

## Pressure-Dependent Kinetics of Methyl Formate Reaction with OH at Combustion, Atmospheric and Interstellar Temperatures

Junjun Wu <sup>a</sup>, Hongbo Ning <sup>a,b</sup>, Lihao Ma <sup>a</sup>, and Wei Ren <sup>a,b,\*</sup>

<sup>a</sup> Department of Mechanical and Automation Engineering, The Chinese University of Hong Kong, New Territories, Hong Kong

<sup>b</sup> Shenzhen Research Institute, The Chinese University of Hong Kong, New Territories, Hong Kong

\* Corresponding author. Fax: +852 2603 6002. Email: renwei@mae.cuhk.edu.hk (W. Ren)

### I. Optimized Geometries at M06-2x/ma-TZVP

#### 1. Reactant: MF

##### Conformer #1

	X	Y	Z
C 6	0.82527383	0.43152491	-0.00003200
O 8	1.28292474	-0.67192186	0.00001900
O 8	-0.47256690	0.72765185	0.00007300
C 6	-1.35372072	-0.39789892	-0.00004400
H 1	-1.18674476	-1.00537079	0.88834982
H 1	-1.18254776	-1.00855579	-0.88541182
H 1	-2.35896152	0.01115500	-0.00308400
H 1	1.41607071	1.35518172	-0.00013300

##### Conformer #2

	X	Y	Z
6	-0.68238686	0.31144894	-0.00616400
8	-1.80205663	-0.08490198	0.00843700
8	0.37682192	-0.50606190	-0.01017300

6	1.65613366	0.11724598	0.00724400
1	1.83544062	0.60449188	0.96668580
1	1.74951964	0.84440183	-0.80096684
1	2.38457251	-0.67459486	-0.13698897
1	-0.41013192	1.38124572	-0.02132900

## 2. Transition States-TS1

### Conformer #1

	X	Y	Z
6	0.16162197	0.22472995	-0.00909400
8	-0.04360199	1.39676371	-0.00114500
8	-0.73255885	-0.74552885	-0.00674600
6	-2.10155157	-0.31416794	0.00782400
1	1.23407175	-0.24805595	-0.01941300
1	-2.31096353	0.28564794	-0.87623482
1	-2.29458953	0.27677094	0.90157282
1	-2.69499545	-1.22227675	0.00874700
8	2.62320046	-0.52090889	0.00221100
1	2.92973840	0.40193692	0.03838899

### Conformer #2

	X	Y	Z
6	0.14400797	0.49403990	-0.00033400
8	-0.38311592	1.55743168	0.00022600
8	-0.44866491	-0.69211686	-0.00037700
6	-1.88370362	-0.65937787	0.00018300
1	1.30518173	0.32847193	-0.00065500
1	-2.24303054	-0.14358397	-0.88867082
1	-2.24233654	-0.14338297	0.88919882
1	-2.20254455	-1.69644665	0.00040900
8	2.53545248	-0.37396492	-0.00000200

1 2.19152955 -1.28382674 0.00185800

**Conformer #3**

	<b>X</b>	<b>Y</b>	<b>Z</b>
6	0.33315800	-0.68711118	0.04949004
8	0.67967375	-1.81879731	0.00234605
8	1.14032992	0.35849076	-0.06638794
6	0.53076339	1.65236813	0.01663805
1	-0.76512145	-0.36952910	0.19753801
1	0.06019463	1.78908360	0.98961685
1	-0.21089333	1.77574188	-0.77058479
1	1.33802497	2.36640915	-0.10947593
8	-2.19904563	0.13204629	0.00789205
1	-2.57339745	-0.72716515	-0.25466390

**Conformer #4**

	<b>X</b>	<b>Y</b>	<b>Z</b>
6	0.33789652	-0.68512197	0.04928777
8	0.69246452	-1.81432403	0.00238478
8	1.13775521	0.36611716	-0.06629721
6	0.51912340	1.65566941	0.01666678
1	-0.76259101	-0.37529313	0.19693074
1	-0.22276236	1.77429499	-0.77106706
1	1.32152782	2.37529660	-0.10860520
1	0.04688760	1.78884576	0.98933858
8	-2.19971131	0.11787195	0.00782978
1	-2.56924894	-0.74374957	-0.25366317

**Conformer #5**

	<b>X</b>	<b>Y</b>	<b>Z</b>
6	-0.32481521	-0.69044859	0.05008009
8	-0.65699971	-1.82639420	0.00231810
8	-1.14474652	0.34505960	-0.06695489
6	-0.55102198	1.64628704	0.01671309

1	0.76924374	-0.35914022	0.19957406
1	0.18883893	1.77904264	-0.77065775
1	-0.08178401	1.78810677	0.98960989
1	-1.36697046	2.35052931	-0.10864488
8	2.19748570	0.15688296	0.00797610
1	2.57977919	-0.69795606	-0.25735485

**Conformer #6**

	<b>X</b>	<b>Y</b>	<b>Z</b>
6	0.31611894	0.69386186	0.05025999
8	0.63346387	1.83402962	0.00225000
8	1.14928977	-0.33103393	-0.06688499
6	0.57214688	-1.63974867	0.01658100
1	-0.77355884	0.34852793	0.20016496
1	1.39701571	-2.33353652	-0.10879398
1	-0.16588697	-1.78164963	-0.77093384
1	0.10461998	-1.78762764	0.98939480
8	-2.19588555	-0.18275396	0.00813600
1	-2.58673247	0.66767287	-0.25888495

**Conformer #7**

	<b>X</b>	<b>Y</b>	<b>Z</b>
6	-0.01435500	0.73632185	0.05596499
8	0.16164197	1.90712961	0.01648600
8	-1.18873675	0.14140697	-0.10137698
6	-1.23228775	-1.28326074	0.03244399
1	0.84131583	-0.01996500	0.22362195
1	-2.09032457	-1.61464467	-0.54431789
1	-1.36581272	-1.54772668	1.08070078
1	-0.32067993	-1.73575564	-0.35537893
8	2.00003959	-0.98449880	0.00612500
1	2.63180246	-0.31257294	-0.30494894

**Conformer #8**

	<b>X</b>	<b>Y</b>	<b>Z</b>
6	-0.14179797	0.73697485	0.05812299
8	-0.17316596	1.92014760	0.01003900
8	-1.19372776	-0.05587899	-0.09242698
6	-0.96298680	-1.46467170	0.02730599
1	0.83076883	0.14118997	0.23300895
1	-0.14011797	-1.77424564	-0.61485987
1	-1.88639561	-1.94219060	-0.28421194
1	-0.74160185	-1.72234665	1.06257978
8	2.10662057	-0.66651386	0.00631700
1	2.64824346	0.08173398	-0.30051594

