

## Supporting Information

Mechanistic understanding of intergranular cracking in NCM cathode material:  
Mesoscale simulation with three-dimensional microstructure

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## Derivation process for simulation parameters

For LJ-SF parameters, the first step is to obtain the particle size distribution from the actual NCM image. We note that since we implement two models (LJ-SF + GH), we use two notations for the particle size ( $D$  for the GH and  $\sigma$  for LJ-SF) for distinguish the model. From the SEM image, we can determine the attractive energy  $\epsilon$ ,  $\sigma$  (or  $D$ ), and the cutoff distance  $r_c$ . To define the interaction between particles with different sizes, the mixing rule is implemented. In addition, we chose the range of  $\epsilon$  which can represent the Young's modulus value of NCM. The weighting factor of 1.2 for the cutoff distance is arbitrary chosen.

For GH model, the particle size  $D$  is already obtained from the procedure above. Then it is important to determine the elastic constant of  $K_n$  and  $K_t$  and the damping coefficient of  $R_n$  and  $R_t$ . First for the elastic constant, since the  $K$  is the function of effective parameters of Young's modulus ( $Y^*$ ), shear modulus ( $G^*$ ), size ( $D^*$ ), and the overlap distance ( $\delta$ ), it is important to obtain the actual  $Y$  and Poisson's ratio ( $\nu$ ) from the DFT calculations.<sup>1</sup> In addition,  $\delta$  is arbitrarily chosen as 25 nm, which is 1/10 of the average particle diameter. For the damping coefficient, it is a function of coefficient of restitution ( $e$ ), effective mass ( $m^*$ ), and the effective damping parameters of  $S_n$  and  $S_t$ . We assume that the coefficient of restitution ( $e$ ) is almost fully-elastic (0.95) because the amount of the dissipative energy after the particle collision is not critical concern for the current work. The mass of NCM is obtained from the density ( $\rho_p$ ) of NCM from previous DFT calculation by multiplying it with the volume. Finally,  $S_n$  and  $S_t$  is the function of  $Y^*$ ,  $G^*$ ,  $D^*$ , and  $\delta$ , which are already described.

