# A remarkable two-dimensional membrane for multifunctional gas separation: halogenated metal-free fused-ring polyphthalocyanine

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**Section S1**. Table S1: Force field (FF) parameters adopted in classical molecular dynamics (MD) simulations.

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Section S3. The derivations of mechanical properties under infinitesimal strain theory and finite strain theory and Fig. S7: the second Piola–Kirchhoff (PK2) stress versus Lagrangian strain under uniaxial tension (*x*-direction) and under biaxial tension for pristine, F- and Cl-H<sub>2</sub>PPc.

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Section S6. Fig. S8–S9: Sketch of the minimum energy path for  $H_2$ , CO, CH<sub>4</sub>, CO<sub>2</sub> and N<sub>2</sub> passing through F- and Cl-H<sub>2</sub>PPc.

Section S7. Fig. S10: Pore areas of pore-I in F- and Cl-H<sub>2</sub>PPc.

	$\varepsilon$ (kcal/mol)	$\sigma$ (Å)
С	0.148	3.617
N	0.167	3.501
F	0.069	3.081
Н	0.038	2.450

Table S1 FF parameters of  $F-H_2PPc$  adopted in classical MD simulations.



**Fig. S1** (a) Top view and (b) side view of  $H_2PPc$  after 10 ps first-principles MD simulation at 300 K, and (c) temperature and (d) energy during the simulation. Grey, blue, and white balls stand for C, N, and H atoms.



**Fig. S2** (a) Top view and (b) side view of F-H<sub>2</sub>PPc after 10 ps first-principles MD simulation at 300 K, and (c) temperature and (d) energy during the simulation. Grey, blue, white, and cyan balls stand for C, N, H, and F atoms.



**Fig. S3** (a) Top view and (b) side view of  $Cl-H_2PPc$  after 10 ps first-principles MD simulation at 300 K, and (c) temperature and (d) energy during the simulation. Grey, blue, white and green balls stand for C, N, H and Cl atoms.



**Fig. S4** (a) Top view and (b) side view of  $H_2PPc$  after 10 ps first-principles MD simulation at 500 K, and (c) temperature and (d) energy during the simulation. Grey, blue, and white balls stand for C, N, and H atoms.



**Fig. S5** (a) Top view and (b) side view of F-H<sub>2</sub>PPc after 10 ps first-principles MD simulation at 500 K, and (c) temperature and (d) energy during the simulation. Grey, blue, white, and cyan balls stand for C, N, H, and F atoms.



**Fig. S6** (a) Top view and (b) side view of  $Cl-H_2PPc$  after 10 ps first-principles MD simulation at 500 K, and (c) temperature and (d) energy during the simulation. Grey, blue, white and green balls stand for C, N, H and Cl atoms.

The involved structures all belong to the tetragonal crystal family of which only one in-plane Young's modulus as well as one Poisson's ratio along the *x*-direction (equivalent to *y*-direction) needs to be determined. In addition, the strength of studied membranes under uniaxial and biaxial tension is another important mechanical property that we expect to know.

# 1. The in-plane Young's modulus and Poisson's ratio under infinitesimal strain theory

For the in-plane Young's modulus (*Y*) and Poisson's ratio ( $\mu$ ) calculations, we adopted the linear approximation of stress–strain relationship under infinitesimal strain of 0–0.05.<sup>1,2</sup> As a result, the Hooke's law in three-dimensional materials is

$$\begin{pmatrix} \sigma_1 \\ \sigma_2 \\ \sigma_3 \\ \sigma_4 \\ \sigma_5 \\ \sigma_6 \end{pmatrix} = \begin{pmatrix} \mathcal{C}_{11} & \mathcal{C}_{12} & \mathcal{C}_{13} & \mathcal{C}_{14} & \mathcal{C}_{15} & \mathcal{C}_{16} \\ \mathcal{C}_{12} & \mathcal{C}_{22} & \mathcal{C}_{23} & \mathcal{C}_{24} & \mathcal{C}_{25} & \mathcal{C}_{26} \\ \mathcal{C}_{13} & \mathcal{C}_{23} & \mathcal{C}_{33} & \mathcal{C}_{34} & \mathcal{C}_{35} & \mathcal{C}_{36} \\ \mathcal{C}_{14} & \mathcal{C}_{24} & \mathcal{C}_{34} & \mathcal{C}_{44} & \mathcal{C}_{45} & \mathcal{C}_{46} \\ \mathcal{C}_{15} & \mathcal{C}_{25} & \mathcal{C}_{35} & \mathcal{C}_{45} & \mathcal{C}_{55} & \mathcal{C}_{56} \\ \mathcal{C}_{16} & \mathcal{C}_{26} & \mathcal{C}_{36} & \mathcal{C}_{46} & \mathcal{C}_{56} & \mathcal{C}_{66} \end{pmatrix} \begin{pmatrix} \varepsilon_1 \\ \varepsilon_2 \\ \varepsilon_3 \\ \varepsilon_4 \\ \varepsilon_5 \\ \varepsilon_6 \end{pmatrix}$$
(1)