**2. Transition States-TS2****Conformer #1**

	<b>X</b>	<b>Y</b>	<b>Z</b>
6	1.24768574	-0.37487992	-0.24167395
8	0.74156285	-1.22476275	0.43038891
8	0.79943084	0.87562182	-0.36118193
6	-0.34526593	1.19658875	0.39139892
1	-0.21279196	0.97960080	1.44958170
1	-1.26107074	0.52409889	0.02426500
1	-0.60183588	2.22961854	0.18155896
1	-1.46556970	-1.21674275	0.06586699
8	-2.04364358	-0.51815289	-0.29038994
1	2.14794556	-0.50847090	-0.85015983

**Conformer #2**

	<b>X</b>	<b>Y</b>	<b>Z</b>
6	1.37236872	-0.15838097	-0.41156792
8	1.45922270	-0.94849881	0.47417390
8	0.46634690	0.83174083	-0.48219790

6	-0.45952591	0.90323081	0.57392488
1	-0.01027800	0.66806086	1.53716068
1	-1.29147074	0.09227098	0.40916592
1	-0.92915281	1.88070962	0.53789689
1	-2.37529751	-0.27924994	-0.99855480
8	-2.28709353	-0.72223785	-0.13779397
1	2.02133058	-0.11892398	-1.29326974

**Conformer #3**

	<b>X</b>	<b>Y</b>	<b>Z</b>
6	-1.49718758	-0.54767727	-0.00031807
8	-2.18506347	0.42533951	-0.00165307
8	-0.15667786	-0.54011923	0.00175193
6	0.44729199	0.73592052	0.00173593
1	0.22617402	1.29431640	-0.90559589
1	1.62920175	0.51401860	-0.00085907
1	0.22993102	1.29242440	0.91116974
1	2.46745062	-1.00630407	0.00290293
8	2.79243653	-0.09048925	-0.00204507
1	-1.85894548	-1.58176307	-0.00055507

**Conformer #4**

	<b>X</b>	<b>Y</b>	<b>Z</b>
6	1.09708877	-0.18701896	0.30331294
8	2.11094457	-0.65375487	-0.09519998
8	0.39051592	0.71155385	-0.41625091
6	-0.81574983	1.14811477	0.14617297
1	-0.71269886	1.45871870	1.18758976
1	-1.58358568	0.26654595	0.15446497
1	-1.21468875	1.93951160	-0.48017390
1	-1.85611362	-1.19279875	-0.90242182
8	-2.12062257	-1.03404279	0.02033500
1	0.63235487	-0.42860591	1.27256074

**Conformer #5**

	<b>X</b>	<b>Y</b>	<b>Z</b>
6	-1.05442579	-0.30291494	0.23092195
8	-2.14300956	-0.66504687	-0.06591699
8	-0.49190390	0.79627384	-0.31963493
6	0.77377384	1.15306576	0.15454097
1	1.10830177	2.02516059	-0.39887992
1	1.51199769	0.28024094	-0.07890698
1	0.79014584	1.31730373	1.23316975
1	2.88741841	-0.85842283	0.39350692
8	2.10796557	-1.01341679	-0.16677597
1	-0.39836692	-0.80766684	0.95695680

**3. Product****P<sub>1</sub>: (CO)OCH<sub>3</sub>**

	<b>X</b>	<b>Y</b>	<b>Z</b>
C	-0.81284400	0.50899500	-0.00000600
O	-1.41335600	-0.50629000	0.00000100
O	0.47587500	0.73398600	0.00002100
C	1.30786700	-0.45078200	-0.00002600
H	1.09625800	-1.04191500	-0.88897500
H	1.10231700	-1.03747900	0.89332100
H	2.33113500	-0.09145900	-0.00432200

**P<sub>2</sub>: H(CO)OCH<sub>2</sub>**

	<b>X</b>	<b>Y</b>	<b>Z</b>
C	0.76453500	0.44516200	-0.00492700
O	1.29579300	-0.62026900	0.00448200
O	-0.56990000	0.64669200	-0.00082800

C	-1.38286600	-0.44452900	0.02911700
H	-2.42784100	-0.21110900	-0.06229800
H	-0.94154200	-1.41865300	-0.09273100
H	1.27222900	1.41457300	-0.01934200

#### 4. H-bonded Complexes

**RC<sub>1</sub>:**

	<b>X</b>	<b>Y</b>	<b>Z</b>
C	-0.25077200	0.82031300	0.00055100
O	-1.31773600	1.35098800	-0.00054000
O	-0.05717400	-0.50594200	0.00068600
C	-1.25040500	-1.29688300	-0.00023000
H	0.71718000	1.33796900	0.00175700
H	-1.83957700	-1.08114100	-0.88981200
H	-1.84429600	-1.07623700	0.88494400
H	-0.92402300	-2.33196100	0.00341400
O	2.72544500	-0.00075400	-0.00040500
H	2.09349900	-0.74354300	-0.00016200

**PC<sub>1</sub>:**

	<b>X</b>	<b>Y</b>	<b>Z</b>
C	-0.28866800	0.78514900	-0.00909600
O	-1.22402300	1.49941400	0.00872400
O	-0.21110700	-0.52346400	-0.01445100
C	-1.47988200	-1.22633200	0.00501300
H	2.59585800	0.78468200	-0.04875500
H	-2.05510500	-0.95349700	-0.87706700
H	-2.02546600	-0.95811800	0.90713100
H	-1.22954300	-2.28139700	-0.00192700
O	2.84881800	-0.14113900	0.00984100
H	2.01604500	-0.62305900	0.01219800



**RC<sub>2</sub>:**

	<b>X</b>	<b>Y</b>	<b>Z</b>
C	1.13919300	-0.79211500	0.00021500
O	0.05211300	-1.30209100	-0.00053400
O	1.38239800	0.50570700	0.00049200
C	0.23404700	1.36393900	-0.00041700
H	-0.36910500	1.18578100	0.88943400
H	-0.36868800	1.18448900	-0.89029200
H	0.62268800	2.37668800	-0.00104200
H	-1.76219900	-0.63411300	-0.00022900
O	-2.48952600	0.02290800	0.00036800
H	2.07798800	-1.35598500	0.00073100

**PC<sub>2</sub>:**

	<b>X</b>	<b>Y</b>	<b>Z</b>
C	0.70487900	-0.85240500	-0.37891100
O	0.25892500	-1.30558900	0.63143200
O	0.99645300	0.44737000	-0.57410800
C	0.75085700	1.31558200	0.44423700
H	0.62983200	0.91078300	1.43599900
H	-1.94291500	1.08608500	0.03308600
H	1.06896500	2.32135400	0.23230100
H	-1.78478900	-0.38022400	0.43108900
O	-2.21161000	0.19596500	-0.21260300
H	0.94434700	-1.41902900	-1.28220500

