

Supplementary materials

Table 1SM. Unit cell parameters and thermal expansion coefficients of the low-temperature modification of $(\text{NH}_4)_3\text{Sc}(\text{SO}_4)_3$ upon temperature

| T, °C | a, Å | b, Å | c, Å | β , ° | V, Å ³ | V/Z, Å ³ | $\alpha_a, \times 10^{-6} \text{ } ^\circ\text{C}^{-1}$ | $\alpha_b, \times 10^{-6} \text{ } ^\circ\text{C}^{-1}$ | $\alpha_c, \times 10^{-6} \text{ } ^\circ\text{C}^{-1}$ | $\alpha_V, \times 10^{-6} \text{ } ^\circ\text{C}^{-1}$ |
|------------|---------|----------|---------|-------------|-------------------|---------------------|---|---|---|---|
| 25 | 9.0524(| 15.4622(| 9.2165(| 108.43(| 1223.9(| 305.97(2) | | | | |
| 40 | 9.0608(| 15.4628(| 9.2198(| 108.41(| 1225.6(| 306.41(2) | 61.7 | 2.58 | 23.9 | 94.0 |
| 50 | 9.0683(| 15.4643(| 9.2208(| 108.42(| 1226.8(| 306.71(2) | 82.7 | 9.69 | 10.8 | 98.7 |
| 60 | 9.0748(| 15.4662(| 9.2226(| 108.41(| 1228.1(| 307.04(2) | 71.6 | 12.3 | 19.5 | 10.7 |
| 70 | 9.0814(| 15.4664(| 9.2238(| 108.41(| 1229.3(| 307.31(2) | 72.6 | 1.29 | 13.0 | 89.9 |
| 80 | 9.0878(| 15.4685(| 9.2248(| 108.41(| 1230.4(| 307.60(2) | 70.4 | 13.6 | 10.8 | 91.8 |
| 90 | 9.0918(| 15.4663(| 9.2268(| 108.41(| 1231.0(| 307.75(2) | 44.0 | -14.2 | 21.7 | 51.1 |
| 100 | 9.0922(| 15.4643(| 9.2284(| 108.41(| 1231.2(| 307.79(2) | 4.71 | -12.9 | 17.5 | 11.6 |
| Mea | | | | | | | 58.2 | 1.75 | 16.8 | 77.7 |

$$\alpha_a = \frac{1}{a} \left(\frac{\partial L}{\partial R} \right), \alpha_b = \frac{1}{b} \left(\frac{\partial L}{\partial R} \right), \alpha_c = \frac{1}{c} \left(\frac{\partial L}{\partial R} \right), \alpha_V = \frac{1}{V} \left(\frac{\partial L}{\partial R} \right)$$

Table 2SM. Unit cell parameters and thermal expansion coefficients of the high-temperature modification of $(\text{NH}_4)_3\text{Sc}(\text{SO}_4)_3$ upon temperature

