Direct epoxidation of propene on silylated Au-Ti catalysts: A study on silylating procedures and effect on propane formation

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1 Mass transfer limitations

1.1 Internal diffusion: Weisz-Prater Criterion

The absence of internal mass transfer limitations was evaluated using the Weisz-Prater criterion [1], where if C_{WP} is lower than 1, the internal mass transfer effects can be neglected:

$$C_{WP} = \frac{-r_{A,\,Obs}\,\rho_c R^2}{D_e C_{AS}} < 1 \tag{S.1}$$

 $-r_{A,Obs}$, Observed reaction rate = 4.83 \cdot 10⁻⁷ kmol/kg_{cat}/sec (taking the maximum PO rate found)

 $\rho_{c'}$ Solid density of catalyst = 350 kg/m³

R, Particle size = $25 \,\mu\text{m} = 2.5 \cdot 10^{-5} \,\text{m}$

 C_{AS} , Concentration of reactant A on surface. A = Propene. Considering 10 vol% propene,

$$C_{AS} = 4 \cdot 10^{-3} \text{ kmol/m}^3$$

 D_e , effective diffusity given by:

$$D_e = \frac{D_{AB}\varepsilon_p \sigma_c}{\tau}$$
(S.2)

 D_{AB} , Gas-phase diffusivity. D_{AB} for a mixture of C₃H₆-He was calculated [2] to be 8.75·10⁻⁵ m²/s

 ε_p , Pellet porosity = 0.4,

 σ_c , Constriction factor = 0.8,

au , Tortuosity = 3.

$$D_e = 9.33*10^{-6} \text{ m}^2/\text{s}$$

Putting the above values in S.1,

$$C_{WP,P0} = \frac{(4.83 \cdot 10^{-7}) \cdot (3.5 \cdot 10^2) \cdot (25 \cdot 10^{-6})^2}{(9.33 \cdot 10^{-6}) \cdot (4.0 \cdot 10^{-2})} = 2.83 \cdot 10^{-7} \ll 1$$

Therefore, this system does not suffer from internal mass transfer limitations.

1.2 External Diffusion: Mears Criterion

The absence of external mass transfer limitations can be evaluated using the Mears criterion [1]:

$$C_{M} = \frac{-r_{A}^{'} \rho_{b} R n}{k_{c} C_{Ab}} < 0.15$$
(S.3)

 $-r_{A,Obs}$, Observed reaction rate = 4.83 · 10⁻⁷ kmol/kg_{cat}/sec

 ho_b , bulk density of the catalyst bed = 350 kg·m-3

R, Particle size = 25
$$\mu$$
m = 2.5 \cdot 10⁻⁵ m

 k_c mass transfer coefficient = 0.089 m.s⁻¹

k_c was calculated from the Sherwood number using the correlation from Perry's Handbook [2]:

$$\frac{k_c d_p}{D_A} = 0.91 \cdot 91 \cdot Re^{0.49} . Sc^{1/3}$$
(S.4)

Putting the values together we get:

$$C_M = \frac{(4.83 \cdot 10^{-7}) \cdot (3.5 \cdot 10^2) \cdot (25 \cdot 10^{-6}) \cdot 1}{(0.089) \cdot (4.0 \cdot 10^{-2})} = 1.18 \cdot 10^{-6} \ll 0.15$$

It can thus be concluded that the system does not suffer from external mass transfer limitations.

2. TEM of synthesized catalysts





Figure S.1 TEM of Au(0.1)/Ti(1)SiO₂ (left) and Au(1)/Ti(5)SiO₂ (right)

3. Reactions using different silylating agents

3.1 TEFS



3.2 TMCS



3.3 TMDS



3.4 HMDS



4. Preliminary results

In the main text we note that liquid phase silvlation procedures are not carried out on the Au loaded catalysts. This is because our initial results suggested that this led to in loss in catalytic activity as shown in Table S.1.

Table S.1: Perform	nance of silylated	and unsil	ylated cata	lysts#
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Catalyst	Unsilylated	Silylated (using TMCS in liquid phase)
Conversion(%)	3.1	1.5
Selectivity to PO (%)	77	68
H ₂ efficiency (%)	14	17
r _{PO} (g _{PO} /kg _{cat} /h)	71	29

[#]Reaction conditions: $H_2/O_2/C_3H_6/He = 1:1:1:7$, Temp = 473 K, GHSV = 10000 mL.g_{cat}⁻¹.h⁻¹

References

[1] H.S. Fogler, Elements Of Chemical Reaction Engineering, Prentice Hall Professional Technical Reference, 2006.

[2] R. Perry, D. Green, Perry's Chemical Engineers' Handbook, Eighth Edition, McGraw-Hill Education, 2008.