## II. IRC Analysis at M06-2x/ma-TZVP

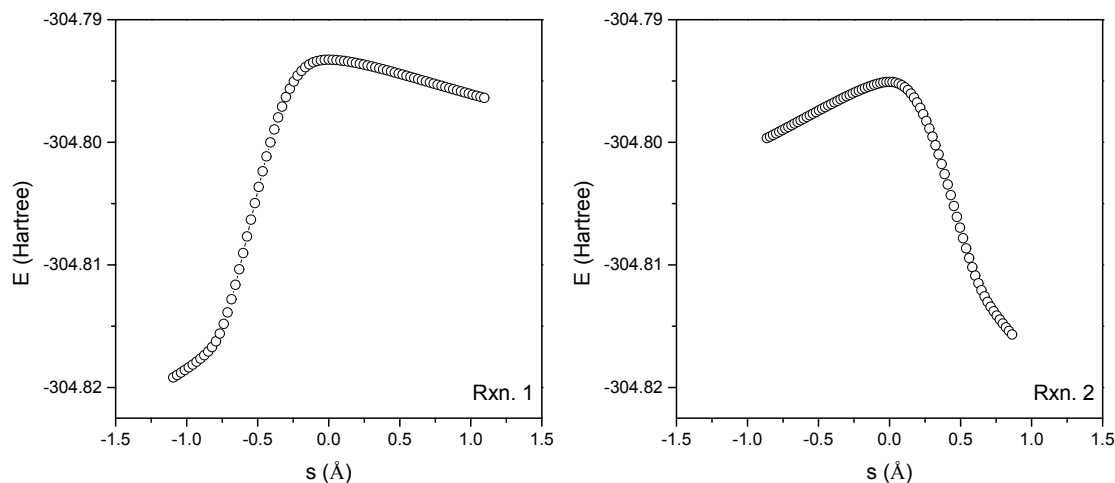
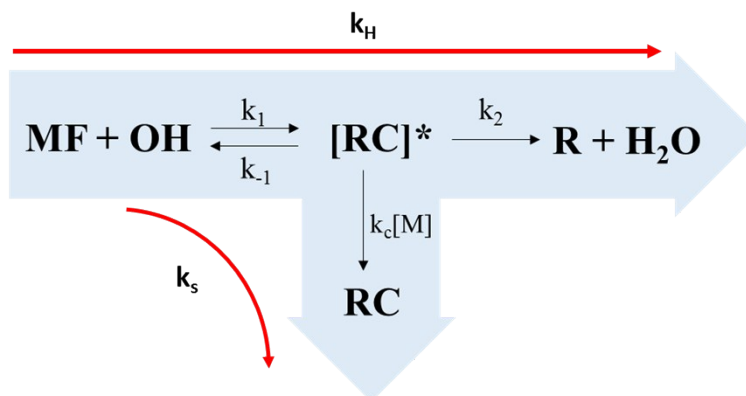


Figure S1. IRC analysis for Rxn. 1 and Rxn. 2 at M06-2x/ma-TZVP level of theory

## III. Summary of Kinetic Data

The whole reaction involves two pathways: one is to form products by abstracting with rate coefficient  $k_H$ , the other is to form stabilized RC by collision with rate coefficient  $k_s$ . Note that the  $k_H$  and  $k_s$  are global rate coefficient (lumped rather than elementary) and therefore,  $k_H$  is not necessarily pressure-independent. A simple analysis is provided here to interpret the pressure-dependence of the two rate coefficient.



Scheme 1. Demonstration of the MF + OH reaction: H-abstraction ( $k_H$ ) and collisional stabilization ( $k_s$ )

For the pure H-abstraction channel that forms final products, we have:

$$\frac{d[R]}{dt} = k_H[MF][OH] = k_2[RC^*], \quad (1)$$

For the stabilization channel that forms products, we have:

$$\frac{d[RC]}{dt} = k_s[MF][OH] = k_c[M][RC^*], \quad (2)$$

The fate of  $RC^*$  can be determined as:

$$\frac{d[RC^*]}{dt} = k_1[MF][OH] - k_{-1}[RC^*] - k_2[RC^*] - k_c[M][RC^*], \quad (3)$$

By adopting the quasi-steady state approximation, we can obtain  $k_H$  and  $k_s$  as:

$$k_H = \frac{k_1 k_2}{k_{-1} + k_2 + k_c[M]}, \quad (4a)$$

$$k_s = \frac{k_1 k_c [M]}{k_{-1} + k_2 + k_c[M]}. \quad (4b)$$

It's seen that both  $k_H$  and  $k_s$  involve the  $[M]$  term and thus the pressure effect. It's also seen that  $k_H$  and  $k_s$  are internally correlated by  $k_c[M]$  term. At high-temperatures,  $k_c$  that represents the deactivation rate coefficient becomes extremely small, i.e.  $k_c \rightarrow 0$ . Therefore, the rate coefficient of pure H-abstraction  $k_H$  becomes pressure-independent (close to HPL) since:

$$k_H \approx \frac{k_1 k_2}{k_{-1} + k_2}, \quad (5)$$

At very low temperatures where  $k_c$  matters, the rate coefficient becomes pressure-dependent. Increased pressure leads to larger  $[M]$  and thus  $k_H$  will decrease. As the pressure decreases to extremely low, i.e.  $[M] \rightarrow 0$ , the rate coefficient will again approach to the HPL. On the contrary,  $k_s$  will increase due to increased pressures, as seen in Equation (4b).

Table S1 Rate coefficient of H-abstraction at 20 K from MF by OH radical with He and N<sub>2</sub> as the bath gas (units in  $\text{cm}^3 \cdot \text{molec}^{-1} \cdot \text{s}^{-1}$ )

	0.001 bar	0.01 bar	0.1 bar	1.0 bar	10 bar	100 bar
in He	6.31E-11	8.09E-11	2.85E-12	3.67E-13	5.84E-15	6.34E-17
in N <sub>2</sub>	6.97E-11	6.94E-11	3.73E-11	8.57E-12	1.14E-12	1.21E-13

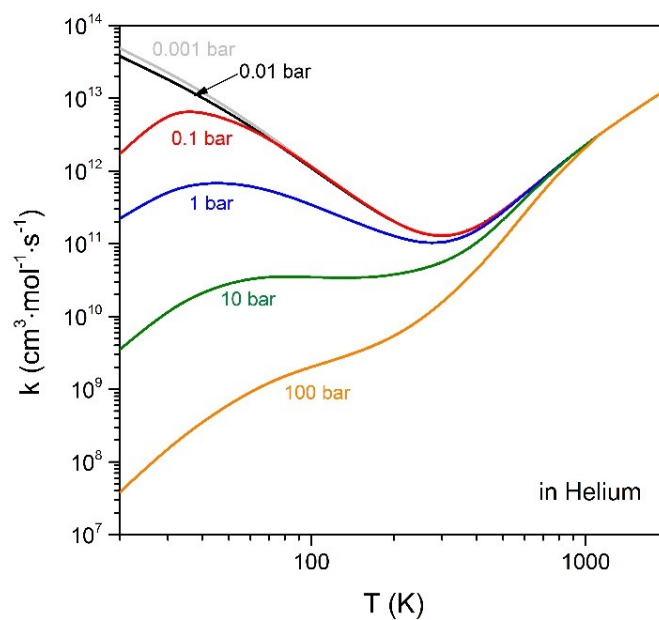


Figure S2. Rate coefficient of H-abstraction from MF by OH radical with He as bath gas