| T, °C | a, Å | c, Å | V, Å ³ | V/Z, Å ³ | $\alpha_a, \times 10^{-6} \text{ } ^\circ\text{C}^{-1}$ | $\alpha_c, \times 10^{-6} \text{ } ^\circ\text{C}^{-1}$ | $\alpha_V, \times 10^{-6} \text{ } ^\circ\text{C}^{-1}$ |
|-------------|------------|-----------|-------------------|---------------------|---|---|---|
| 80 | 15.4278(4) | 9.2190(2) | 1900.3(1) | 316.72(2) | | | |
| 90 | 15.4309(4) | 9.2203(2) | 1901.3(1) | 316.89(2) | 20.1 | 14.1 | 53.6 |
| 100 | 15.4329(4) | 9.2228(2) | 1902.4(1) | 317.06(2) | 13.0 | 27.1 | 53.6 |
| 110 | 15.4350(4) | 9.2251(2) | 1903.3(1) | 317.22(2) | 13.6 | 24.9 | 52.0 |
| 120 | 15.4391(4) | 9.2262(2) | 1904.6(1) | 317.43(2) | 26.6 | 11.9 | 65.2 |
| 140 | 15.4435(3) | 9.2305(2) | 1906.6(1) | 317.76(2) | 14.2 | 23.3 | 51.9 |
| 150 | 15.4457(4) | 9.2327(2) | 1907.5(1) | 317.92(2) | 14.2 | 23.8 | 51.4 |
| 160 | 15.4495(4) | 9.2342(2) | 1908.8(1) | 318.13(2) | 24.6 | 16.2 | 65.5 |
| 180 | 15.4552(4) | 9.2382(2) | 1911.0(1) | 318.50(2) | 18.4 | 21.6 | 58.3 |
| 200 | 15.4618(4) | 9.2410(2) | 1913.3(1) | 318.88(2) | 21.3 | 15.1 | 58.3 |
| 220 | 15.4672(4) | 9.2441(2) | 1915.2(1) | 319.20(2) | 17.5 | 16.8 | 51.4 |
| 240 | 15.4743(4) | 9.2469(2) | 1917.6(1) | 319.59(2) | 22.9 | 15.1 | 61.0 |
| 260 | 15.4801(4) | 9.2491(2) | 1919.5(1) | 319.91(2) | 18.7 | 11.9 | 49.2 |
| 280 | 15.4873(4) | 9.2525(2) | 1921.9(1) | 320.32(2) | 23.2 | 18.4 | 64.8 |
| Mean | | | | | 19.1 | 18.5 | 56.6 |

$$\alpha_a = \frac{1}{a} \left(\frac{\partial L}{\partial R} \right), \alpha_b = \frac{1}{b} \left(\frac{\partial L}{\partial R} \right), \alpha_c = \frac{1}{c} \left(\frac{\partial L}{\partial R} \right), \alpha_V = \frac{1}{V} \left(\frac{\partial L}{\partial R} \right)$$

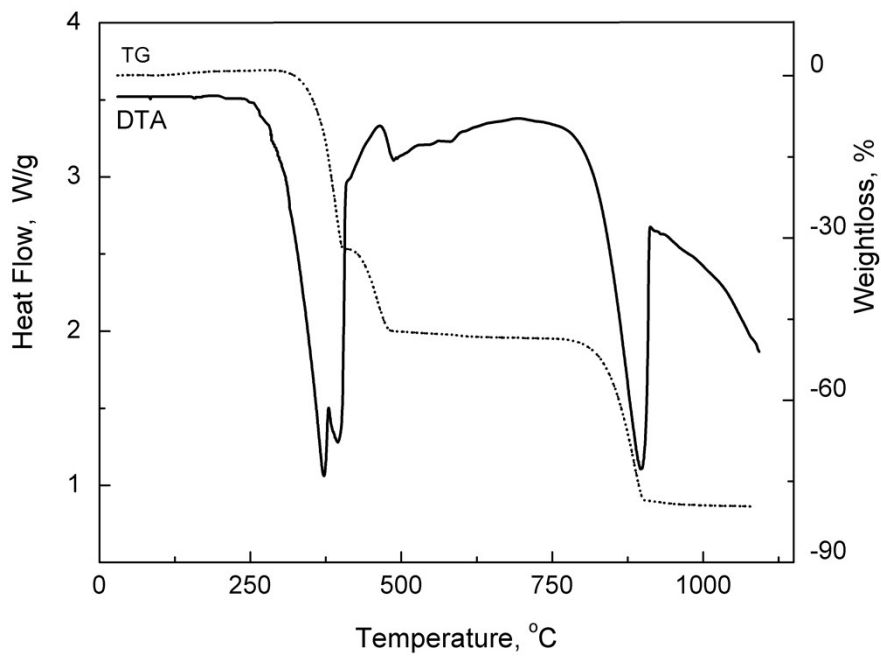


Fig. 1SM. TG and DTA curves of $(\text{NH}_4)_3\text{Sc}(\text{SO}_4)_3$ at a heating rate of $10^\circ/\text{min}$ in air

