

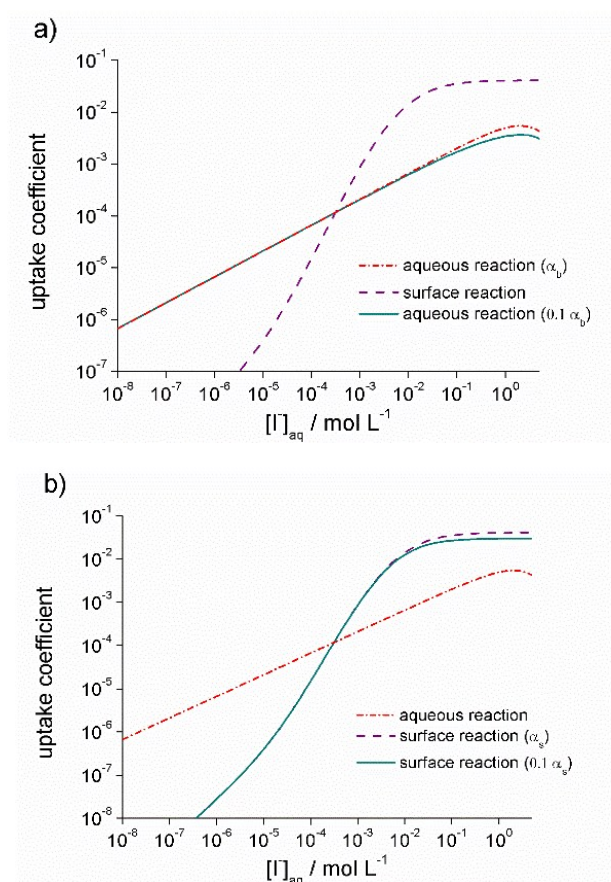
## Supplementary information

### A revisit of the interaction of gaseous ozone with aqueous iodide. Estimating the contributions of the surface and bulk reactions

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#### S1. Sensitivity analysis of accommodation coefficients on uptake coefficients

Sensitivity analyses of the bulk ( $\alpha_b$ ) and surface ( $\alpha_s$ ) accommodation coefficients on uptake coefficients are shown in Fig. S1. For the former, the values  $\alpha_b=0.01$  versus the base case value ( $\alpha_b=0.1$ ) have been contrasted (Fig. S1a). The minimum value of  $\alpha_b$  should be 0.002, as this is the value determined for water,<sup>1</sup> and should prevail at sufficiently low iodide concentrations, while the maximum value is expected to be  $>0.1$  because this is the value determined for 3 mol L<sup>-1</sup> aqueous NaI particles. For the surface accommodation coefficient, the values that have been contrasted in Fig. S1b are the minimum possible value, which is equal to the bulk accommodation coefficient ( $\alpha_s=0.1$ ) versus the maximum value ( $\alpha_s=1$ ). Both Figures S1a and S1b show that both accommodation coefficients influence uptake only at high iodide concentrations ( $>0.1$  mol L<sup>-1</sup> and  $>0.01$  mol L<sup>-1</sup>, respectively). This is because at high iodide concentrations the rate of reaction is fast enough so that O<sub>3</sub> uptake can become limited by accommodation instead of reaction.



**Fig. S1** Sensitivity analysis of the bulk (a) and surface (b) accommodation coefficient for  $[O_3]_{gs}=1$  ppm. The studied value is given between parenthesis as a function of the base case value ( $\alpha_b$  and  $\alpha_s$ , respectively).