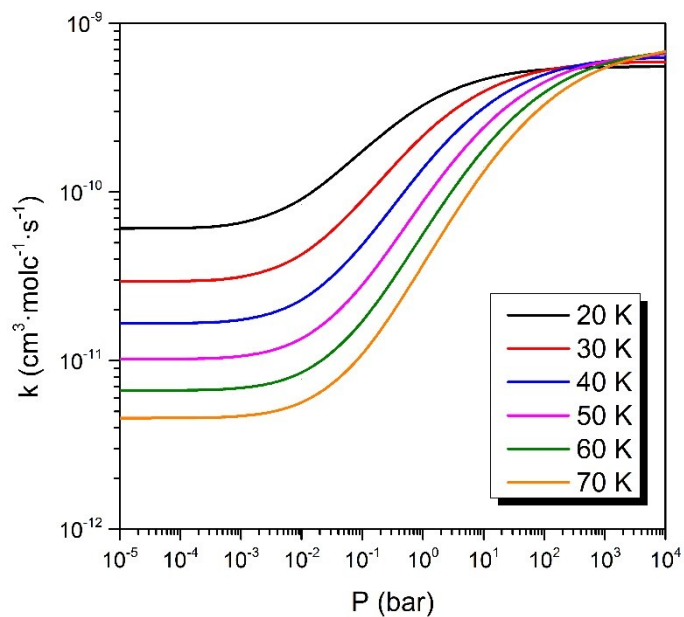


Figure S3. Plots of the pressure- and temperature-dependent rate coefficient of MF + OH with He as the bath gas.

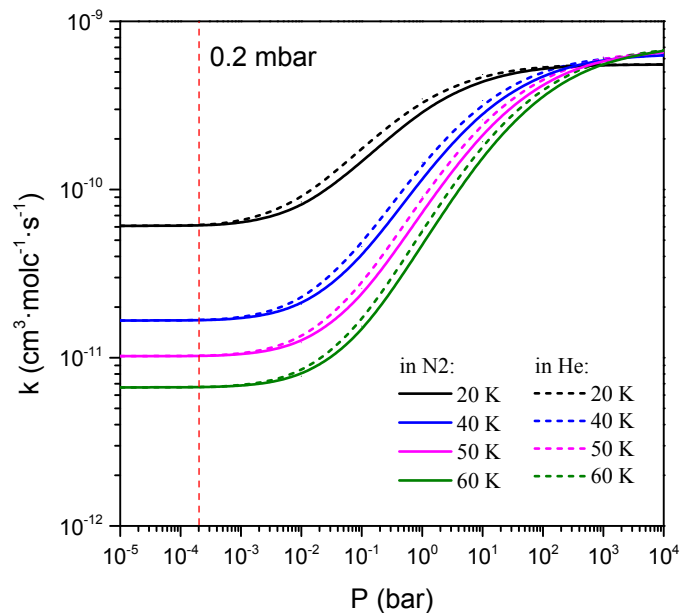


Figure S4. Rate coefficients of MF + OH as the function of pressures at 20,40,50, 60 K. Bath gas including nitrogen (N<sub>2</sub>) and helium (He) are considered. The experimental measurements at interstellar temperatures were benchmarked by Jiménez et al<sup>11</sup>.

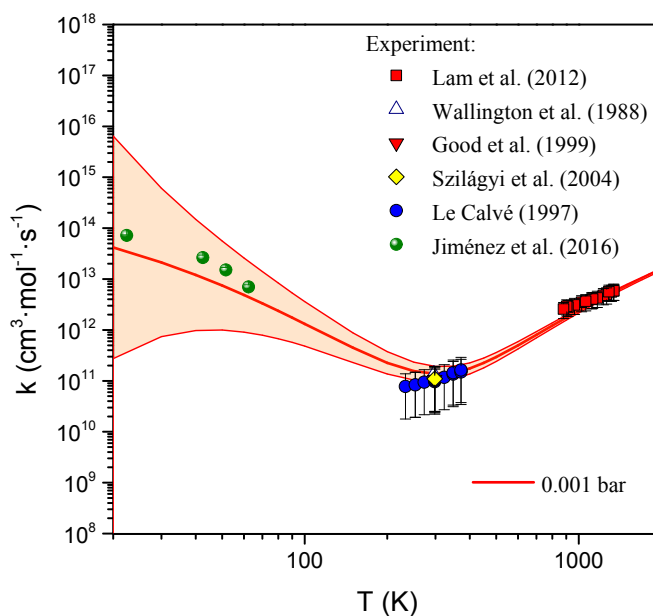


Figure S5. The rate coefficient of MF+OH reactions at 20-2000 K and at 0.001 bar in N<sub>2</sub>. The shadow region indicate the uncertainty caused by an uncertainty of  $0.2 \text{ kcal} \cdot \text{mol}^{-1}$  in energy barrier.

Table S2. Detailed H-abstraction rate coefficient  $k_H$  of MF + OH with He as the bath gas (units in  $\text{cm}^3 \cdot \text{molec}^{-1} \cdot \text{s}^{-1}$ )

