.4 \pm 0.4$	$1581 \pm 414$	$8 \pm 1$
C36-6-MG16	$0.8 \pm 0.1$	$1817 \pm 104$	$18 \pm 1$	$25 \pm 2$	$36341 \pm 1467$	$2355 \pm 176$	$37.9 \pm 2.4$	$2.9 \pm 0.1$	$1451 \pm 208$	$6 \pm 1$
CA-ES15	$1.5 \pm 0.2$	$2387 \pm 173$	$13 \pm 1$	$27 \pm 1$	$35809 \pm 5763$	$2769 \pm 167$	$50.2 \pm 3.5$	$5.2 \pm 0.5$	$1817 \pm 217$	$5 \pm 1$
CA-ES16	$0.3 \pm 0.1$	$1589 \pm 95$	$11 \pm 1$	$28 \pm 2$	$30771 \pm 1553$	$2149 \pm 99$	$27.2 \pm 1.6$	$4.0 \pm 0.2$	$1328 \pm 122$	$6 \pm 1$
CA-MG14	<LOD	$1784 \pm 244$	$10 \pm 1$	$23 \pm 4$	$36617 \pm 4255$	$2854 \pm 240$	$12.1 \pm 0.9$	$1.0 \pm 0.2$	$1413 \pm 242$	$5 \pm 1$
CA-SP14	$3.6 \pm 0.9$	$1808 \pm 417$	$15 \pm 4$	$25 \pm 2$	$40825 \pm 9012$	$2419 \pm 478$	$55.2 \pm 12.4$	$5.6 \pm 1.3$	$1495 \pm 350$	$6 \pm 1$
CR-MG-16	$1.0 \pm 0.3$	$1615 \pm 302$	$15 \pm 4$	$27 \pm 1$	$35238 \pm 7044$	$2424 \pm 475$	$33.8 \pm 6.8$	$2.8 \pm 0.6$	$1520 \pm 228$	$6 \pm 1$
CV-MG14	<LOD	$1894 \pm 227$	$11 \pm 2$	$24 \pm 2$	$38254 \pm 4337$	$3327 \pm 394$	$16.6 \pm 3.0$	$1.1 \pm 0.2$	$2429 \pm 643$	$5 \pm 1$
IAC-144-MG14	$4.1 \pm 0.9$	$2379 \pm 455$	$19 \pm 4$	$24 \pm 4$	$43396 \pm 7630$	$3016 \pm 546$	$54.3 \pm 10.3$	$6.4 \pm 1.3$	$1740 \pm 253$	$7 \pm 2$
IAC-144-SP14	$2.7 \pm 0.3$	$1841 \pm 160$	$16 \pm 2$	$26 \pm 2$	$32942 \pm 2638$	$2424 \pm 416$	$26.5 \pm 4.9$	$6.3 \pm 0.5$	$1700 \pm 462$	$5 \pm 1$
IAC-44-ES12	$1.2 \pm 0.3$	$2067 \pm 449$	$30 \pm 6$	$32 \pm 2$	$45585 \pm 9714$	$2717 \pm 214$	$26.2 \pm 2.2$	$5.2 \pm 1.0$	$1665 \pm 317$	$7 \pm 2$
IAC-44-ES13	$1.3 \pm 0.4$	$2145 \pm 355$	$23 \pm 7$	$22 \pm 2$	$44818 \pm 11224$	$2421 \pm 124$	$20.4 \pm 1.6$	$5.4 \pm 1.2$	$1434 \pm 416$	$4 \pm 1$
IAC-44-ES14	$1.1 \pm 0.2$	$1867 \pm 191$	$21 \pm 2$	$26 \pm 2$	$38585 \pm 1843$	$2998 \pm 201$	$29.8 \pm 2.0$	$4.8 \pm 0.5$	$2061 \pm 347$	$5 \pm 1$