## S2. Determination of apparent adsorption constants

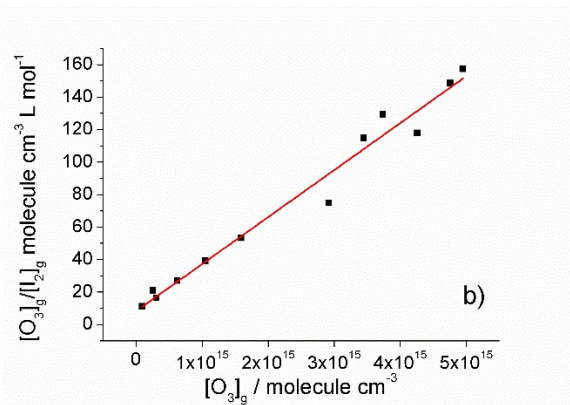
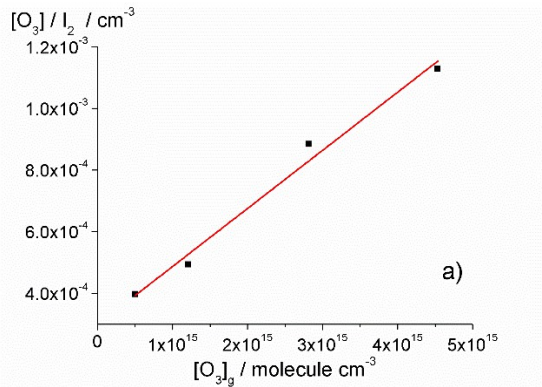
Figure 1 in Reeser et al.'s work<sup>2</sup> shows measured  $I_2$  production as a function of  $O_3$  concentration for  $[I^-]_{aq}=0.01 \text{ mol L}^{-1}$  and for a particular set of operating conditions (residence time of ozone, reactor dimensions, etc). The data from this figure have been used to obtain the apparent adsorption constant of ozone ( $K_{O_3,app}$ ) for those particular conditions, as explained below.

The data from the cited figure have been fit to a linear function that derives from equation 22:

$$[O_3]_g/n_{iodine} = \frac{\sigma}{f \cdot K_{O_3,app}} + \frac{\sigma}{f}[O_3]_g$$

where  $n_{iodine}$  is the amount of  $I_2$  produced and  $f$  is the factor of proportionality between the concentration of adsorbed ozone and  $I_2$  produced by the surface reaction among ozone and iodide. From the above equation it follows that a linear correlation of  $[O_3]_g/n_{iodine}$  versus  $1/[O_3]_g$  can be used to obtain  $K_{O_3,app}$  by dividing the y-intercept by the slope of this linear correlation. Using the slope and y-intercept of the correlation shown in Fig. S2a, the apparent constant for Reeser et al.'s<sup>2</sup> conditions is determined to be  $1.9 \cdot 10^{-19}/3.0 \cdot 10^{-4} \text{ cm}^3 \text{ molecule}^{-1} = 6 \cdot 10^{-16} \text{ cm}^3 \text{ molecule}^{-1}$ .

The same linearization has been used to obtain the apparent adsorption equilibrium constant for Sakamoto et al.'s<sup>3</sup> results of concentration of gas phase  $I_2$  as a function of ozone concentration (their Figure 3). The correlation is shown in Fig. S2b, whose slope and y-intercept allow to calculate  $K_{O_3,app}=4 \cdot 10^{-15} \text{ cm}^3 \text{ molecule}^{-1}$ .



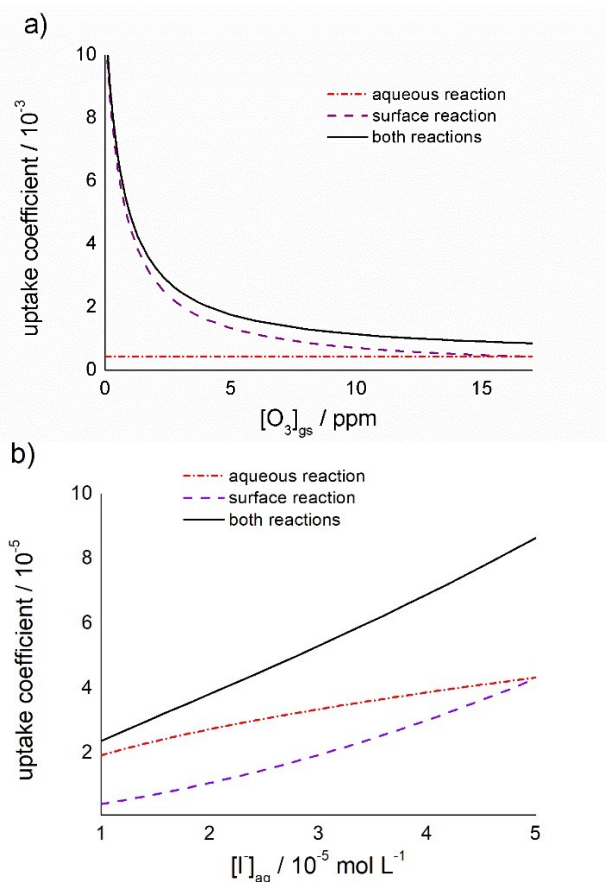
**Fig. S2** Linearization of data reported by Reeser et al.<sup>2</sup> for  $[I^-]_{aq}=0.01 \text{ mol L}^{-1}$  **(a)** and by Sakamoto et al.<sup>3</sup> for  $[I^-]_{aq}=5 \cdot 10^{-3} \text{ mol L}^{-1}$  **(b)** to obtain apparent adsorption equilibrium constants of ozone.