in which the column matrices of stress and strain with Voigt notation<sup>3</sup> represent the stress and strain tensor respectively:

$$\sigma = \begin{pmatrix} \sigma_{1} & \sigma_{6} & \sigma_{5} \\ \sigma_{6} & \sigma_{2} & \sigma_{4} \\ \sigma_{5} & \sigma_{4} & \sigma_{3} \end{pmatrix} = \begin{pmatrix} \sigma_{xx} & \sigma_{xy} & \sigma_{xz} \\ \sigma_{xy} & \sigma_{yy} & \sigma_{yz} \\ \sigma_{xz} & \sigma_{yz} & \sigma_{zz} \end{pmatrix}$$
(2)
$$\varepsilon = \begin{pmatrix} \varepsilon_{1} & \frac{1}{2}\varepsilon_{6} & \frac{1}{2}\varepsilon_{5} \\ \frac{1}{2}\varepsilon_{6} & \varepsilon_{2} & \frac{1}{2}\varepsilon_{4} \\ \frac{1}{2}\varepsilon_{5} & \frac{1}{2}\varepsilon_{4} & \varepsilon_{3} \end{pmatrix} = \begin{pmatrix} \varepsilon_{xx} & \frac{1}{2}\gamma_{xy} & \frac{1}{2}\gamma_{xz} \\ \frac{1}{2}\gamma_{xy} & \varepsilon_{yy} & \frac{1}{2}\gamma_{yz} \\ \frac{1}{2}\gamma_{xz} & \frac{1}{2}\gamma_{yz} & \varepsilon_{zz} \end{pmatrix}$$
(3)

where  $\sigma_{ij}$  indicates that stress with *j*-direction orientation acts on the plane with an

external normal direction of *i*,  $\varepsilon_{ii}$  means normal strain along the axis of *i* and  $\gamma_{ij}$  stands for shear strain between axes of *i* and *j*. The  $C_{ij}$  matrix represents the elastic stiffness constant with twenty-one independent elements at most.<sup>3</sup> The tetragonal crystal system with symmetry of  $D_{4h}$  possesses six independent matrix elements as:<sup>3</sup>

$$\begin{pmatrix}
C_{11} & C_{12} & C_{13} & 0 & 0 & 0 \\
& C_{11} & C_{13} & 0 & 0 & 0 \\
& & C_{33} & 0 & 0 & 0 \\
& & & C_{44} & 0 & 0 \\
& & & & C_{44} & 0 \\
& & & & & C_{66}
\end{pmatrix}$$
(4)

so we get a simple form by applying 3D Hooke's law in two-dimensional studied monolayers:

$$\begin{cases} \sigma_1 = \mathcal{C}_{11}\varepsilon_1 + \mathcal{C}_{12}\varepsilon_2\\ \sigma_2 = \mathcal{C}_{12}\varepsilon_1 + \mathcal{C}_{11}\varepsilon_2 \end{cases}$$
(5)

According to the superposition principle under infinitesimal strain approximation:

$$\begin{cases} \varepsilon_1 = \frac{1}{Y}(\sigma_1 - \mu \sigma_2) \\ \varepsilon_2 = \frac{1}{Y}(\sigma_2 - \mu \sigma_1) \end{cases}$$
(6)

from which we derived:

$$\begin{cases} \sigma_1 = \frac{Y}{1 - \mu^2} (\varepsilon_1 + \mu \varepsilon_2) \\ \sigma_2 = \frac{Y}{1 - \mu^2} (\mu \varepsilon_1 + \varepsilon_2) \end{cases}$$
(7)

So we easily obtained the in-plane Young's modulus and the Poisson's ratio as:

$$\begin{cases} Y = C_{11} - \frac{C_{12}^2}{C_{11}} \\ \mu = \frac{C_{12}}{C_{11}} \end{cases}$$
(8)

Thus, two matrix elements of  $C_{11}$  and  $C_{12}$  should be known to calculate Y and  $\mu$ . The density of structures' total energy difference can be expressed as Taylor series expansion under the infinitesimal strain approximation:

$$\frac{\Delta E}{V} = \frac{1}{2}C_{11}\varepsilon_1^2 + \frac{1}{2}C_{11}\varepsilon_2^2 + C_{12}\varepsilon_1\varepsilon_2$$
(9)