IAC-44-ES16	$1.0 \pm 0.1$	$1752 \pm 149$	$19 \pm 2$	$29 \pm 3$	$41843 \pm 2526$	$3163 \pm 212$	$21.4 \pm 1.7$	$3.3 \pm 0.3$	$2766 \pm 106$	$10 \pm 2$
IAC-62-SP14	$4.3 \pm 0.7$	$1943 \pm 314$	$15 \pm 2$	$29 \pm 6$	$36042 \pm 4557$	$2452 \pm 257$	$148.8 \pm 19.9$	$6.8 \pm 1.1$	$1597 \pm 169$	$6 \pm 1$
IP59-ES12	<LOD	$1853 \pm 582$	$13 \pm 5$	$26 \pm 2$	$33682 \pm 11120$	$2841 \pm 965$	$28.9 \pm 9.7$	$2.7 \pm 1.0$	$2097 \pm 768$	$9 \pm 1$
IP59-ES13	$0.6 \pm 0.1$	$1759 \pm 198$	$14 \pm 2$	$35 \pm 4$	$36346 \pm 3168$	$2970 \pm 262$	$35.8 \pm 3.5$	$2.7 \pm 0.3$	$1977 \pm 470$	$4 \pm 1$
IP59-ES14	<LOD	$1924 \pm 117$	$12 \pm 1$	$32 \pm 2$	$38281 \pm 4978$	$2813 \pm 568$	$26.9 \pm 5.1$	$2.4 \pm 0.2$	$1611 \pm 318$	$5 \pm 1$
IP59-ES15	$0.5 \pm 0.2$	$1952 \pm 629$	$14 \pm 4$	$28 \pm 3$	$38263 \pm 7246$	$2463 \pm 331$	$23.4 \pm 5.2$	$3.9 \pm 0.9$	$1792 \pm 932$	$6 \pm 1$
IP59-ES16a	$0.5 \pm 0.2$	$1795 \pm 277$	$5 \pm 1$	$31 \pm 2$	$33385 \pm 5020$	$2508 \pm 397$	$32.0 \pm 5.4$	$6.0 \pm 1.0$	$1506 \pm 279$	$5 \pm 1$
IP59-ES16b	<LOD	$1784 \pm 185$	$15 \pm 2$	$38 \pm 5$	$35325 \pm 2948$	$2482 \pm 338$	$22.5 \pm 3.5$	$2.8 \pm 0.3$	$1548 \pm 370$	$4 \pm 1$

MN-376-4-MG14	$2.0 \pm 0.4$	$2391 \pm 448$	$23 \pm 4$	$30 \pm 3$	$46646 \pm 7799$	$2848 \pm 367$	$20.3 \pm 2.1$	$5.2 \pm 0.9$	$1506 \pm 313$	$7 \pm 1$
MN-376-4-MG16	$4.3 \pm 1.7$	$2110 \pm 739$	$17 \pm 6$	$30 \pm 2$	$37476 \pm 14041$	$2376 \pm 667$	$28.2 \pm 8.8$	$4.7 \pm 0.2$	$1105 \pm 371$	$6 \pm 1$
MN-474-19-MG14	$2.7 \pm 0.4$	$2576 \pm 452$	$23 \pm 6$	$44 \pm 3$	$48181 \pm 6973$	$2695 \pm 506$	$29.2 \pm 4.8$	$7.6 \pm 0.8$	$1344 \pm 481$	$6 \pm 1$
MN-474-19-MG16	$1.7 \pm 0.5$	$2256 \pm 448$	$21 \pm 4$	$32 \pm 3$	$41990 \pm 7278$	$3132 \pm 648$	$45.6 \pm 7.9$	$3.7 \pm 0.9$	$1954 \pm 602$	$5 \pm 1$
MN-479-19-MG16	$1.4 \pm 0.2$	$1832 \pm 117$	$20 \pm 1$	$27 \pm 2$	$43416 \pm 2581$	$3172 \pm 226$	$32.6 \pm 2.1$	$3.0 \pm 0.2$	$2082 \pm 226$	$6 \pm 1$