## S3. Estimation of the rate constant of the surface reaction $I^-_{(int)}+O_{3(surf)}$

Minimum and maximum rate constants ( $k_s$ ) of the surface reaction  $I^-_{(int)} + O_{3(surf)}$ , where  $I^-_{(int)}$  is aqueous iodide residing at the surface and  $O_{3(surf)}$  is adsorbed ozone, have been estimated using results from literature as explained below.

A lower limit of the rate constant can be estimated using the concentrations of a study where the surface reaction was found to be dominant and where the concentration of gaseous ozone near the surface ( $O_{3(g)}^s$ ) was relatively high, as sufficiently high concentrations of  $O_{3(g)}^s$  lead to aqueous-phase reaction dominance due to surface saturation in ozone. Results shown in Figure 3 by Sakamoto et al.<sup>3</sup> meet these conditions, where maximum  $[O_3]_{gs}$  is believed to be 17 ppm (see section S2) and  $[I^-]_{aq}=5 \cdot 10^{-3} \text{ mol L}^{-1}$ . The lower limit of  $k_s$  has been estimated imposing as a condition that, for these reactant concentrations, the uptake due to surface reaction be equal to the uptake to the aqueous-phase reaction. The result is  $k_{s,min}=3 \cdot 10^{-13} \text{ cm}^2 \text{ molecule}^{-1} \text{ s}^{-1}$ . Figure S3a shows the predicted uptakes for each reaction pathway for the conditions used by Sakamoto et al.<sup>3</sup>

An upper limit of the surface reaction rate constant can be estimated by considering the conditions of a study where a relatively high concentration of iodide and a low ozone concentration were used and aqueous-phase reaction dominance was concluded, as sufficiently high iodide concentrations lead to surface reaction dominance, according to the present model. Therefore, the conditions of the results of Carpenter et al.<sup>4</sup> will be used (specifically, their experiments with pure KI solution from Figure 1c). These authors<sup>4</sup> used an iodide concentration of up to  $5 \cdot 10^{-5} \text{ mol L}^{-1}$  and  $[O_3]_g=0.15 \text{ ppm}$ . In this case, it is not necessary to estimate  $[O_3]_{gs}$  to calculate the uptake because the uptake scarcely depends on  $[O_3]_{gs}$  at concentrations as low as 0.15 ppm. Imposing as a condition that, for these concentrations, the uptake coefficient due to each reaction pathway be equal to each other, a maximum surface reaction rate constant of  $4 \cdot 10^{-12} \text{ cm}^2 \text{ molecule}^{-1} \text{ s}^{-1}$  is obtained. Figure S3b shows the predicted uptake coefficients for the conditions used by Carpenter et al.<sup>4</sup>



**Fig. S3** Predicted uptake coefficients under the conditions used to estimate the lower and upper limit of the surface reaction rate constant ( $k_s$ ), respectively. Figure a corresponds to Sakamoto et al.'s<sup>3</sup> conditions (their Figure 3), where

$[I^-]_{aq}=5\cdot 10^{-3}$  mol L<sup>-1</sup>, and to the lower limit of  $k_s$  presently estimated, and Figure **b** corresponds to Carpenter et al.'s conditions<sup>4</sup> (their Figure 1c), where  $[O_3]_{gs}<0.15$  ppm, and to the upper limit of  $k_s$  estimated in the present work.

## References

1. R. G. Utter, J. B. Burkholder, C. J. Howard and A. R. Ravishankara, *The Journal of Physical Chemistry*, 1992, 96, 4973-4979.
2. D. I. Reeser and D. J. Donaldson, *Atmos. Environ.*, 2011, 45, 6116-6120.
3. Y. Sakamoto, A. Yabushita, M. Kawasaki and S. Enami, *J. Phys. Chem. A*, 2009, 113, 7707-7713.
4. L. J. Carpenter, S. M. MacDonald, M. D. Shaw, R. Kumar, R. W. Saunders, R. Parthipan, J. Wilson and J. M. C. Plane, *Nature Geosci.*, 2013, 6, 108-111.