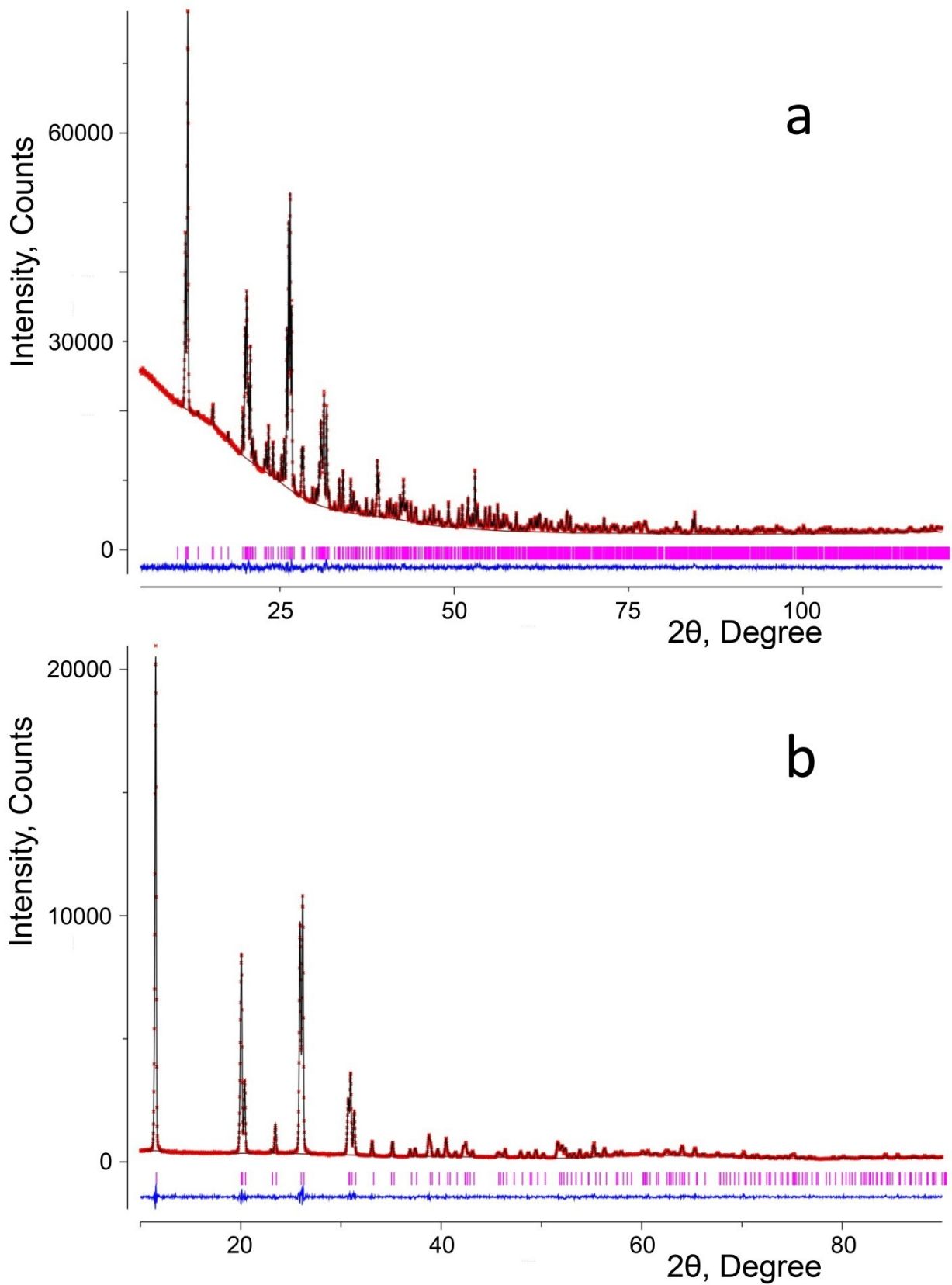


Fig. 4 Experimental (crosses), calculated (solid line), and difference (bottom line) XRPD patterns of the low-temperature (a) and high-temperature modifications (b) of $(\text{NH}_4)_3\text{Sc}(\text{SO}_4)_3$. Series of tick marks correspond to the Bragg reflection.