T	0.001 Bar	0.01 Bar	0.1 Bar	1.0 Bar	10 Bar	100 bar
20	6.31E-11	8.09E-11	2.85E-12	3.67E-13	5.84E-15	6.34E-17
30	3.04E-11	3.77E-11	1.14E-11	9.17E-13	2.04E-14	2.60E-16
40	1.70E-11	2.03E-11	1.08E-11	1.14E-12	3.57E-14	5.87E-16
50	1.04E-11	1.21E-11	8.43E-12	1.13E-12	4.73E-14	1.02E-15
60	6.76E-12	7.64E-12	6.25E-12	1.03E-12	5.46E-14	1.53E-15
70	4.62E-12	5.12E-12	4.56E-12	9.00E-13	5.80E-14	2.04E-15
80	3.28E-12	3.58E-12	3.34E-12	7.71E-13	5.88E-14	2.51E-15
90	2.41E-12	2.59E-12	2.50E-12	6.62E-13	5.84E-14	2.95E-15
100	1.82E-12	1.94E-12	1.90E-12	5.70E-13	5.75E-14	3.36E-15
150	6.28E-13	6.46E-13	6.47E-13	3.09E-13	5.56E-14	5.39E-15
200	3.27E-13	3.30E-13	3.27E-13	2.08E-13	6.15E-14	8.71E-15
250	2.33E-13	2.33E-13	2.27E-13	1.70E-13	7.31E-14	1.49E-14
300	2.13E-13	2.12E-13	2.07E-13	1.70E-13	9.11E-14	2.57E-14
350	2.33E-13	2.33E-13	2.27E-13	1.95E-13	1.21E-13	4.40E-14
400	2.85E-13	2.84E-13	2.79E-13	2.49E-13	1.69E-13	7.28E-14
450	3.67E-13	3.66E-13	3.62E-13	3.34E-13	2.43E-13	1.18E-13
500	4.81E-13	4.81E-13	4.78E-13	4.53E-13	3.53E-13	1.88E-13
600	8.18E-13	8.18E-13	8.16E-13	7.98E-13	6.96E-13	4.36E-13
700	1.31E-12	1.31E-12	1.31E-12	1.30E-12	1.21E-12	8.78E-13
800	1.97E-12	1.97E-12	1.97E-12	1.97E-12	1.90E-12	1.53E-12
900	2.81E-12	2.81E-12	2.81E-12	2.81E-12	2.81E-12	2.41E-12
1000	3.80E-12	3.80E-12	3.80E-12	3.80E-12	3.80E-12	3.45E-12
1100	4.96E-12	4.96E-12	4.96E-12	4.96E-12	4.96E-12	4.96E-12
1200	6.28E-12	6.28E-12	6.28E-12	6.28E-12	6.28E-12	6.28E-12
1300	7.76E-12	7.76E-12	7.76E-12	7.76E-12	7.76E-12	7.76E-12
1400	9.40E-12	9.40E-12	9.40E-12	9.40E-12	9.40E-12	9.40E-12
1500	1.12E-11	1.12E-11	1.12E-11	1.12E-11	1.12E-11	1.12E-11
1600	1.31E-11	1.31E-11	1.31E-11	1.31E-11	1.31E-11	1.31E-11
1700	1.53E-11	1.53E-11	1.53E-11	1.53E-11	1.53E-11	1.53E-11
1800	1.76E-11	1.76E-11	1.76E-11	1.76E-11	1.76E-11	1.76E-11
1900	2.00E-11	2.00E-11	2.00E-11	2.00E-11	2.00E-11	2.00E-11
2000	2.26E-11	2.26E-11	2.26E-11	2.26E-11	2.26E-11	2.26E-11

Table S3. Detailed H-abstraction rate coefficient  $k_H$  of MF + OH with N<sub>2</sub> as the bath gas (units in cm<sup>3</sup>·molec<sup>-1</sup>·s<sup>-1</sup>)

T	0.001 Bar	0.01 Bar	0.1 Bar	1.0 Bar	10 Bar	100 bar
20	6.97E-11	6.94E-11	3.73E-11	8.57E-12	1.14E-12	1.21E-13
30	3.52E-11	3.52E-11	2.98E-11	1.09E-11	2.12E-12	2.66E-13
40	2.00E-11	2.00E-11	1.73E-11	1.05E-11	2.80E-12	4.41E-13
50	1.24E-11	1.24E-11	1.08E-11	8.87E-12	3.05E-12	6.05E-13
60	8.08E-12	8.08E-12	7.21E-12	7.18E-12	3.00E-12	7.38E-13
70	5.54E-12	5.54E-12	5.02E-12	5.02E-12	2.76E-12	8.19E-13
80	3.94E-12	3.94E-12	3.63E-12	3.63E-12	2.44E-12	8.51E-13
90	2.90E-12	2.90E-12	2.71E-12	2.71E-12	2.12E-12	8.51E-13
100	2.19E-12	2.19E-12	2.08E-12	2.08E-12	1.80E-12	8.14E-13
150	7.43E-13	7.43E-13	7.18E-13	7.18E-13	6.36E-13	5.42E-13
200	3.76E-13	3.76E-13	3.69E-13	3.69E-13	3.34E-13	3.02E-13
250	2.58E-13	2.58E-13	2.57E-13	2.57E-13	2.38E-13	2.20E-13
300	2.28E-13	2.28E-13	2.28E-13	2.28E-13	2.15E-13	2.04E-13
350	2.43E-13	2.44E-13	2.44E-13	2.44E-13	2.35E-13	2.27E-13
400	2.92E-13	2.92E-13	2.93E-13	2.93E-13	2.89E-13	2.85E-13
450	3.73E-13	3.73E-13	3.74E-13	3.75E-13	3.75E-13	3.75E-13
500	4.88E-13	4.88E-13	4.88E-13	4.89E-13	4.89E-13	4.89E-13
600	8.29E-13	8.29E-13	8.29E-13	8.29E-13	8.29E-13	8.29E-13
700	1.34E-12	1.34E-12	1.34E-12	1.34E-12	1.34E-12	1.34E-12
800	2.03E-12	2.03E-12	2.03E-12	2.03E-12	2.03E-12	2.03E-12
900	2.90E-12	2.90E-12	2.90E-12	2.90E-12	2.90E-12	2.90E-12
1000	3.97E-12	3.97E-12	3.97E-12	3.97E-12	3.97E-12	3.97E-12
1100	5.23E-12	5.23E-12	5.23E-12	5.23E-12	5.23E-12	5.23E-12
1200	6.69E-12	6.69E-12	6.69E-12	6.69E-12	6.69E-12	6.69E-12
1300	8.35E-12	8.35E-12	8.35E-12	8.35E-12	8.35E-12	8.35E-12
1400	1.02E-11	1.02E-11	1.02E-11	1.02E-11	1.02E-11	1.02E-11
1500	1.23E-11	1.23E-11	1.23E-11	1.23E-11	1.23E-11	1.23E-11
1600	1.45E-11	1.45E-11	1.45E-11	1.45E-11	1.45E-11	1.45E-11
1700	1.70E-11	1.70E-11	1.70E-11	1.70E-11	1.70E-11	1.70E-11
1800	1.97E-11	1.97E-11	1.97E-11	1.97E-11	1.97E-11	1.97E-11
1900	2.26E-11	2.26E-11	2.26E-11	2.26E-11	2.26E-11	2.26E-11
2000	2.57E-11	2.57E-11	2.57E-11	2.57E-11	2.57E-11	2.57E-11

Table S4. Collection of the pressure-dependent rate coefficient for Rxn. 1 (units in  $\text{cm}^3 \cdot \text{molec}^{-1} \cdot \text{s}^{-1}$ )