That is to say, let  $\varepsilon_1$  and  $\varepsilon_2$  vary from 0 to 0.03 by an increment of 0.005, we could get the value of  $C_{11}$  and  $C_{12}$  by fitting data of the density of total energy difference versus strain. Note that, the transformation of lattice vectors from R to R' is computed by  $R_i' = FR_i = (\varepsilon + I)R_{i,14,5}$  in which F is the deformation gradient tensor and I is the identity tensor. The fitted surfaces are drawn in Figure 1 in the main text.

#### 2. The strength under finite strain theory

With respect to the strength of studied structures, i.e. the ultimate strain and the ultimate stress, the finite strain theory is employed instead of the infinitesimal strain approximation. The finite strain brings more specific definition of strain and stress and the curves of the second Piola–Kirchhoff (PK2) stress versus the Lagrangian strain are needed to observe the strength of materials. The Lagrangian strain is defined as:

$$\eta = \frac{1}{2} (F^T F - I) \tag{10}$$

For uniaxial tensions, the Lagrangian strain tensor and the deformation gradient tensor are respectively

$$\eta_{uniaxial} = \begin{pmatrix} \delta & 0 & 0\\ 0 & 0 & 0\\ 0 & 0 & 0 \end{pmatrix}$$
(11)

and

$$F_{uniaxial} = \begin{pmatrix} \varepsilon + 1 & 0 & 0\\ 0 & 1 & 0\\ 0 & 0 & 1 \end{pmatrix}$$
(12)

Therefore, in a range of 0–0.3 with an increment of 0.02 for the Lagrangian strain element  $\delta$ , we can obtain transformed structures by the transformation gradient tensor and compute their stresses by further. Note that the associated deformation gradient tensor is not unique for a given Lagrangian strain tensor, however only differing by a rigid rotation from one to another. Since the rigid deformation does not change the relative position of the atoms and the desired stress and energy,<sup>6,7</sup> we take the most uncomplicated treatment of the deformation. For biaxial tensions, the Lagrangian strain tensor and the deformation gradient tensor and the deformation.

$$\eta_{biaxial} = \begin{pmatrix} \delta & 0 & 0\\ 0 & \delta & 0\\ 0 & 0 & 0 \end{pmatrix}$$
(13)

and

$$F_{biaxial} = \begin{pmatrix} \varepsilon + 1 & 0 & 0 \\ 0 & \varepsilon + 1 & 0 \\ 0 & 0 & 1 \end{pmatrix}$$
(14)

with the same data spacing for the Lagrangian strain element  $\delta$ .

The stress calculated by the Vienna ab initio simulation package<sup>8</sup> is the true or Cauchy stress,  $\sigma$ , which related to PK2 stress as:

$$\Sigma = det^{\overline{m}}(F)F^{-1}\sigma F^{-T}$$
(15)

Because the uniaxial and biaxial tensions lead to two nonzero elements of the true stress tensor, the  $\sigma$  can be written as:

$$\sigma = \begin{pmatrix} \sigma_1 & 0 & 0\\ 0 & \sigma_2 & 0\\ 0 & 0 & 0 \end{pmatrix}$$
(16)

Combined these equations, we deduce the PK2 stresses under uniaxial and biaxial tension are:

$$\Sigma_{uniaxial} = \begin{pmatrix} \sigma_1 & 0 & 0\\ \hline (\epsilon+1) & 0 & 0\\ 0 & (\epsilon+1)\sigma_2 & 0\\ 0 & 0 & 0 \end{pmatrix}$$
(17)

$$\Sigma_{biaxial} = \begin{pmatrix} \sigma_1 & 0 & 0\\ 0 & \sigma_2 & 0\\ 0 & 0 & 0 \end{pmatrix}$$
(18)

The curves of two components of PK2 stress versus Lagrangian strain are drawn in Fig. S7.



**Fig. S7** PK2 stress versus Lagrangian strain under uniaxial tension (*x*-direction) for (a)  $H_2PPc$ , (c) F- $H_2PPc$  and (e) Cl- $H_2PPc$  and under biaxial tension for (b)  $H_2PPc$ , (d) F- $H_2PPc$  and (f) Cl- $H_2PPc$ .

Table S2 Adsorption energy (eV) for  $H_2$ , CO,  $CH_4$ ,  $CO_2$  and  $N_2$  adsorbing on pore-II of pristine, F- and Cl-H<sub>2</sub>PPc.