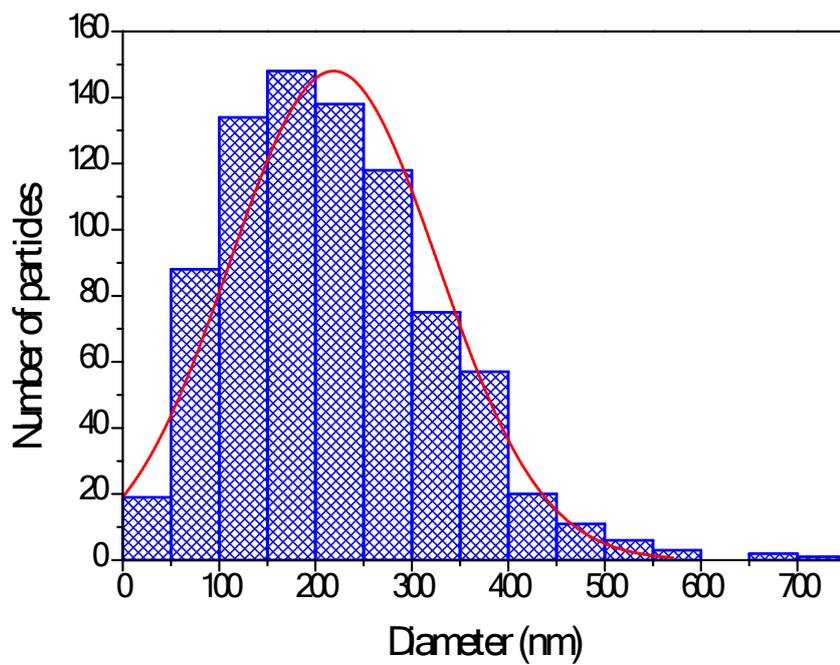


Figure S.2. The size distribution of primary particles from the FIB-SEM image

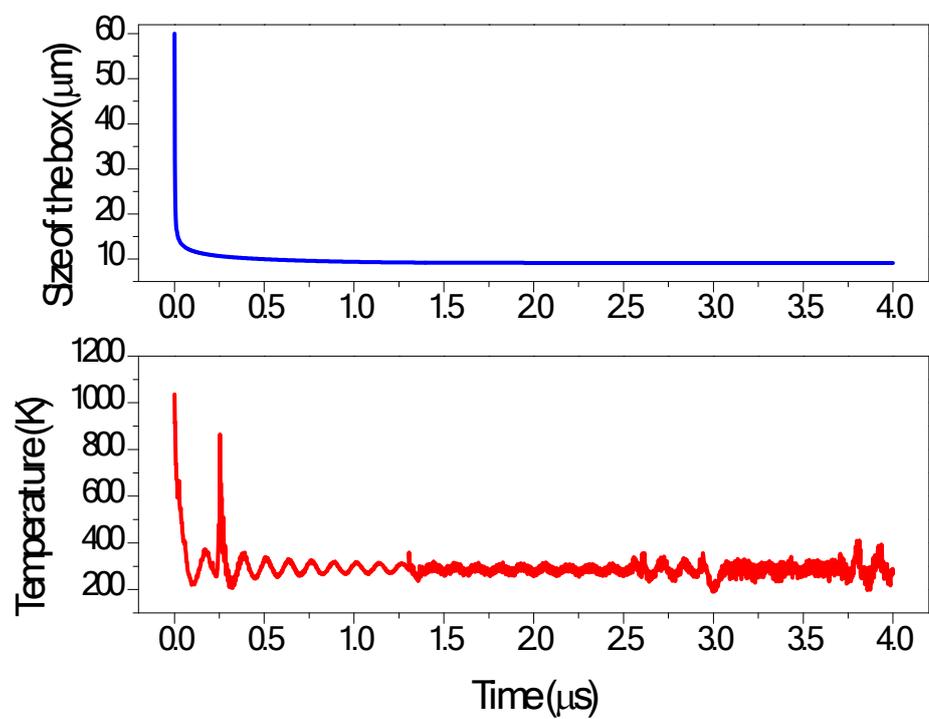


Figure S.3. Simulation output during NPT simulation for (a) the size of the simulation box and (b) the temperature.

Epsilon ( $\epsilon$ ) [pg/ $\mu\text{m}\cdot\mu\text{s}^2$ ]	10	$10^2$	$10^3$	$10^4$	$10^5$	$10^6$
Max. Stress [MPa]	0.83	6.11	46.09	328.84	2540.95	22005.85
Stress at 0.60 [MPa]	0.15	1.16	9.00	90.88	1212.37	12718.53
Reduction [%]	18.46	19.04	19.54	27.64	47.71	57.80

Table S.I. The percent reduction of the stress at strain of 0.6 after maximum stress value during tensile test for the structure with  $\epsilon = 1\text{e}1$  to  $1\text{e}6$  pg/ $\mu\text{m}\cdot\mu\text{s}^2$ .

**a**      **Open only in z-direction**      **Open boundary to all-direction**

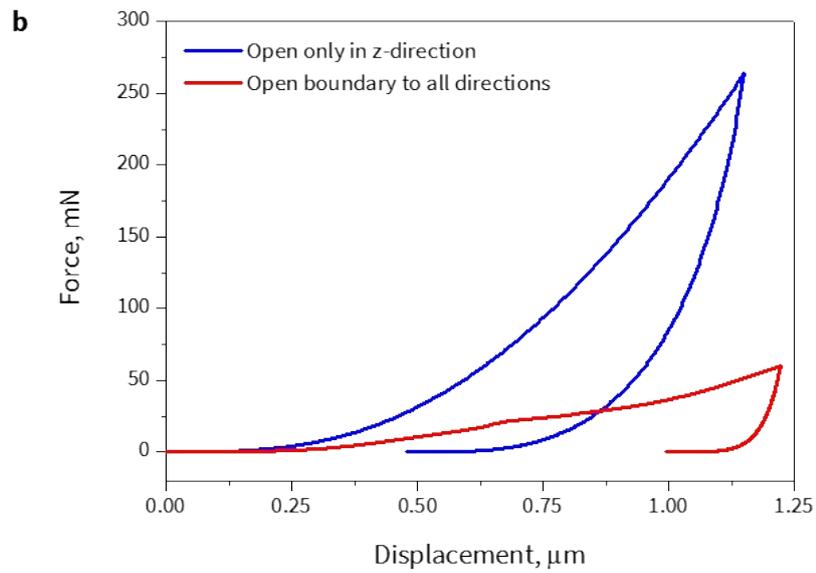
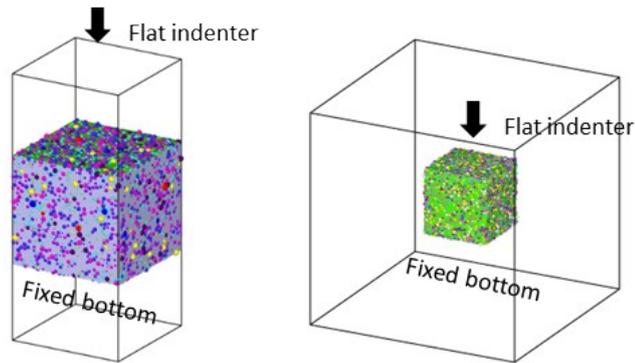


Figure S.4. (a) The boundary condition for NCM structure for nano-indentation test and (b) Force vs displacement curve for each case

## References

1. Min, K. & Cho, E. Intrinsic origin of intra-granular cracking in Ni-rich layered oxide cathode materials. *Phys. Chem. Chem. Phys.* **20**, 9045–9052 (2018).