T	0.001 Bar	0.01 Bar	0.1 Bar	1.0 Bar	10 Bar	100 bar	LPL	HPL	PEM
20	5.48E-13	5.41E-13	3.57E-13	1.60E-13	4.38E-14	6.94E-15	1.14E-15	1.73E-10	2.06E-08
30	1.98E-13	2.29E-13	1.86E-13	1.13E-13	4.70E-14	1.14E-14	1.03E-15	1.93E-10	2.39E-11
40	9.58E-14	1.18E-13	1.07E-13	7.67E-14	4.12E-14	1.41E-14	1.04E-15	8.43E-11	8.85E-13
50	5.51E-14	6.84E-14	6.62E-14	5.26E-14	3.35E-14	1.47E-14	1.13E-15	3.90E-12	1.37E-13
60	3.54E-14	4.37E-14	4.40E-14	3.75E-14	2.69E-14	1.43E-14	1.23E-15	4.17E-13	4.28E-14
70	2.54E-14	3.04E-14	3.12E-14	2.79E-14	2.17E-14	1.35E-14	1.44E-15	9.51E-14	2.06E-14
80	1.94E-14	2.26E-14	2.32E-14	2.14E-14	1.79E-14	1.25E-14	1.73E-15	3.52E-14	1.31E-14
90	1.59E-14	1.78E-14	1.83E-14	1.73E-14	1.52E-14	1.16E-14	2.06E-15	1.81E-14	9.88E-15
100	1.35E-14	1.48E-14	1.52E-14	1.46E-14	1.33E-14	1.09E-14	2.49E-15	1.18E-14	8.50E-15
150	1.22E-14	1.26E-14	1.32E-14	1.34E-14	1.20E-14	1.16E-14	6.33E-15	8.17E-15	9.61E-15
200	1.81E-14	1.83E-14	1.83E-14	1.84E-14	1.84E-14	1.84E-14	1.39E-14	1.43E-14	1.68E-14
250	3.04E-14	3.04E-14	3.05E-14	3.05E-14	3.05E-14	3.05E-14	2.71E-14	2.66E-14	2.99E-14
300	5.05E-14	5.05E-14	5.05E-14	5.05E-14	5.05E-14	5.05E-14	4.77E-14	4.70E-14	5.06E-14
350	8.12E-14	8.12E-14	8.12E-14	8.12E-14	8.12E-14	8.12E-14	7.90E-14	7.82E-14	8.24E-14
400	1.26E-13	1.26E-13	1.26E-13	1.26E-13	1.26E-13	1.26E-13	1.24E-13	1.23E-13	1.28E-13
450	1.88E-13	1.88E-13	1.88E-13	1.88E-13	1.88E-13	1.88E-13	1.88E-13	1.86E-13	1.91E-13
500	2.71E-13	2.71E-13	2.71E-13	2.71E-13	2.71E-13	2.71E-13	2.72E-13	2.69E-13	2.76E-13
600	5.08E-13	5.08E-13	5.08E-13	5.08E-13	5.08E-13	5.08E-13	5.13E-13	5.05E-13	5.18E-13
700	8.55E-13	8.55E-13	8.55E-13	8.55E-13	8.55E-13	8.55E-13	8.67E-13	8.47E-13	8.72E-13
800	1.31E-12	1.31E-12	1.31E-12	1.31E-12	1.31E-12	1.31E-12	1.33E-12	1.29E-12	1.34E-12
900	1.89E-12	1.89E-12	1.89E-12	1.89E-12	1.89E-12	1.89E-12	1.91E-12	1.84E-12	1.93E-12
1000	2.57E-12	2.57E-12	2.57E-12	2.57E-12	2.57E-12	2.57E-12	2.61E-12	2.49E-12	2.62E-12
1100	3.35E-12	3.35E-12	3.35E-12	3.35E-12	3.35E-12	3.35E-12	3.42E-12	3.20E-12	3.42E-12
1200	4.23E-12	4.23E-12	4.23E-12	4.23E-12	4.23E-12	4.23E-12	4.32E-12	4.02E-12	4.32E-12
1300	5.20E-12	5.20E-12	5.20E-12	5.20E-12	5.20E-12	5.20E-12	5.33E-12	4.88E-12	5.33E-12
1400	6.26E-12	6.26E-12	6.26E-12	6.26E-12	6.26E-12	6.26E-12	6.43E-12	5.81E-12	6.43E-12
1500	7.40E-12	7.40E-12	7.40E-12	7.40E-12	7.40E-12	7.40E-12	7.62E-12	6.81E-12	7.60E-12
1600	8.62E-12	8.62E-12	8.62E-12	8.62E-12	8.62E-12	8.62E-12	8.90E-12	7.85E-12	8.88E-12
1700	9.91E-12	9.91E-12	9.91E-12	9.91E-12	9.91E-12	9.91E-12	1.03E-11	8.97E-12	1.03E-11
1800	1.13E-11	1.13E-11	1.13E-11	1.13E-11	1.13E-11	1.13E-11	1.17E-11	1.01E-11	1.17E-11
1900	1.27E-11	1.27E-11	1.27E-11	1.27E-11	1.27E-11	1.27E-11	1.32E-11	1.13E-11	1.32E-11
2000	1.42E-11	1.42E-11	1.42E-11	1.42E-11	1.42E-11	1.42E-11	1.49E-11	1.26E-11	1.49E-11



Table S5. Collection of the pressure-dependent rate coefficient for Rxn. 2 (units in  $\text{cm}^3 \cdot \text{molec}^{-1} \cdot \text{s}^{-1}$ )