	H <sub>2</sub>	CO	$CH_4$	$CO_2$	$N_2$
H <sub>2</sub> PPc	0.07	0.13	0.13	0.18	0.12
F-H <sub>2</sub> PPc	0.07	0.13	0.13	0.18	0.12
Cl-H <sub>2</sub> PPc	0.13	0.22	0.23	0.25	0.18

**Table S3** Top view, side view and corresponding energy (eV) of the structures of IS, TS and FS for  $H_2$ , CO,  $CH_4$ ,  $CO_2$  and  $N_2$  passing through pristine  $H_2PPc$ .

Gas	Property	Initial State	Transition State	Final State
H <sub>2</sub>	Top View			
	Side View	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	0 <b>0-000000-000-000</b> -00	~~~ <del>~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~</del>
	Energy	-1085.09	-1085.09	-1085.09
СО	Top View			
	Side View			
	Energy	-1093.16	-1093.14	-1093.17
CH4	Top View			
	Side View		ം-ഞാത്ത-ട്രിട്ടി-താത്താ-ം-	
	Energy	-1102.44	-1102.45	-1102.44
CO <sub>2</sub>	Top View			
	Side View	00-000000-00		
	Energy	-1101.38	-1101.36	-1101.38
N <sub>2</sub>	Top View			
	Side View	C301003688	~~~~ <b>~~~~~~~~~~~~~~~~~</b>	->
	Energy	-1095.00	-1094.98	-1095.00

23		21 0 0	4	
Gas	Property	Initial State	Transition State	Final State
H <sub>2</sub>	Top View			
	Side View	6	0-0-C2000002-0-0-0-0-0-0-0-0-0-0-0-0-0-0	
	Energy	-1085.16	-1085.10	-1085.16
СО	Top View			
	Side View			
	Energy	-1093.19	-1092.99	-1093.20
CH <sub>4</sub>	Top View			
	Side View	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	00-massa file fallena-00	
	Energy	-1102.50	-1101.88	-1102.50
CO <sub>2</sub>	Top View			
	Side View		~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	
	Energy	-1101.36	-1101.31	-1101.36
N <sub>2</sub>	Top View			
	Side View		-0-0-CRIED-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0	
	Energy	-1095.05	-1094.81	-1095.05

**Table S4** Top view, side view and corresponding energy (eV) of the structures of IS, TS and FS for  $H_2$ , CO,  $CH_4$ , CO<sub>2</sub> and N<sub>2</sub> passing through F-H<sub>2</sub>PPc.

Gas	Property	Initial State	Transition State	Final State
H <sub>2</sub>	Top View			
	Side View	o Constant of the constant of	somercanfolaceano.	<b>de marado de Cananado d</b> O
	Energy	-1058.12	-1057.57	-1058.13
СО	Top View			
	Side View	eologicanofoquestion	fo baser fabilitano.	Someren of officers of
	Energy	-1066.18	-1065.14	-1066.19
CH <sub>4</sub>	Top View			
	Side View	eologasenadoo	for the state of t	<b>Boltranago Boltanago B</b> H
	Energy	-1075.46	-1074.09	-1075.46
CO <sub>2</sub>	Top View			
	Side View	oolaaaaagaaaaaaaaaaaaaaaaaaaaaaaaaaaaaa	toway former.	foranserofolationepoli vo
	Energy	-1074.42	-1072.92	-1074.40
N <sub>2</sub>	Top View			
	Side View	e-commencedermental-e-	to base filting or	gosamenanogosamenanogosamenanogosamenanogosamenanogosamenanogosamenanogosamenanogosamenanogosamenanogosamenanog S
	Energy	-1068.02	-1066.92	-1068.01

**Table S5** Top view, side view and corresponding energy (eV) of the structures of IS, TS and FS for  $H_2$ , CO,  $CH_4$ , CO<sub>2</sub> and  $N_2$  passing through Cl-H<sub>2</sub>PPc.



Fig. S8 Sketch of the minimum energy path for  $H_2$ , CO,  $CH_4$  and  $N_2$  passing through F- and Cl- $H_2PPc$ .



Fig. S9 Sketch of the minimum energy path for CO<sub>2</sub> passing through F- and Cl-H<sub>2</sub>PPc.

Section S7



**Fig. S10** Yellow areas stand for the pore areas in F- and Cl-H<sub>2</sub>PPc. Grey, blue, white, cyan and green balls stand for C, N, H, F and Cl atoms. Larger balls represent atoms with  $R_{\text{eff}}$  at pore-I.

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