T	0.001 Bar	0.01 Bar	0.1 Bar	1.0 Bar	10 Bar	100 bar	LPL	HPL	PEM
20	7.02E-11	7.01E-11	3.75E-11	8.55E-12	1.11E-12	1.17E-13	2.61E-13	3.67E-10	3.20E+35
30	3.50E-11	3.75E-11	2.96E-11	1.08E-11	2.08E-12	2.54E-13	1.91E-13	4.00E-10	3.82E+17
40	1.99E-11	2.16E-11	2.09E-11	1.04E-11	2.76E-12	4.27E-13	1.53E-13	4.25E-10	4.25E+08
50	1.23E-11	1.33E-11	1.44E-11	8.82E-12	3.02E-12	5.91E-13	1.46E-13	4.43E-10	1.86E+03
60	8.05E-12	8.63E-12	9.96E-12	7.14E-12	2.97E-12	7.24E-13	1.13E-13	4.57E-10	5.08E-01
70	5.51E-12	5.88E-12	6.99E-12	5.63E-12	2.74E-12	8.05E-13	9.51E-14	4.65E-10	1.53E-03
80	3.92E-12	4.15E-12	5.00E-12	4.40E-12	2.42E-12	8.38E-13	8.68E-14	4.72E-10	1.99E-05
90	2.87E-12	3.02E-12	3.67E-12	3.47E-12	2.11E-12	8.38E-13	8.47E-14	4.73E-10	7.12E-07
100	2.17E-12	2.27E-12	2.74E-12	2.71E-12	1.79E-12	8.04E-13	7.55E-14	4.60E-10	5.20E-08
150	7.31E-13	7.47E-13	8.50E-13	9.40E-13	7.95E-13	5.30E-13	6.23E-14	1.48E-11	3.14E-11
200	3.59E-13	3.62E-13	3.90E-13	4.23E-13	3.97E-13	3.24E-13	6.13E-14	9.98E-13	1.51E-12
250	2.27E-13	2.29E-13	2.37E-13	2.47E-13	2.41E-13	2.17E-13	7.45E-14	3.14E-13	4.00E-13
300	1.78E-13	1.78E-13	1.83E-13	1.99E-13	1.81E-13	1.73E-13	6.99E-14	1.94E-13	2.26E-13
350	1.62E-13	1.62E-13	1.64E-13	1.71E-13	1.74E-13	1.76E-13	8.47E-14	1.65E-13	1.81E-13
400	1.66E-13	1.66E-13	1.68E-13	1.69E-13	1.71E-13	1.71E-13	1.04E-13	1.66E-13	1.78E-13
450	1.86E-13	1.86E-13	1.86E-13	1.88E-13	1.88E-13	1.88E-13	1.30E-13	1.83E-13	1.94E-13
500	2.17E-13	2.17E-13	2.17E-13	2.17E-13	2.19E-13	2.19E-13	1.65E-13	2.14E-13	2.24E-13
600	3.20E-13	3.20E-13	3.20E-13	3.20E-13	3.20E-13	3.20E-13	2.72E-13	3.14E-13	3.29E-13
700	4.83E-13	4.83E-13	4.83E-13	4.83E-13	4.83E-13	4.83E-13	4.48E-13	4.68E-13	4.95E-13
800	7.11E-13	7.11E-13	7.11E-13	7.11E-13	7.12E-13	7.12E-13	6.86E-13	6.82E-13	7.26E-13
900	1.01E-12	1.01E-12	1.01E-12	1.01E-12	1.01E-12	1.01E-12	9.80E-13	9.65E-13	1.03E-12
1000	1.40E-12	1.40E-12	1.40E-12	1.40E-12	1.40E-12	1.40E-12	1.39E-12	1.32E-12	1.43E-12
1100	1.88E-12	1.88E-12	1.88E-12	1.88E-12	1.88E-12	1.88E-12	1.88E-12	1.76E-12	1.91E-12
1200	2.46E-12	2.46E-12	2.46E-12	2.46E-12	2.46E-12	2.46E-12	2.46E-12	2.29E-12	2.51E-12
1300	3.14E-12	3.14E-12	3.14E-12	3.14E-12	3.14E-12	3.14E-12	3.20E-12	2.91E-12	3.20E-12
1400	3.95E-12	3.95E-12	3.95E-12	3.95E-12	3.95E-12	3.95E-12	4.10E-12	3.62E-12	4.02E-12
1500	4.86E-12	4.86E-12	4.86E-12	4.86E-12	4.86E-12	4.86E-12	5.01E-12	4.45E-12	4.96E-12
1600	5.91E-12	5.91E-12	5.91E-12	5.91E-12	5.91E-12	5.91E-12	6.06E-12	5.40E-12	6.03E-12
1700	7.11E-12	7.11E-12	7.11E-12	7.11E-12	7.11E-12	7.11E-12	7.39E-12	6.44E-12	7.26E-12
1800	8.42E-12	8.42E-12	8.42E-12	8.42E-12	8.42E-12	8.42E-12	8.67E-12	7.62E-12	8.60E-12
1900	9.88E-12	9.88E-12	9.88E-12	9.88E-12	9.88E-12	9.88E-12	1.02E-11	8.92E-12	1.01E-11
2000	1.15E-11	1.15E-11	1.15E-11	1.15E-11	1.15E-11	1.15E-11	1.19E-11	1.03E-11	1.18E-11

Table S6. The MS-T scaling factors for Rxn. 1 and Rxn. 2 over 20-20000 K at the theory level of M06-2x/ma-TZVP

T	Rxn. 1	Rxn. 2
20	0.988922	1.853978
30	0.988922	1.853978
40	1.012871	1.880198
50	1.037938	1.892023
60	1.060172	1.888252
70	1.080827	1.87594
80	1.097222	1.855556
90	1.112431	1.832724
100	1.125792	1.80905
150	1.180531	1.704425
200	1.233304	1.634907
250	1.302452	1.603996
300	1.391993	1.620112
350	1.50622	1.694737
400	1.634936	1.828263
450	1.772864	2.020101
500	1.910678	2.262834
600	2.157672	2.853968
700	2.34338	3.523143
800	2.456216	4.195676
900	2.508073	4.835307
1000	2.514408	5.427962
1100	2.483667	5.955743
1200	2.436004	6.436004
1300	2.374101	6.86742
1400	2.304569	7.249746
1500	2.231928	7.593373
1600	2.158052	7.898608
1700	2.086785	8.178501
1800	2.01665	8.428012
1900	1.949367	8.648491
2000	1.885548	8.85354

**Sample input file for MS-T calculation**

```
### Template of input file for MSTor program ###  
### User needs to input correct values for all the keywords ###
```

```
$GENERAL
```

```
  natoms  8
```

```
  nstr    2
```

```
  ntor    2
```

```
  elec
```

```
    1 0.0
```

```
  end
```

```
  freqscale 1.000
```

```
  deltat 0.5
```

```
END
```

```
$framechain
```

```
  1 2
```

```
  1 2 3
```

```
end
```

```
$framedef
```

```
  1 : 1 2 8
```

```
  2 : 3
```

```
  3 : 4 5 6 7
```

```
end
```

```
$INTDEF
```

```
2-1 8-1 1-3 3-4 4-5 4-6 4-7
```

```
2-1-8 2-1-3 8-1-3
```

```
3-4-6 3-4-7 5-4-6 5-4-7 6-4-7
```

```
1-3-4
```

```
4-3-1-8 5-4-3-1
```

```
END
```

\$TEMP

20 30 40 50 60 70 80 90 100 150 200 250 300 350 400 450 500 600. 700. 800. 900. 1000. 1100. 1200. 1300.  
1400. 1500. 1600. 1700. 1800. 1900. 2000.

END

\$structure 1

geom

6 0.82527383 0.43152491 -0.00003200  
8 1.28292474 -0.67192186 0.00001900  
8 -0.47256690 0.72765185 0.00007300  
6 -1.35372072 -0.39789892 -0.00004400  
1 -1.18674476 -1.00537079 0.88834982  
1 -1.18254776 -1.00855579 -0.88541182  
1 -2.35896152 0.01115500 -0.00308400  
1 1.41607071 1.35518172 -0.00013300

end

energy 0.00000

weight 1

rotsigma 1

# Symmetry point group: Cs

mtor

2.0180 3.

end

END

\$structure 2

geom

6 -0.68238686 0.31144894 -0.00616400  
8 -1.80205663 -0.08490198 0.00843700  
8 0.37682192 -0.50606190 -0.01017300  
6 1.65613366 0.11724598 0.00724400  
1 1.83544062 0.60449188 0.96668580  
1 1.74951964 0.84440183 -0.80096684

1 2.38457251 -0.67459486 -0.13698897

1 -0.41013192 1.38124572 -0.02132900

end

energy 5.44041

weight 2

rotsigma 1

# Symmetry point group: C1

mtor

3.9646 3.

end

END



O	-0.05717400	-0.50594200	0.00068600
C	-1.25040500	-1.29688300	-0.00023000
H	0.71718000	1.33796900	0.00175700
H	-1.83957700	-1.08114100	-0.88981200
H	-1.84429600	-1.07623700	0.88494400
H	-0.92402300	-2.33196100	0.00341400
O	2.72544500	-0.00075400	-0.00040500
H	2.09349900	-0.74354300	-0.00016200

Core RigidRotor

SymmetryFactor 1

End

Frequencies[1/cm] 24

44.2814

71.4963

128.3625

165.5097

296.2958

328.2133

338.7320

504.8841

790.3547

977.4539

1056.5992

1193.6528

1202.3594

1251.3466

1426.1566

1482.0710

1492.4851

1504.8799

1862.0931

3095.2097

3123.6237

3175.7209

3203.0190

3727.6231

ZeroEnergy[kcal/mol] 0 !-1.875

```
End
End
Bimolecular          R          # MF + OH
Fragment    C2H4O2
RRHO
Geometry[angstrom]      8
  C    0.82527400  0.43152500 -0.00003200
  O    1.28292500 -0.67192200  0.00001900
  O   -0.47256700  0.72765200  0.00007300
  C   -1.35372100 -0.39789900 -0.00004400
  H   -1.18674500 -1.00537100  0.88835000
  H   -1.18254800 -1.00855600 -0.88541200
  H   -2.35896200  0.01115500 -0.00308400
  H    1.41607100  1.35518200 -0.00013300
Core RigidRotor
SymmetryFactor          1
End
Frequencies[1/cm]      18
91.3023
318.5380
350.6410
792.5903
985.1802
1067.7163
1184.5877
1204.2954
1272.8776
1405.5534
1475.2131
1487.0945
1500.4241
1850.7900
3077.6375
3102.3855
3157.1877
3184.8780
ZeroEnergy[1/cm]      0
```



```
ElectronicLevels[1/cm] 1
  0 1
End
Fragment OH
RRHO
Geometry[angstrom] 2
O 0.00000000 0.00000000 0.10815400
H 0.00000000 0.00000000 -0.86523400
Core RigidRotor
  SymmetryFactor 1
  End
  Frequencies[1/cm] 1
  3738.6669
ZeroEnergy[1/cm] 0
ElectronicLevels[1/cm] 1
  0 2
End
GroundEnergy[kcal/mol] 1.874495963
End
Bimolecular P1 # (CO)OCH3 + H2O
Fragment C2H3O2
RRHO
Geometry[angstrom] 7
C -0.81284400 0.50899500 -0.00000600
O -1.41335600 -0.50629000 0.00000100
O 0.47587500 0.73398600 0.00002100
C 1.30786700 -0.45078200 -0.00002600
H 1.09625800 -1.04191500 -0.88897500
H 1.10231700 -1.03747900 0.89332100
H 2.33113500 -0.09145900 -0.00432200
Core RigidRotor
  SymmetryFactor 1
  End
  Frequencies[1/cm] 15
  126.8874
  293.2097
  389.6733
```

```
776.0953
956.1352
1175.3106
1181.7938
1225.6315
1470.5068
1492.1729
1496.7755
1909.5486
3092.8521
3179.1821
    3207.4870
ZeroEnergy[1/cm]    0
ElectronicLevels[1/cm]  1
  0    2
End
Fragment    H2O
RRHO
  Geometry[angstrom]    3
  O      0.00000000  0.00000000  0.11600300
  H      0.00000000  0.76532600 -0.46401400
  H      0.00000000 -0.76532600 -0.46401400
  Core  RigidRotor
  SymmetryFactor    2
  End
  Frequencies[1/cm]    3
  1597.3541
  3866.1715
  3974.4742
ZeroEnergy[1/cm]    0
ElectronicLevels[1/cm]  1
  0    1
End
GroundEnergy[kcal/mol]    -15.80228555 !-17.677+1.187
End
!Barriers
Barrier B1  W1  R          # MF~OH = MF + OH
```

RRHO

Stoichiometry C2H5O3

Core PhaseSpaceTheory

FragmentGeometry[angstrom] 8

C	0.82527400	0.43152500	-0.00003200
O	1.28292500	-0.67192200	0.00001900
O	-0.47256700	0.72765200	0.00007300
C	-1.35372100	-0.39789900	-0.00004400
H	-1.18674500	-1.00537100	0.88835000
H	-1.18254800	-1.00855600	-0.88541200
H	-2.35896200	0.01115500	-0.00308400
H	1.41607100	1.35518200	-0.00013300

FragmentGeometry[angstrom] 2

O	0.00000000	0.00000000	0.10815400
H	0.00000000	0.00000000	-0.86523400

SymmetryFactor 1

PotentialPrefactor[au] 13.96048875 !13.60473028

PotentialPowerExponent 6.

End

Frequencies[1/cm] 19

91.3023  
318.5380  
350.6410  
792.5903  
985.1802  
1067.7163  
1184.5877  
1204.2954  
1272.8776  
1405.5534  
1475.2131  
1487.0945  
1500.4241  
1850.7900  
3077.6375  
3102.3855  
3157.1877

3184.8780

3738.6669

ZeroEnergy[kcal/mol] 1.874495963

ElectronicLevels[1/cm] 1

0 2

End

Barrier B2 W1 P1 # MF~OH -&gt; TS -&gt; P2

RRHO

Geometry[angstrom] 10

C 0.14400800 0.49404000 -0.00033400

O -0.38311600 1.55743200 0.00022600

O -0.44866500 -0.69211700 -0.00037700

C -1.88370400 -0.65937800 0.00018300

H 1.30518200 0.32847200 -0.00065500

H -2.24303100 -0.14358400 -0.88867100

H -2.24233700 -0.14338300 0.88919900

H -2.20254500 -1.69644700 0.00040900

O 2.53545300 -0.37396500 -0.00000200

H 2.19153000 -1.28382700 0.00185800

Core RigidRotor

SymmetryFactor 1.

End

Frequencies[1/cm] 23

95.8609

100.6793

161.1072

167.3333

314.1870

391.5209

669.6510

762.0822

953.7332

993.5146

1027.5409

1186.9036

1200.4409

1251.2415

1477.1568

1495.8540

1505.1790

1688.3705

1894.2250

3086.6694

3167.2821

3207.4579

3758.9903

Tunneling Eckart

ImaginaryFrequency[1/cm] 792.2006

WellDepth[kcal/mol] 3.635950298

WellDepth[kcal/mol] 19.43823585

End

ZeroEnergy[kcal/mol] 3.635950298

ElectronicLevels[1/cm] 1

0 2

End

End